

Our Ref: 1584

30 June 2011

Insight Unlimited Ltd P.O Box 1219 GISBORNE 4040

Attention: John Radburn

Dear John,

Re: Opawa Library – POST-EARTHQUAKE INSPECTION

Scope of this Report

This report covers our assessment of the structural condition of the Opawa Library building at 151 Opawa Rd, Opawa, Christchurch, following the magnitude 6.3 earthquake on 22nd February 2011. Our assessment is based on a visual inspection inside and out, which was carried out on the 28th April 2011and again on 11th May 2011.

This report describes the damage observed, and comments on remedial work options for both temporary securing of the building, and long term repair where appropriate. This report does not cover a detailed structural strength assessment or detailed specification of remedial works, which may be required by the client following consideration of this report.

1. Scope of Investigation

On the 28th April 2011 and again on 11th May 2011, we visually inspected the building including: The exterior from ground level The interior

This report is based on our assessment of the building at the time stated. Photos attached in Appendix A are indicative of the damage. Any subsequent loading by aftershocks, or high winds, may initiate further damage.

2. Building Description

General description:

The Opawa Library is a single storey gable structure consisting of double skin unreinforced brick walls with light timber framed roof structure supporting concrete roof tiles. The building is approximately 11m wide by 22m long and approximately 240m2 with an eaves



dimension approximately 3.0m. It has a small lean to attached of approximately 10m2 to the rear. The occupancy classification is library.

The building was first constructed in the early 1900's, with the rear addition added at a later date.

The building was being used as a library, but is currently unoccupied due to earthquake damage. The occupancy classification in NZS1170 is E (Reading rooms with book storage e.g. libraries) with an occupant load of 36 as classified by the Building Code Clause C table 2.2 and importance level of 2.

Roof construction: Concrete tiles on timber framing.

External Wall construction:

Double skin unreinforced brick walls with solid plaster over.

Internal Wall construction:

Double skin unreinforced brick walls with solid plaster over. Light timber framing lined with plasterboard.

Floor construction:

Timber framing on piles, with a concrete perimeter foundation wall.

Structural System:

The structural system can be described as face loaded unreinforced masonry nominally supported at floor level and ceiling/roof level but nominal diaphragms taking loads back to unreinforced masonry walls acting in-plane. Load then transfers to mass concrete foundations to the ground.

3. Strength

The strength of the building has been determined as a % NBS using methodologies provided by NZSEE.

Before September 2010:

The strength of the building before September 2010 is determined as Using pre 19 May 2011 site hazard coefficient of 0.22

Main Building 40% NBS

Gables 14% NBS

Using post 19 May 2011 site hazard coefficient of 0.3

Main Building 30% NBS

Gables 10% NBS (using post 19 May 2011 site hazard factor of 0.3)

On day of inspection:

The strength of the building on the day of inspection is determined asUsing post 19 May 2011 site hazard factor of 0.3Main Building30% NBSGables0% NBS



The % NBS determined relies upon the ceiling acting as a diaphragm adequately tied to the walls and it has also been assumed that there is a concrete beam running around the top of the wall. These elements have yet to be confirmed and require destructive investigation to assess. From our inspection of the ceiling and walls and their intersection we believe that this is a reasonable assumption for the %NBS level determined.

4. Damage Description

Damage caused by the February earthquake to the Opawa Library is described below. Damage described is additional to earlier earthquake damage. Refer to Appendix B for marked-up drawings indicating damaged locations.

i. General Damage:

General damage includes cracking of plaster on masonry walls and foundations.

ii. Damage to Gables:

The Front Gable has collapsed. The remaining two side gables on the original building are cracked at their support and leaning.

iii. Damage to Join between Original and Extension: A large vertical crack has opened up between the original construction and extension.

iv. Damage to Interior Walls:

The interior walls have numerous cracks in the surface plaster to brick walls and timber framed walls

v. Damage to Ceilings:

The ceilings have numerous cracks mainly around the edges and in the front portion of the building.

vi. Liquefaction:

There is general liquefaction around the greater local area but none adjacent to the building. Liquefaction does not appear to have affected the foundations.

5. Immediate Securing of the Building

The following works are required to mitigate immediate hazards, temporarily secure the building, and provide weather tightness:

Fence of site completely and restrict access especially adjacent gables and at the vertical crack location.

