

City Care Milton Street Depot Plant Maintenance Workshop, Part 1 & 2 Detailed Engineering Evaluation BU 1141-002 EQ2 Quantitative Report

Prepared for Christchurch City Council (Client)

By Beca Carter Hollings & Ferner Ltd (Beca)

14 June 2013

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Revision History

Revision Nº	Prepared By	Description	Date
A	George El Haddad	Draft for CCC review	1 March 2013
B	Laura Chen	Final	14 June 2013

Document Acceptance

Action	Name	Signed	Date
Prepared by	George El Haddad		14 June 2013
Reviewed by	Nicholas Charman		14 June 2013
Approved by	David Whittaker		14 June 2013
on behalf of	Beca Carter Hollings & Ferner Ltd		

City Care Milton Street Depot – Plant Maintenance Workshop, Part 1 & 2 BU 1141-002 EQ2

Detailed Engineering Evaluation Quantitative Report – SUMMARY Version 1

Address

245 Milton Street
Sydenham
Christchurch



Background

This is a summary of the Quantitative Assessment report for the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

Separate Qualitative Reports for the Plant Maintenance Workshop Part 1 and Part 2 were issued to CCC on 4 September 2012

The Plant Maintenance Workshop Part 1 and 2 (Plant Maintenance Workshop) is located at the City Care Milton St Depot at 245 Milton Street, Sydenham, Christchurch. It is part of the same building which also encompasses the Tyre Bay (BU 1141-011 EQ2) and primarily consists of steel portal frames with precast concrete shear walls. The structural drawings available indicate the Plant Maintenance Workshop was designed in 1979. Calculations have been undertaken as part of the Quantitative Assessment.

Key Damage Observed

Visual inspection on 8 February 2012 indicates the building has suffered minor damage. Key damage observed includes:

- n Minor cracking to concrete encasement of steel columns.
- n Cracking along vertical joint between concrete wall and internal timber framed wall.
- n Horizontal cracking to concrete shear walls.
- n Cracking of the sealant in the vertical movement joints between concrete panels.
- n Cracking in masonry block wall mortar joints in the oxygen storage area.

Critical Structural Weaknesses (CSW)

The following Critical Structural Weaknesses have been identified:

- n Site characteristics due to liquefaction occurring on the Milton St site.

Indicative Building Strength (from Detailed Assessment)

The building has been assessed to have a seismic capacity in the order of 35%NBS, using the New Zealand Society for Earthquake Engineering (NZSEE) Detailed Assessment guideline 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. The Plant Maintenance Workshop is therefore classified as Earthquake Risk and Seismic Grade C.

The structural damage observed is predominantly minor and the seismic capacity is not considered to have materially diminished from its pre-earthquake level.

Our assessment has identified the structural components that have governed/limited the building's seismic performance, and their potential failure mechanisms, are as follows:

- n Overturning capacity of the precast shear walls and foundation achieves 35%NBS under longitudinal (in-plane) loading.
- n RHS door header (tie member) connections under longitudinal (in-plane) loading achieve 36%NBS.
- n Eaves channel (tie member) connections under longitudinal (in-plane) loading achieve 38%NBS.
- n Precast panel connections to the portal frames achieve 46%NBS under longitudinal (in-plane) loading.

Recommendations

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be earthquake risk, having an assessed capacity of between 34% and 67% NBS. The risk of collapse of an earthquake risk building is considered to be 5 to 10 times greater than that of an equivalent new building.

No significant damage or hazards were identified to the seismic or gravity load resisting system that would reduce its ability to resist further loads and therefore no restrictions on use or occupancy are recommended.

It is recommended that:

- n A level survey could be carried out to determine the extent of settlement of the building for insurance purposes.
- n According to the recent CCC Instructions to Engineers document (16 October 2012), Council's insurance provides for repairing damaged elements to a condition substantially as new. We suggest you consult further with your insurance advisor.

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1 Background

Beca Carter Hollings & Ferner Ltd (Beca) has been engaged by Christchurch City Council (CCC) to undertake a Quantitative Detailed Engineering Evaluation (DEE) of the Plant Maintenance Workshop building located at 245 Milton Street, Sydenham, Christchurch.

This report is a Quantitative Assessment of the building structure, and is based on the document 'Guidance on Detailed Engineering Evaluation of Earthquake Affected Non-residential Buildings in Canterbury – Part 2 Evaluation Procedure' (draft) issued by the Engineering Advisory Group (EAG) on 19 July 2011.

A quantitative assessment involves analytical calculations of the building's strength and may involve material testing, geotechnical testing and intrusive investigation. The qualitative assessment previously carried out involved inspections of the building, a desktop review of existing structural and geotechnical information, including existing drawings and calculations, if available and an assessment of the level of seismic capacity against current code using the Initial Evaluation Procedure (IEP).

The purpose of these assessments is to determine the likely building performance and damage patterns, to identify any potential Critical Structural Weaknesses (CSW) or collapse hazards, and to make an assessment of the likely building strength in terms of percentage of New Building Standard (%NBS).

A full set of structural drawings was made available and has been used in our assessment of the building. The building description below is based on a review of the drawings and our visual inspections.

The format and content of this report follows a template provided by CCC, which is based on the EAG document.

2 Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

2.1 Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 – Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 – Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee carry out a full structural survey before the building is re-occupied.

We understand that CERA will require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building Act). It is understood that CERA is adopting the Detailed Engineering Evaluation Procedure document (draft) issued by the Engineering Advisory Group on 19 July 2011, which sets out a methodology for both qualitative and quantitative assessments. We understand this report will be used in response to CERA Section 51.

The qualitative assessment includes a thorough visual inspection of the building coupled with a desktop review of available documentation such as drawings, specifications and IEP's. The quantitative assessment involves analytical calculation of the building's strength and may require non-destructive or destructive material testing, geotechnical testing and intrusive investigation.

It is anticipated that factors determining the extent of evaluation and strengthening level required will include:

- n The importance level and occupancy of the building
- n The placard status that was assigned during the state of emergency following the 22 February 2011 earthquake
- n The age and structural type of the building
- n Consideration of any Critical Structural Weaknesses
- n The extent of any earthquake damage

2.2 Building Act

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 – Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to any alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

Section 115 – Change of Use

This section requires that the territorial authority (in this case Christchurch City Council (CCC)) be satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'. Regarding seismic capacity 'as near as reasonably practicable' has previously been interpreted by CCC as achieving a minimum of 67%NBS however where practical achieving 100%NBS is desirable. The New Zealand Society for Earthquake Engineering (NZSEE) recommend a minimum of 67%NBS.

Section 121 – Dangerous Buildings

The definition of dangerous building in the Act was extended by the Canterbury Earthquake (Building Act) Order 2010, and it now defines a building as dangerous if:

- n In the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
- n In the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
- n There is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a 'moderate earthquake' (refer to Section 122 below); or
- n There is a risk that that other property could collapse or otherwise cause injury or death; or

- n A territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.

Section 122 – Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property. A moderate earthquake is defined by the building regulations as one that would generate ground shaking 33% of the shaking used to design an equivalent new building.

Section 124 – Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 – Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

2.3 Christchurch City Council Policy

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake of the 4th September 2010.

The 2010 amendment includes the following:

- n A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
- n A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
- n A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
- n Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

It is understood that any building with a capacity of less than 33%NBS (including consideration of Critical Structural Weaknesses) will need to be strengthened to a target of 67%NBS of new building standard as recommended by the Policy.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply 'as near as is reasonably practicable' with:

- n The accessibility requirements of the Building Code.
- n The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

2.4 Building Code

The building code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.

On 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

- Hazard Factor increased from 0.22 to 0.3 (36% increase in the basic seismic design load)
- Serviceability Return Period Factor increased from 0.25 to 0.33 (80% increase in the serviceability design loads when combined with the Hazard Factor increase)

The increase in the above factors has resulted in a reduction in the level of compliance of an existing building relative to a new building despite the capacity of the existing building not changing.

3 Earthquake Resistance Standards

For this assessment, the building's Ultimate Limit State earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The new building standard load requirements have been determined in accordance with the current earthquake loading standard (NZS 1170.5:2004 Structural design actions - Earthquake actions - New Zealand).