The three front gables should be removed and a temporary plywood lining over new framing installed to provide temporary water proofing.

The wall adjacent the vertical crack should be propped to prevent the possibility of collapse.

Access to the front section of the building is viable without further need for securing. Books etc may be retrieved under supervision of an Engineer.



Due care, safety equipment and precautions must be taken when carrying out the above work. Maintain awareness of fall hazards and escape routes if entering the building.

6. Long Term Repair

This section of the report outlines options for repair to restore the building to its preearthquake condition. Options for repair and/or strengthening will need to be discussed with the owner, and will be subject to revised local authority legislation.

i. Gables:

Install new timber framing and solid plaster gable on cavity battens to the three gables to the original building.

ii. Joint Between Original and Extension:

Seal crack using a pressure injected epoxy (e.g. Sikadur injectokit and Sikadur520, or similar). Install new steel plate to exterior and interior and bolt through wall sandwiching the wall plus install new bolts epoxied into the back of the return wall.

iii. General Cracking to Foundations:

Seal all cracks in concrete foundation wall larger than 0.2mm with a pressure injected epoxy (e.g. Sikadur injectokit and Sikadur 52⁰), or similar). Seal smaller cracks by painting over with a brushable crack filler (e.g. Resene Brushable Crack Filler).

iv. General Interior Repair to Cracks in Walls and Ceilings:

Repair as appropriate using one of the following: Grind-out v-shape into cracked plaster. Re-plaster and overlay crack with fibreglass reinforcing mesh. Re-plaster over to provide a smooth finish. Remove lath and plaster walls and replace with Braceline GIB, or plaster over corru-lath/rib-lath.

In all cases, wall ties and hold-down straps should be installed in accordance with GIB braced wall and ceiling diaphragm specifications.

Realign, re-fix and re-paint racked door frames and architraves.

iv. Strengthening to provide 67%NBS or 100%NBS if this was necessary:

Two options are available

1. Strengthening could be completed the installation of ceiling diaphragms and substantial fixings between diaphragm and walls. Walls will require strengthening for face loading via ties being installed between the brick skins (e.g. Helifix Cemtie) and either filling the cavity or installing steel mullions internally.



2. Strengthening could be successfully completed by removing the internal brick skin and replacing it with a new timber framed wall. Tying the external skin to the new framing. Install new linings to provide any bracing required. Install conventional ceiling diaphragms. Steel studs will be required adjacent windows to support any concrete lintels.

Either option is likely to bring the building back up to 100%NBS by default.

The costs associated with the repairs would require the appropriate professional to visit the site to view the extent of damage. At this stage we have not provided any specific detailing for repair works but can so at your request.

7. Elements Not Inspected

The following is a list of elements not specifically inspected:

- Subfloor construction
- Piles
- Roof space
- Soils
- 8. Limitations

Findings presented in this report are for the sole use of the client. The findings may not contain sufficient information for use by other parties, and as such should not be relied upon unless discussed with Structural Concepts Ltd. We have exercised our services in a professional manner using a degree of care and skill normally, under similar circumstances, by reputable consultants practicing in this field at this time. No other warranty, expressed or implied, is made as to the professional advice presented in this report.

Yours faithfully STRUCTURAL CONCEPTS LTD

Garry Newton BE (Civil), MIPENZ(Civil, Structural), CPEng, IntPE(NZ)

Director



APPENDIX A. PHOTOGRAPHS

<u>Please note that the photographs provided in this report are not high quality and are for</u> providing information that shows the indicative damage found around the building for structural engineering assessment only.









































APPENDIX B. MARKED-UP DRAWING INDICATING DAMAGED LOCATIONS







APPENDIX C. REPAIR AND STRENGTHENING WORKS

STRUCTURAL CONCEPTS LIMITED				
55 DUNLOP ROAD, PO BOX 3315	Client:	Christchurch City Council	Ref:	1584
NAPIER, 4142, NEW ZEALAND	Project:	Opawa Library	Date:	26/5/11
P (06) 842 0111 F (06) 842 0113		151 Opawa Road, Opawa, Christchurch	BY:	GN
E info@structuralconcepts.co.nz	Subject:			
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Sketch Details Gable Sketch - Section

existing _____ structure existing nail plate new Soming building L new Granney len -New plaster on mobilities on baittens existing well. flashing

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			Sheet No.:	SK2

Sketch Details Creck Repair





APPENDIX D. DESIGN FEATURES REPORT



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Client: Christchurch City Council

Project: Opawa Library 151 Opawa Road, Opawa, Christchurch

Ref: 1584

Date: 26-May-11

CALCULATIONS

BY GARRY NEWTON

BE (Civil), MIPENZ(Civil, Structural), CPEng, IntPE(NZ)

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Design Features Report

<u>Scope</u>

In general terms, the scope of work is as follows:

- Provide bracing design for timber frame building for a residential building.

Means of compliance

The following standards have been used:

- NZS 1170.0:2002
- NZS 1170.1:2002
- NZS 1170.5:2004

THE STRUCTURE

<u>General</u>

The building is constructed of double skin unreinforced brick walls on a concrete ring foundation. The ground floor is timber over joists and bearers on piles. The roof consists of light timber framed roof structure supporting concrete roof tiles. The location of the building is 151 Opawa Road, Opawa, Christchurch. The importance level for the building has been assessed as Importance Level 2. The design life of the structure is 50 years. For the purpose of analysis, the across and along directions are as per the geometric shape.

Chosen Design Life		50 Years
Chosen Importance Level		2
Annual Probability of exceedance (inve	erse) Ultimate	500
Annual Probability of exceedance (inve	erse) Service	25
Gravity structure		
Load paths: \rightarrow \rightarrow	\rightarrow	\longrightarrow
Trusses/rafters Walls	~	foundations
Lateral load resisting structure		
Across the building	>	\rightarrow
Roof \longrightarrow In-plane masonry	foundatio	ns
walls		
Along the building		
Roof → In-plane masonry ⁻ walls		ns

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Sheet No.: 3

Design Features Report

<u>Significant Design Features</u> There are no special design features.

SOIL CONDITIONS

No specific Soils investigation or report has been completed at this time. We have noticed that there has been lateral spread and liquefaction adjacent to the building and we recomend that a specific soils report be sort to confirm design assumptions. at this stage we have assumed low bearing pressures of factored ULS 75 kPa.

DESIGN LOADS

Vertical loads

All Dead loads are listed on the gravity loads sheet at the front of these calculations.

All Live loads are listed on the gravity loads sheet at the front of these calculations.

<u>Lateral Loads</u> <u>Wind</u>

Site wind speed 37.35 Ult (m/s)

Further information on wind speeds, internal pressures etc are on the main wind load sheets contained in these calculations.

Seismic loads

Analysis methodology

The seismic analysis has been completed in accordance with NZS 1170.5:2004. Design Spectra are in accordance with NZS 1170.5:2004 for site sub soil class D. Analysis has been completed using the Equivalent Static Method for bracing. A Seismic Hazard Factor of Z=0.3 has been used.

Across the building		
Structural ductility factor (Ultimate)	μ	2.00
Structural Performance factor (Ultimate)	Sp	1.00
Along the building		
Structural ductility factor (Ultimate)	μ	2.00
Structural Performance factor (Ultimate)	Sp	1.00

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Design Features Report

SERVICEBILITY CRITERIA

The following servicebility criteria have been chosen for the project: Note: These are generally in line with those recommanded in NZS1170.2 Table C1.

Seismic deflections/storey drift	Criteria	Phenomenon controlled
Maximum allowable deflection (SLS)	spacing/200	Damage to cladding
Maximum allowable storey Drift (ULS)	height/40	Soft storey protection
Wind deflections		
Maximum allowable lateral deflection (SLS)	spacing/200	Damage to cladding
Maximum allowable vertical deflection (SLS)	span/200	Damage to cladding/finishes
Gravity deflections		
Maximum allowable deflection (SLS)	span/500	Visual sag

SOFTWARE

The following computer applications were used for the design:

Analysis type	Software used
Stuctural analysis	Excel 2009
Structural design	Excel 2009

Significant or Special Construction Features

None.