No consideration has been given at this stage to checking the level of compliance against the increased Serviceability Limit State requirements.

The likely ultimate capacity of this building has been derived in accordance with the New Zealand Society for Earthquake Engineering (NZSEE) guidelines 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. These guidelines provide an Initial Evaluation Procedure that assesses a building's capacity based on a comparison of loading codes from when the building was designed and currently. It is a quick high-level procedure that can be used when undertaking a Qualitative analysis of a building. The guidelines also provide guidance on calculating a modified Ultimate Limit State capacity of the building which is much more accurate and can be used when undertaking a Quantitative analysis.

The New Zealand Society for Earthquake Engineering has proposed a way for classifying earthquake risk for existing buildings in terms of %NBS and this is shown in Figure 3.1 below.

Description	Grade	Risk	%NBS	Existing Building Structural Performance	Improvement of Structural Performance	
					Legal Requirement	NZSEE Recommendation
Low Risk Building	A or B	Low	Above 67	Acceptable (improvement may be desirable)	The Building Act sets no required level of structural improvement (unless change in use) This is for each TA to decide. Improvement is not limited to 34%NBS.	100%NBS desirable. Improvement should achieve at least 67%NBS
Moderate Risk Building	B or C	Moderate	34 to 66	Acceptable legally. Improvement recommended		Not recommended. Acceptable only in exceptional circumstances
High Risk Building	D or E	High	33 or lower	Unacceptable (Improvement	Unacceptable	Unacceptable

Figure 3.1: NZSEE Risk Classifications Extracted from Table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table 3.1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% risk of exceedance in 50 years (i.e. on average 0.2% in any year). It is noted that the current seismic risk in Christchurch results in a 6% risk of exceedance in the next year.

Table 3.1: %NBS Compared to Relative Risk of Failure

Building Grade	Percentage of New Building Standard (%NBS)	Approx. Risk Relative to a New Building
A+	>100	<1
A	80-100	1-2 times
B	67-80	2-5 times
C	33-67	5-10 times
D	20-33	10-25 times
E	<20	>25 times

4 Building Description

4.1 General

Summary information about the building is given in the following table. The Plant Maintenance Workshop is part of the same structure which contains the Tyre Bay.

Table 4.1: Building Summary Information

Item	Details	Comment
Building name	City Care Milton Street Depot – Plant Maintenance Workshop,	
Street Address	245 Milton Street Sydenham Christchurch	
Age	Designed in 1979	From drawings available
Description	Single storey garage facility	
Building Footprint / Floor Area	Approx. 100m x 15m, 1500m ² internally	Excluding Tyre Bay area
No. of storeys / basements	1 storey/no basement	2 storey office area at centre of building
Occupancy / use	Workshop and offices	Importance Level 2
Construction	Steel portal frame with glazed infills and concrete walls. Concrete frame in office area. A timber framed extension at the entrance to the two storey office area was designed in 1995.	The timber extension is tied into the concrete frame of the office area.
Gravity load resisting system	Timber framed roof supported by steel portal frames. Concrete ground to mezzanine floor structure in two-storey office.	
Seismic load resisting system	The transverse lateral load resisting system comprises steel portal frames. The longitudinal lateral load resisting system	The drawings indicate rod bracing on both the north and south elevations of the building, however site

Item	Details	Comment
	<p>comprises of a plywood roof diaphragm which transfers the load through struts/ties at the eaves level into the precast panel shear walls at each end of the building (Tyre Bay and Plant Maintenance Workshop).</p> <p>In the two storey office area, the lateral load resisting system is reinforced concrete frames in both directions (ground to mezzanine), with transverse portal frames from mezzanine floor level and tied into the primary longitudinal load resisting system at door header level.</p> <p>Lateral loads from the timber framed extension are resisted by the concrete frames of the office area.</p>	<p>observations suggest the northern bracing was not installed. This Quantitative Assessment did not include the northern bracing.</p> <p>The south elevation structures of both the Tyre Bay and Plant Maintenance Workshop have been considered as a single continuous lateral load resisting system for longitudinal loading including precast panels, RHS door header and channel eaves members.</p>
Foundation system	Reinforced concrete slab with concrete pads and tie beams.	
Stair system	Timber stairs up to Fleet Services office.	
Other notable features	None	
External works		
Construction information	Structural drawings by City Engineer's Department and Architectural drawings by City Architectural Division both dated 1979.	
Likely design standard	NZS 4203:1976	Inferred from age of building
Heritage status	No heritage status	
Other	Masonry block walls in oxygen storage area	

4.2 Structural 'Hot-spots'

Areas in which damage may be expected to occur from earthquake shaking are outlined below;

- n Cracking of the office concrete frames.
- n Cracking of the precast panels.
- n Damage to the roof diaphragm between the portal frame structures and the concrete frame office area due to the different behaviour of the different structures.
- n Damage at panel connections and panel interfaces.

5 Site Investigations

5.1 Previous Assessments

It is understood that Opus International Consultants undertook rapid assessments of the buildings on the Milton St Depot site. These reports were not available for review.

Visual inspections as part of the Level 4 assessment were undertaken on 8 February 2012. A qualitative report was issued to CCC on 4 September 2012.

5.2 Level 5 Intrusive Investigations

Intrusive Investigations were carried out on the roof structure on 9 October 2012 to confirm the presence of a plywood roof diaphragm.

6 Damage Assessment

6.1 Damage Summary

The table below provides a summary of damage that we observed on our inspection visit. Refer to Appendix A for photographs of the observed damage. The damage described in this report is for the Plant Maintenance Workshop only.

Table 6.1: Damage Summary

Damage type	Unknown	Minor	Moderate	Major	Comment
settlement of foundations	ü				None observed during visual inspection. Level survey may be required to confirm.
tilt of building	ü				None observed during visual inspection. Verticality survey may be required to confirm.
liquefaction		ü			None observed during visual inspection. Contacts on site stated it had occurred in areas throughout the site. The aerial reconnaissance on 24 Feb 2011 indicates the extent was minor.
settlement of external ground					None observed during visual inspection.
lateral spread / ground cracks					None observed during visual inspection.
Frame		ü			Minor cracking of column concrete encasement was observed.
concrete walls		ü			Minor cracking of the concrete shear walls was observed. Minor separation along movement joints between concrete panels was observed.
cracking to concrete floors		ü			Cracks in floor slabs were observed.
Bracing	ü				No damage to the vertical steel cross bracing was observed.

Damage type	Unknown	Minor	Moderate	Major	Comment
					Only a small area of the roof diaphragm was able to be inspected during the intrusive investigation. No damage to this area was observed.
Precast flooring seating	ü				Ceiling lining prevented visual inspection of precast floor seating (mezzanine level of office structure). Drawings indicate 55mm seating which is in accordance with NZS 3101:2006
Stairs					No damage observed during visual inspection
cladding /envelope		ü			Cracking to precast concrete wall panels observed as described above
Internal fit out		ü			Minor plasterboard cracking observed.
building services	ü				No inspection of services. No obvious damage was observed.
Adjacent building					The Plant Maintenance Workshop and the Tyre Bay have been considered as one building.

6.2 Surrounding Buildings

The Tyre Bay (BU 1141-011 EQ2) is part of the same structure as the Plant Maintenance Workshop.

6.3 Residual Displacements and General Observations

No evidence of permanent settlement or displacements was observed during our visual inspection, however a global settlement survey may reveal movement that could be described as damage under insurance entitlement.

6.4 Implication of Damage

Based on our visual inspection, the structure appears to have only suffered minor damage and therefore we believe the structural capacity has not materially diminished.

7 Generic Issues

The generic issues referred to in Appendix A of the EAG guideline document have been assessed and are not considered applicable to the Plant Maintenance Workshop.

8 Geotechnical Consideration

No geotechnical information was available for this site. During the inspection, any damage to the surrounding pavement was noted and any affect to the structure was considered.

9 Survey

No level or verticality surveys were carried out as there was no evidence of settlement or displacement observed during the inspection. CCC may wish to undertake a level survey as part of insurance entitlement considerations.

10 Detailed Seismic Capacity Assessment

10.1 Assessment Methodology

The building has had its seismic capacity assessed using the Forced-based Detailed Assessment Procedures in the NZSEE 2006 AISPBE guidelines, based on the drawings and intrusive investigations.