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Loads

Roof Concrete tiles Timber 20.6 Purlins 05 .4 Battens 05 1.2 Rockwool Insu. Gypsum Plaster	0.530 0.092 0.034 0.011 0.002 0.130	External Walls brick brick Lime Plaster Lime Plaster	2.200 2.200 0.240 0.240
	0.800 kPa		4.880 kPa
Timber floor 21mm Particie Bd Timber 20.6 90. Nogs & plates Battens 05 1.2 Rockwool Insu. Gib Board 13	0.150 0.092 0.067 0.011 0.002 0.120	Partitions Timber 10.4 90. Nogs & plates Gib Board 10 Gib Board 10	0.069 0.067 0.090 0.090
	0.442 kPa		0.316 kPa
		<u>Live loads</u> E Reading rooms	4.00 kPa

R2 Roofs

0.25

kPa

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Client: Christchurch City Council Project: Opawa Library 151 Opawa Road, Opawa, Christchurch Subject: Seismic loads to NZS1170

Ref:	1584
Date:	26/5/11
BY:	GN

<u>Seismic</u>	Loads to NZS 1170.5							Sheet No.:	6
Ref:	Design							Output	
	Design working live					50 Years			
	Importance level					2			
	Annual Probability of exceedance (inverse) Ultimate 500								
	Annual Probability of	l Probability of exceedance (inverse) Service							
	Element	Element Roof			Area/length Load Kpa		Live lo	ad reduction	
	Roof				0.80	95.94	Total floor area	0.0	
	External Walls			60.00	4.88	292.80		-	
				0.00	0.00	0.00	3+	3	
				0.00	0.00	0.00	.51	\sqrt{A} =	1.000
				0.00	0.00	0.00	But not	t less than .5	
				0.00	0.00	0.00			
		1.00	0.40	0.00	0.00	0.00			
						388.74	kN		

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Ei	nfo@structuralconcepts.co.nz	Subject: Seismic loads	s to NZS1170						
							7		
	Dosign					Sheet No.:	Ι		
	Soil type					Output			
		_							
	C. Shallow Soil Across the building	•							
	Period of building acr	oss the building		0.40					
	Does the seismic brac	cing have ductile capabi	lities but is desig	ned as r	nominally d	uctile			
	Structural ductility fac	tor (Ultimate)	m =	2.00					
	Structural ductility fac	tor (Service SLS1)	m =	1.25					
	Hazard Factor	Christchurch	Ζ =	0.3					
	Return period factor		Ru =	1.00					
	Return period factor		Rs =	0.25					
	Structural Performance	e factor (Ultimate)	Sp =	0.70					
	Structural Performance	ce factor (Service)	Sp =	0.70					
	Spectral Shape Facto	or (across)	Ch(T) =	2 36					
	Near Fault factor		N(T D) =	1.0	n/a				
	Flastic site spectra (U	timate)	С(Т) =	0.71	n# d				
	Elastic site spectra (Se	arvice)	= (т)Э	0.18					
	Lilitimate		km =	1 57					
	Service		km =	1.57					
	Ultimate			1.14					
	Horizontal design acti	ion coefficients (Across)	Cd(I1) -	0 22	But not la	 ss than 0.0	30 D u		
	Illtimate force across	the building	Cd(T1) x Wi –	122.60	kN Total		30110		
	Service	and ballaning		122.00	in rotar				
	Horizontal design acti	ion coefficients (Across)	Cd(I1) -	0 11					
	Service force across t	he building	Cd(T1) x Wi –	0.11 12 11	kN Total				
	Along the building	ne building		42.14	KN IOLAI				
	Period of building alo	na the huilding		0.40					
	Deep the seizmic bracing have ductile capabilities but is designed as periodly directly								
	Structural ductility fac								
	Structural ductility fac	tor (Sonvice SLS1)	m –	2.00					
	Structural Performance	co factor (Illtimate)	- III - Sp -	1.25					
	Shactral Shana Fasta			0.70					
	Specifal Shape Facil			2.30					
		timeta)	N(I,D) =	1.0					
	Elastic site spectra (UI		C(I) =	0.71					
	Elastic site spectra (Se	ervice)	∪(I) = km =	0.18					
				1.57					
	Service		кш =	1.14					
				.			200.		
	Horizontal design act	ion coefficients (Across)	Cd(11) =	0.32	BUT NOT IE	ss than 0.0 I	30RU		
	ultimate force along	ine building	Ca(II) X WI =	122.60	KIN IOTAI				
	<u>Service</u>								
	Horizontal design acti	ion coefficients (Across)	Cd(I1) =	0.11					
	Service force across t	he building	Cd(11) x Wi =	42.14	kN Total				