The structure has suffered minor damage. The post-damage capacity is considered to be the same as the original capacity.

The concrete framed structure of the office area was assessed separately to the rest of the structure. The precast concrete panels of the Tyre Bay and Plant Maintenance Workshop, plus associated steel tie members, have been assumed to contribute to the overall longitudinal lateral load resisting system of both structures i.e. they have been considered as one structure when assessing the seismic capacity of the building.

10.2 Assumptions

The following assumptions were used in our quantitative assessment:

- n Reinforcing steel yield strength $f_y = 275$ MPa (as noted on the drawings)
- n Concrete compressive strength $f_c' = 25$ MPa (as noted on the drawings)
- n Structural steel yield strength $f_y = 250$ MPa
- n Soil ultimate bearing strength $q_u = 300$ kPa

10.3 Critical Structural Weaknesses

The following Critical Structural Weakness has been identified:

- n Site characteristics due to liquefaction occurring on the Milton St site

The site characteristics have been identified as a potential CSW in our earlier qualitative report. We note that liquefaction is still considered a potential CSW however has not been considered in this quantitative assessment as we believe it will not have a direct impact on the structure's ability to resist further loads or cause global failure of the structure.

10.4 Seismic Parameters

The seismic design parameters based on current design requirements from NZS 1170.5:2004 and the NZBC clause B1 for this building are:

- n Site soil class: D – NZS 1170.5:2004, Clause 3.1.3, Soft Soil
- n Site hazard factor, $Z = 0.3$ – NZBC, Clause B1 Structure, Amendment 11 effective from 19 May 2011
- n Return period factor $R_u = 1$ – NZS 1170.5:2004, Table 3.5, Importance Level 2 structure with a 50 year design life.
- n Near fault factor $N(T,D) = 1$ – NZS 1170.5:2004, Clause 3.1.6, Distance more than 20 km from fault line.

10.5 Results of Seismic Assessment

The results of our quantitative assessment indicate the building has a seismic capacity in the order of 35%NBS. This is similar to the IEP assessment of 36%NBS in the previous Qualitative Report. Table 10.1 presents the evaluated seismic capacity in terms of %NBS of the individual structural systems in each building direction.

Table 10.1: Summary of Seismic Assessment of Structural Systems

Item	Loading Direction	Ductility, μ	Seismic Capacity	Notes
Overall %NBS adopted from DEE	Longitudinal		35%NBS	Governed by precast shear wall overturning.
Portal frames	Transverse	1.25	>100%NBS	
Precast panel, in-plane capacity	Longitudinal	1.25	>100%NBS	
Foundations	Longitudinal	1.25	35%NBS	Resistance to overturning of precast panels. Based on combined Tyre Bay and Plant Maintenance Workshop longitudinal load resisting system adopted.
Precast panel, out-of-plane flexural capacity	Both	3	92%NBS	Precast panels have been analysed as a part.
Precast panel connections	Longitudinal	1.25	46%NBS	Shear capacity under In-plane loading.
RHS door header beam	Longitudinal	1.25	36%NBS	Pull out of connection to the precast panels.
Channel eaves beam	Longitudinal	1.0	38%NBS	Shear capacity of connection to precast panels.
Mezzanine office reinforced concrete frames	Transverse	3	85%NBS	Capacity governed by columns (flexure).
Mezzanine office reinforced concrete frames	Longitudinal	3	70%NBS	Capacity governed by beams (flexure).

Note: Ductility factors are in accordance with values recommended in the NZSEE 2006 AISPBE guidelines.

10.6 Discussion of results

The key findings of the assessment are as follows:

- n Overturning capacity of the precast shear walls and foundation achieves 35%NBS under longitudinal (in-plane) loading.
- n RHS door header (tie member) connections under longitudinal (in-plane) loading achieve 36%NBS.
- n Eaves channel (tie member) connections under longitudinal (in-plane) loading achieve 38%NBS.
- n Precast panel connections to the portal frames achieve 46%NBS under longitudinal (in-plane) loading.

Based on the results of our Quantitative Assessment, the Plant Maintenance Workshop is considered Earthquake Risk and Seismic Grade C as the seismic capacity was assessed to be between 34%NBS and 67%NBS.

11 Recommendations

11.1 Occupancy

In order that the owner can make an informed decision about the on-going use and occupancy of their building the following information is presented in line with the Department of Building and Housing document 'Guidance for engineers assessing the seismic performance of non-residential and multi-unit residential buildings in greater Christchurch', June 2012.

The building is considered to be earthquake risk, having an assessed capacity of between 34% and 67%NBS. The risk of collapse of an earthquake risk building is considered to be 5 to 10 times greater than that of an equivalent new building.

No significant damage or hazards were identified to the seismic or gravity load resisting system that would reduce its ability to resist further loads and therefore no restrictions on use or occupancy are recommended.

11.2 Further Investigations, Survey or Geotechnical Work

A settlement survey could be carried out to determine the extent of settlement of the building for insurance purposes.

11.3 Damage Reinstatement

According to the recent CCC Instructions to Engineers document (16 October 2012), Council's insurance provides for repairing damaged elements to a condition substantially as new. We suggest you consult further with your insurance advisor.

12 Design Features Report

Repairs will be required to reinstate the existing structural system. A repair methodology has not been prepared at this stage. No new load paths are expected as a result of the repairs required.

13 Limitations

The following limitations apply to this engagement:

- n Beca and its employees and agents are not able to give any warranty or guarantee that all defects, damage, conditions or qualities have been identified.
- n Inspections are primarily limited to visible structural components. Appropriate locations for invasive inspection, if required, will be based on damage patterns observed in visible elements, and review of the construction drawings and structural system. As such, there will be concealed structural elements that will not be directly inspected.
- n The inspections are limited to building structural components only.
- n Inspection of building services, pipework, pavement, and fire safety systems is excluded from the scope of this report.
- n Inspection of the glazing system, linings, carpets, claddings, finishes, suspended ceilings, partitions, tenant fit-out, or the general water tightness envelope is excluded from the scope of this report.
- n The assessment of the lateral load capacity of the building is limited by the completeness and accuracy of the drawings provided. Assumptions have been made in respect of the geotechnical conditions at the site and any aspects or material properties not clear on the drawings. Where these assumptions are considered material to the outcome further investigations may be recommended. It is noted the assessment has not been exhaustive, our analysis and calculations have focused on representative areas only to determine the level of provision made. At this stage we have not undertaken any checks of the gravity system, wind load capacity, or foundations.
- n The information in this report provides a snapshot of building damage at the time the detailed inspection was carried out. Additional inspections required as a result of significant aftershocks are outside the scope of this work.

This report is of defined scope and is for reliance by CCC only, and only for this commission. Beca should be consulted where any question regarding the interpretation or completeness of our inspection or reporting arises.

Appendix A

Photographs



Figure 1A: Site Layout (North is to the left of page)



Photo 1: External view of Plant Maintenance Workshop



Photo 2: External view of Plant Maintenance Workshop



Photo 3: External view of Plant Maintenance Workshop



Photo 4: Internal view of Plant Maintenance Workshop.

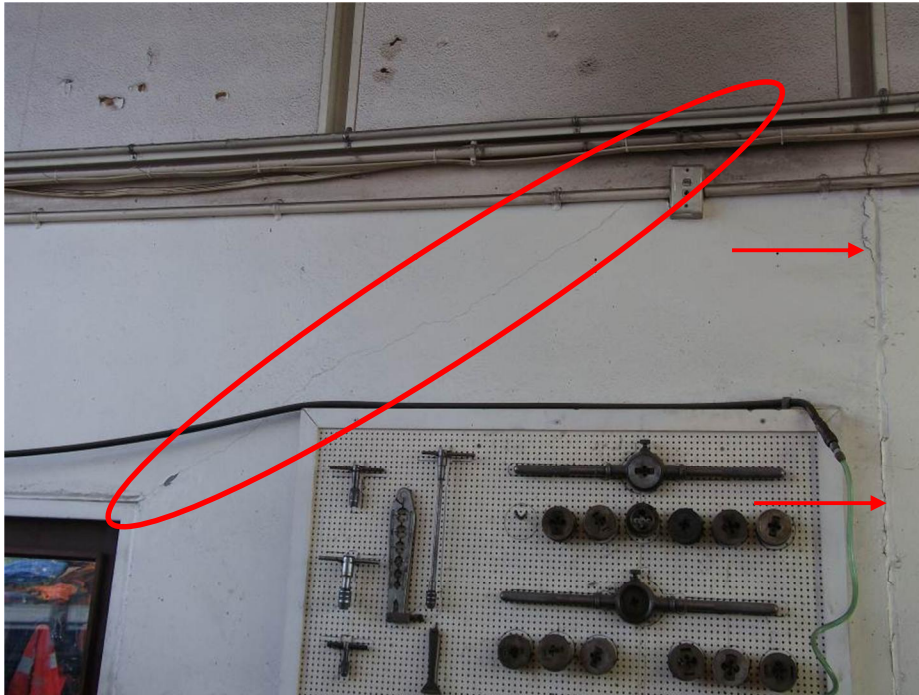


Photo 5: Typical cracking to concrete shear walls.

Description of Damage: Cracking to concrete shear walls and movement joints, with some spalling at movement joint.



Photo 6: Typical slab cracking

Description of Damage: Cracking to concrete slab at Fleet Services entrance.



Photo 7: Movement between concrete wall and timber wall.

Description of Damage: Damage from movement between concrete wall and timber wall.



Photo 8: Typical cracking to concrete encasement of column.

Description of Damage: Cracking to column concrete encasement.



Photo 9: Typical cracking to concrete shear walls at corners of building.

Description of Damage: Cracking to concrete shear walls.



Photo 10: Typical cracking to concrete shear walls at corners of building

Description of Damage: Shear crack in concrete shear wall.



Photo 11: Typical cracking along movement joints

Description of Damage: Cracking to vertical movement joints.



Photo 12: Typical slab cracking

Description of Damage: Cracking to concrete slab.

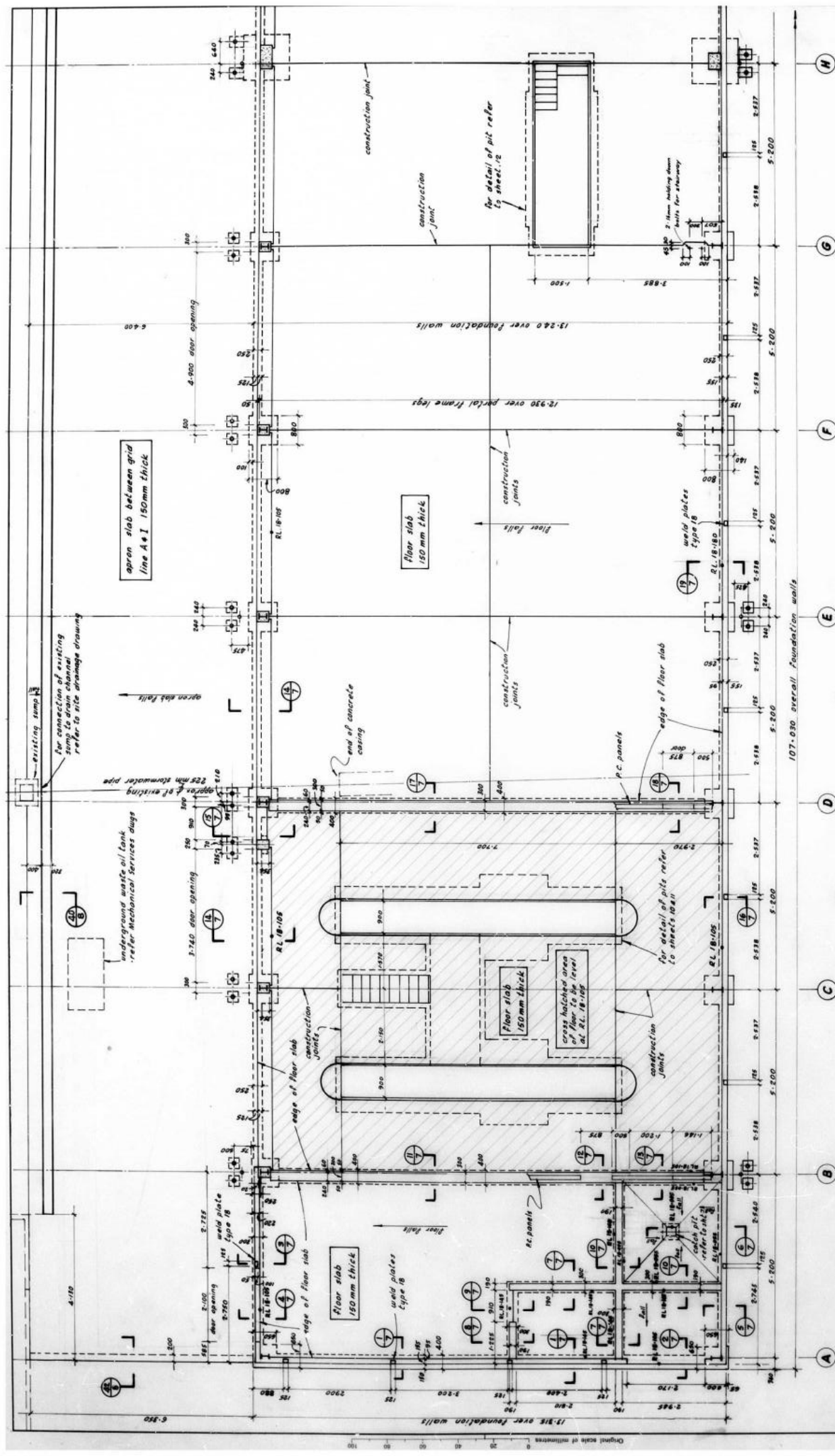


Photo 13: Cracking to oxygen tank storage blockwork

Description of Damage: Cracking to blockwork mortar.

Appendix B

Existing Drawings



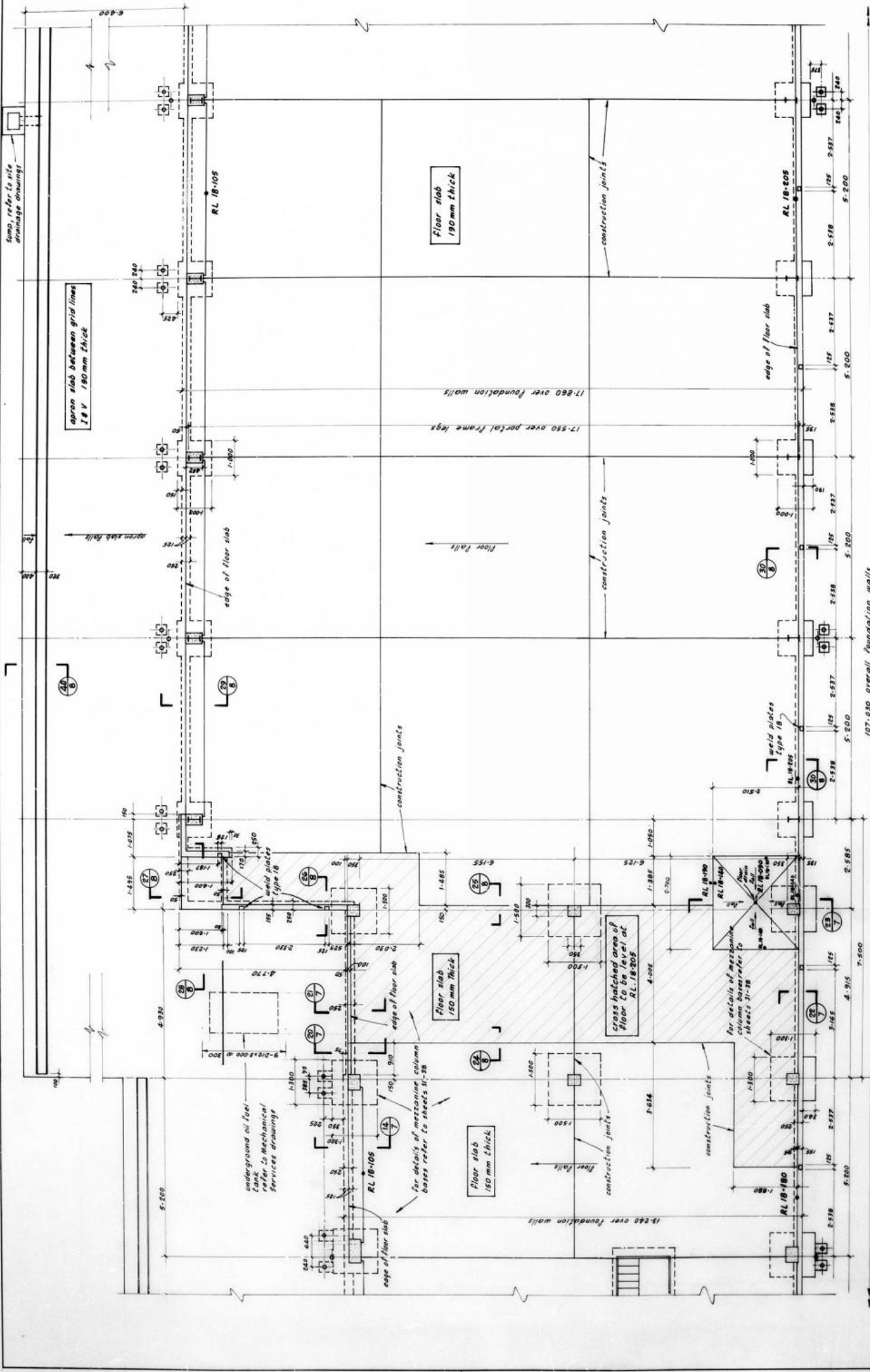
DETAILS OF CONSTRUCTION JOINTS
Scale 1:10

CHRISTCHURCH CITY COUNCIL — CITY ENGINEER'S DEPARTMENT NEW CENTRAL DEPOT — PLANT MAINTENANCE — STAGE 2 — JOHNSON ST — PART FOUNDATION PLAN — GRID LINES A-H —		Date: 10/19/10 Scale: 1:50 1:10	D.2278
Drawn: A. Shawcross Checked: P. R. 2/10/10 Date: 10/19/10	Design: A. Shawcross Checked: P. R. 2/10/10 Date: 10/19/10	Engineer: A. Shawcross Checked: P. R. 2/10/10 Date: 10/19/10	Project: 10/19/10 Sheet: 1 of 1

Notes: Refer to sheet 8

centimetres

0 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290 300



Notes Refer to sheet 8

Notes Refer to sheet 8

Sheet 2 of 43

D.2278

1:50

CHRISTCHURCH CITY COUNCIL — CITY ENGINEER'S DEPARTMENT

NEW CENTRAL DEPOT — PLANT MAINTENANCE — STAGE 2 — JOHNSON ST —

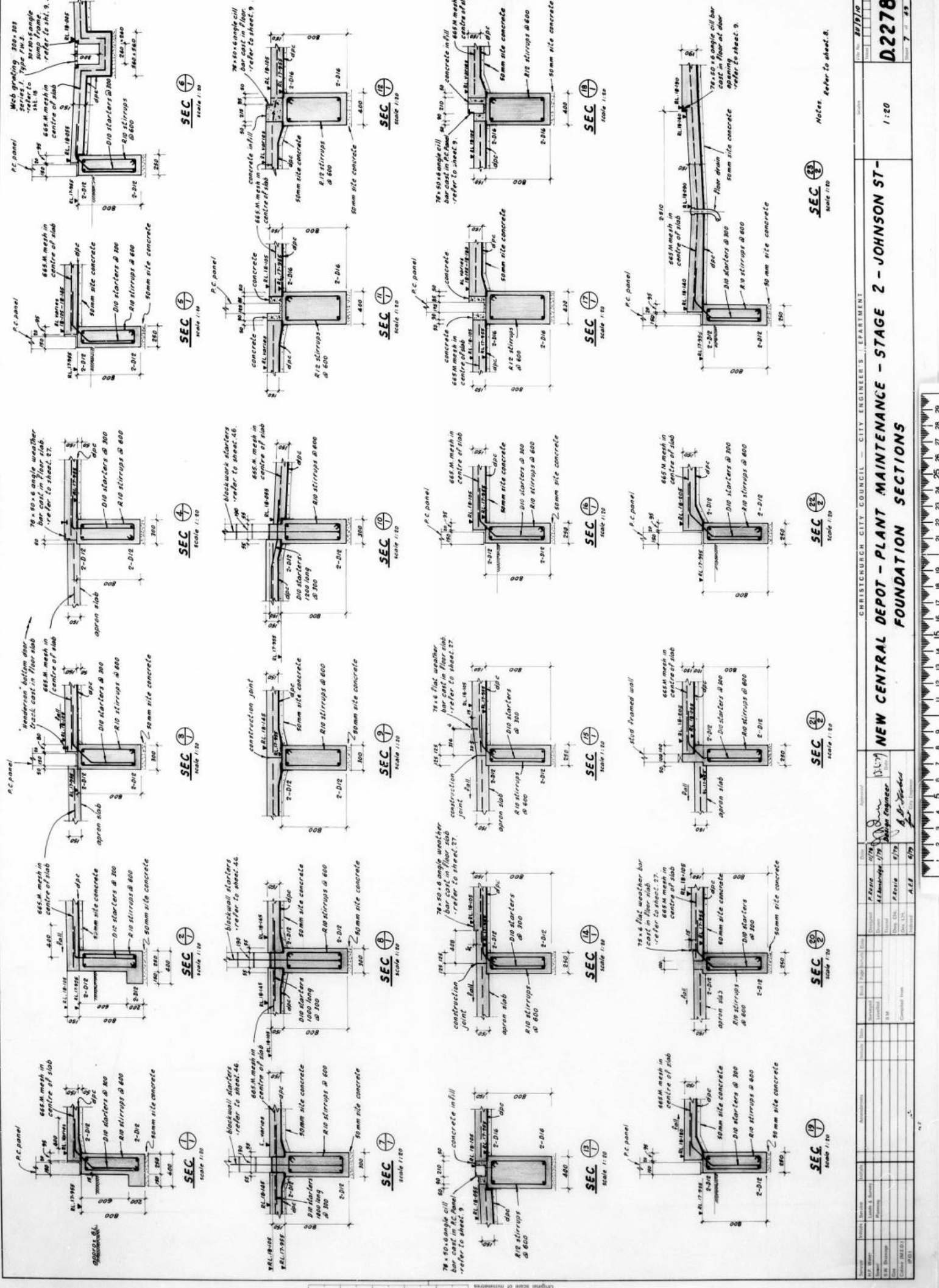
PART FOUNDATION PLAN — GRID LINES H — O —

Authorised		Checked		Reviewed		Approved		Date	
For	By	For	By	For	By	For	By	For	By
Authorised	For	Checked	For	Reviewed	For	Approved	For	For	By
City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12
City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12
City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12	City Engineer	12/12

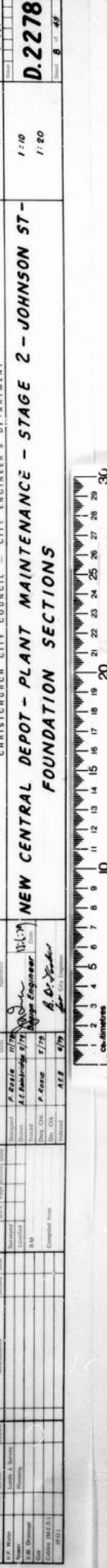
Original scale of millimetres

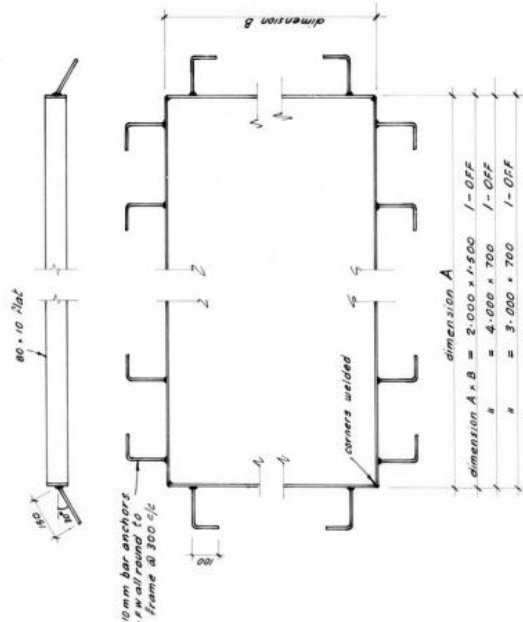
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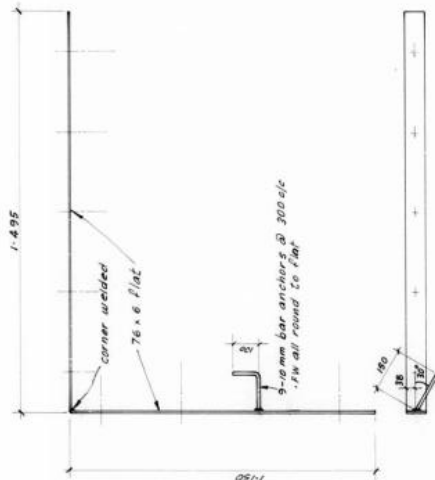


CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT										NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST-1										FOUNDATION SECTIONS										D.2278										1:20										Notes Refer to sheet 8.										Scale 1:20										SEC 19										SEC 18										SEC 17										SEC 16										SEC 15										SEC 14										SEC 13										SEC 12										SEC 11										SEC 10										SEC 9										SEC 8										SEC 7										SEC 6										SEC 5										SEC 4										SEC 3										SEC 2										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1										SEC 1			
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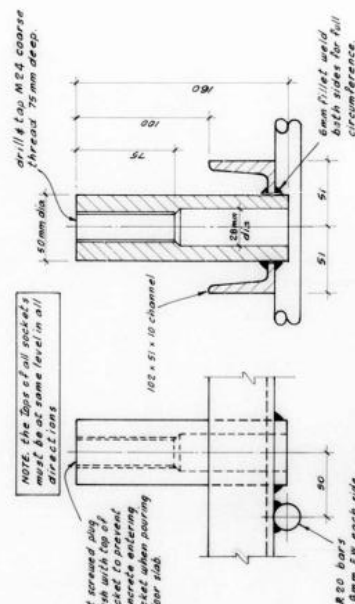


FRAMES FOR HARDWOOD FLOOR INSETS



PORCH EDGING 1-0FF

• hot dip galvanise after fabrication
scale 1:10

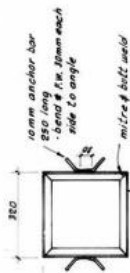


DETAIL OF SOCKETS

84 - OFF

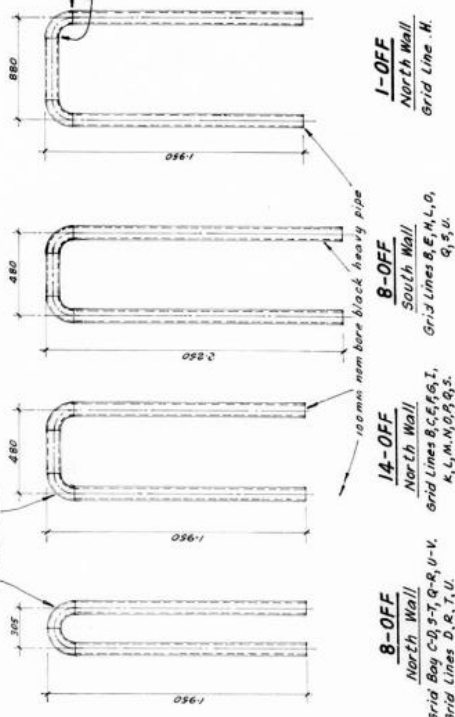


0111 1/233
hot dip galvanise after fabrication



SUMP GRATING FRAME

1-OFF
hot dip galvanise after

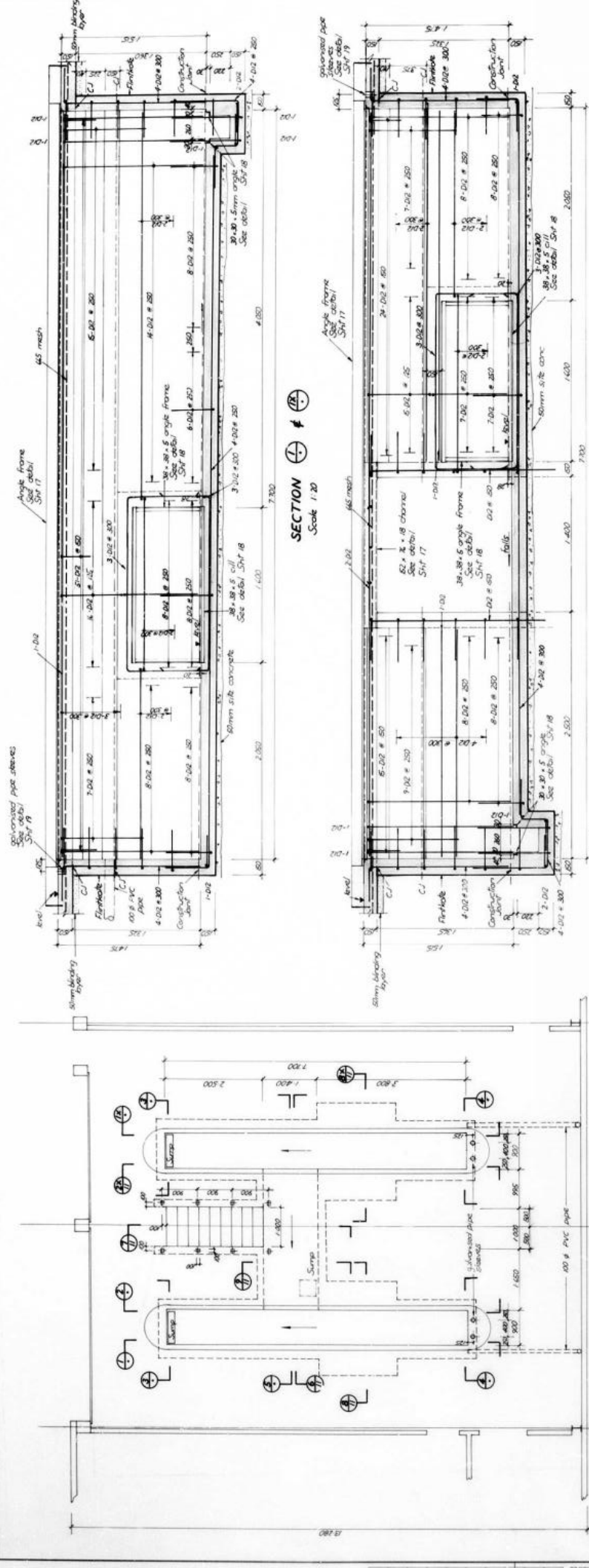


DETAILS OF BOLLARDS

hot dip galvanise after fabrication

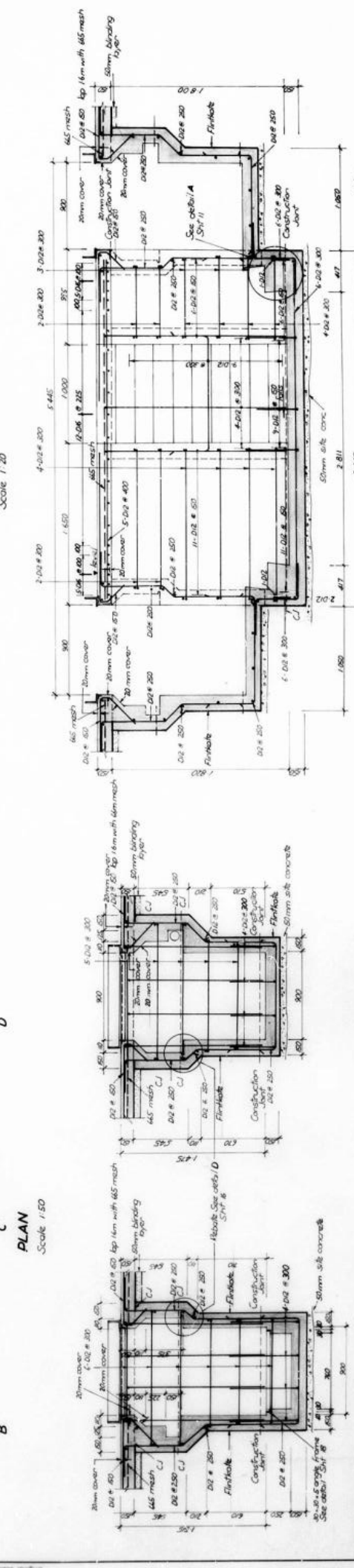
Notes. Refer to notes on sheet. 21.

[illegible]



SECTION 1
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SECTION 2
Scale 1:20



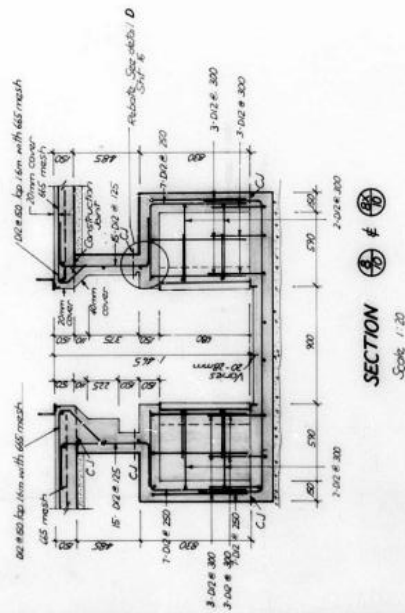
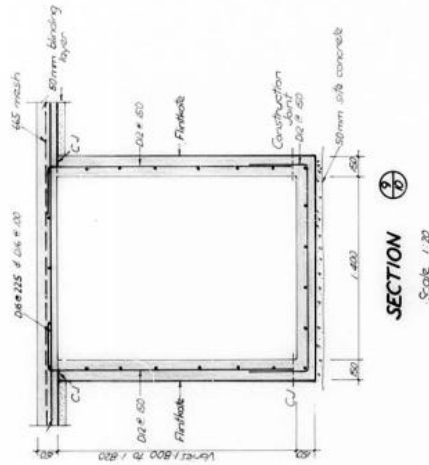
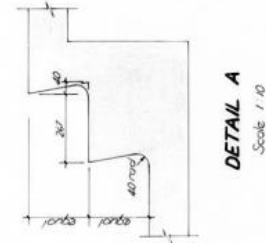
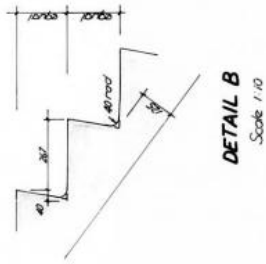
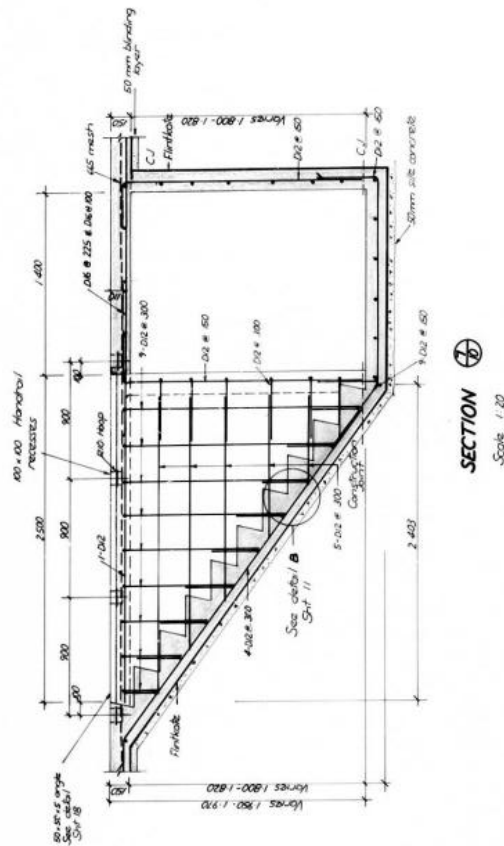
SECTION 1
Scale 1:20

SECTION 2
Scale 1:20

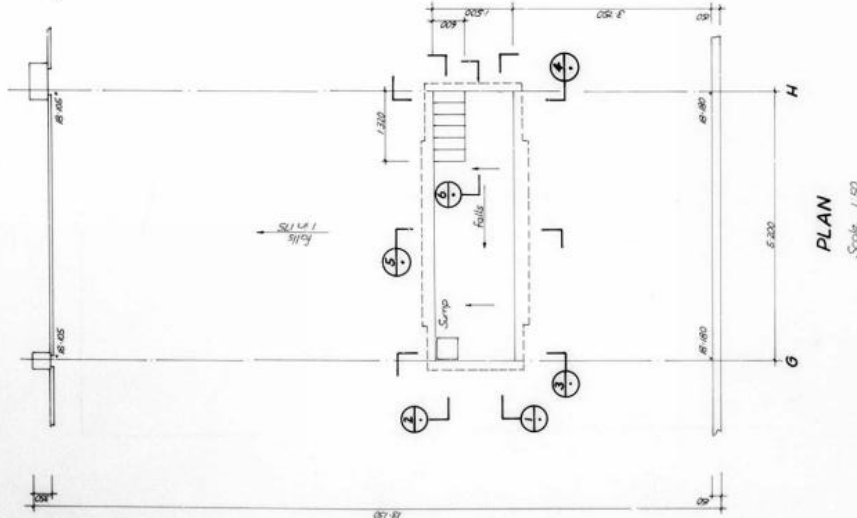
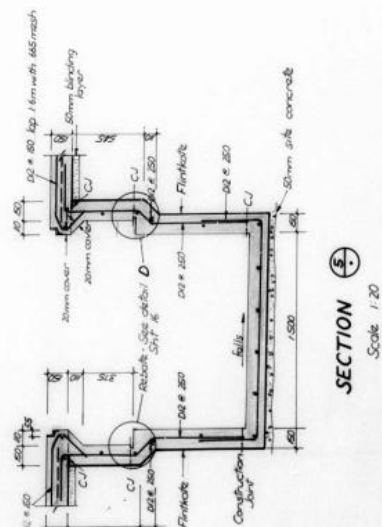
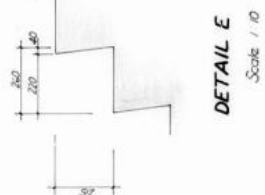
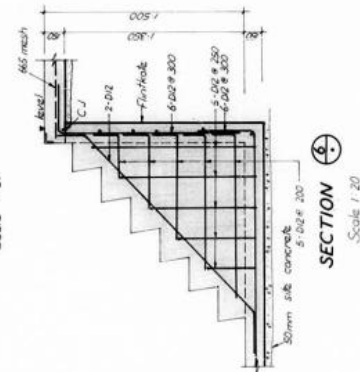
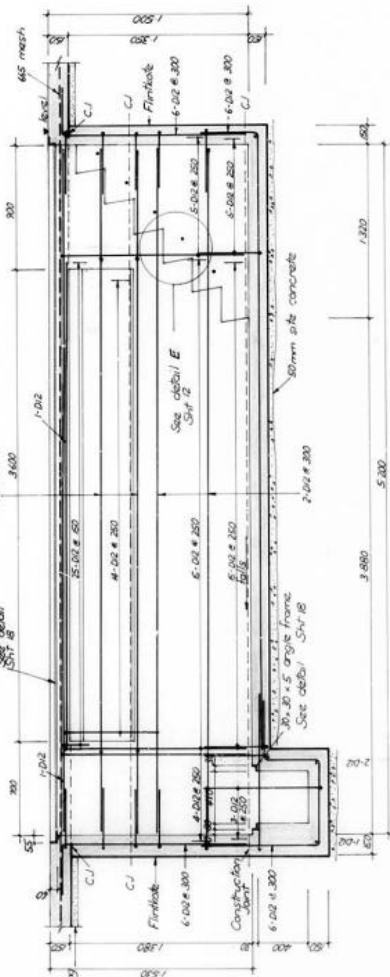
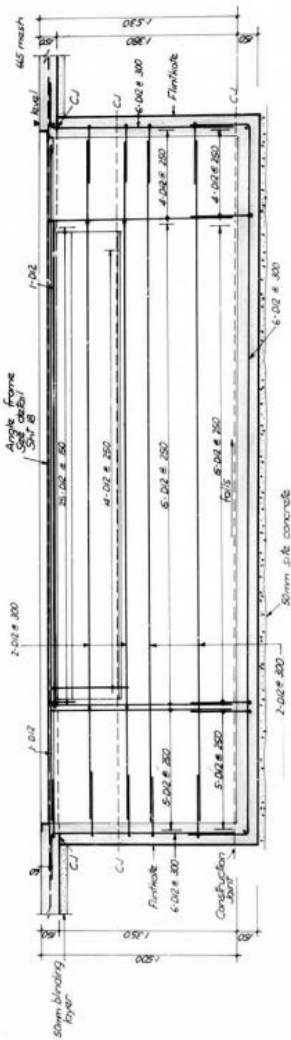
Score 1/20

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Service	Materials	Recurrent	Inspection	Investigate	Design	Draw	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	Detail	De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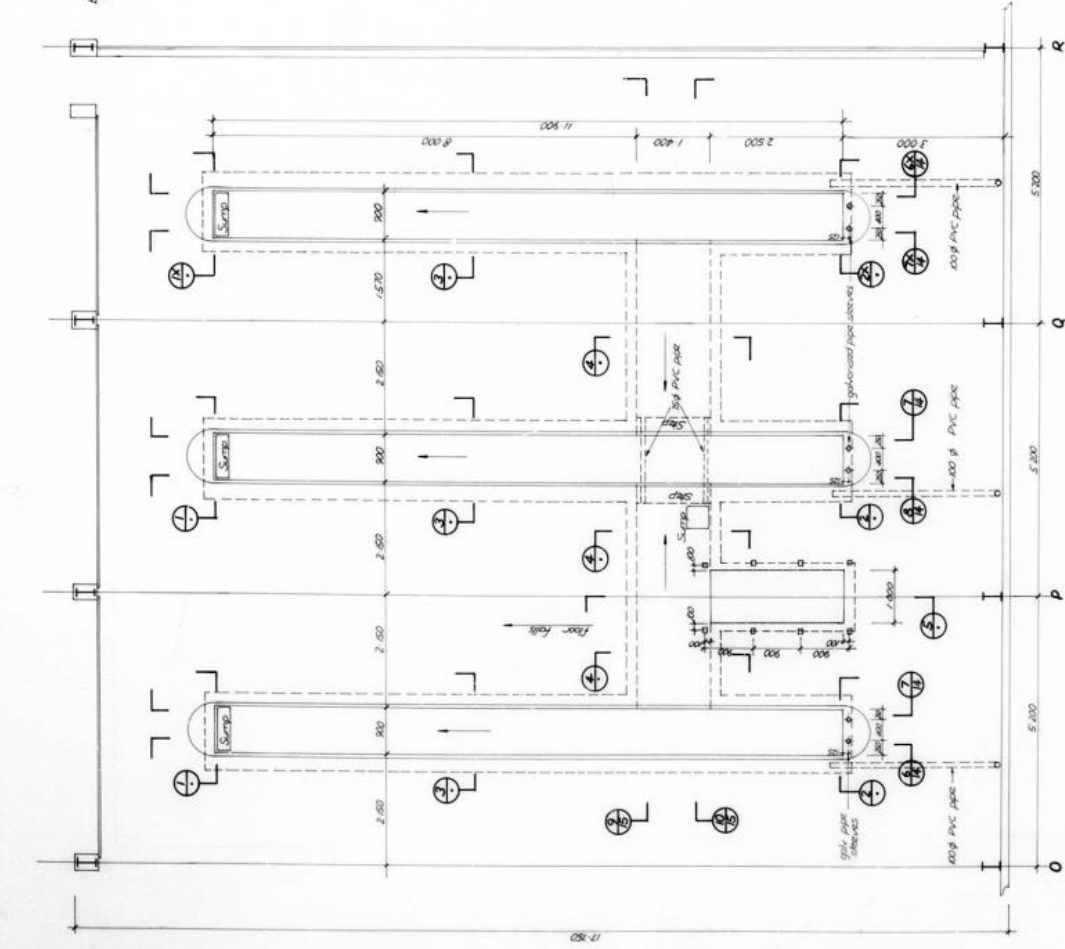


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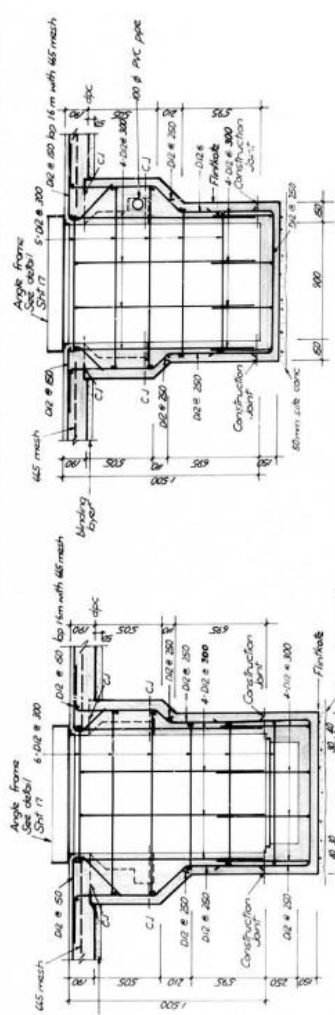


Notes

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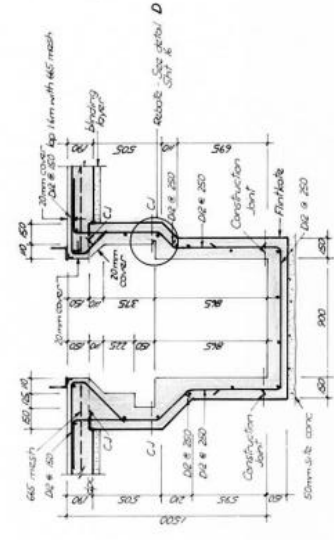


PLAN
Scale 1/50

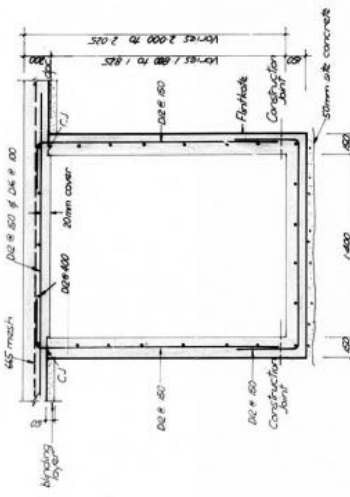


SECTION 1
Scale 1/20

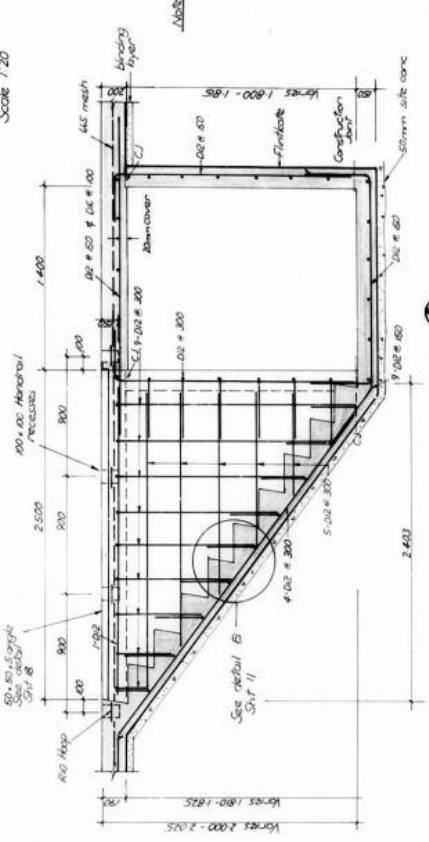
SECTION 2
Scale 1/20



SECTION 3
Scale 1/20



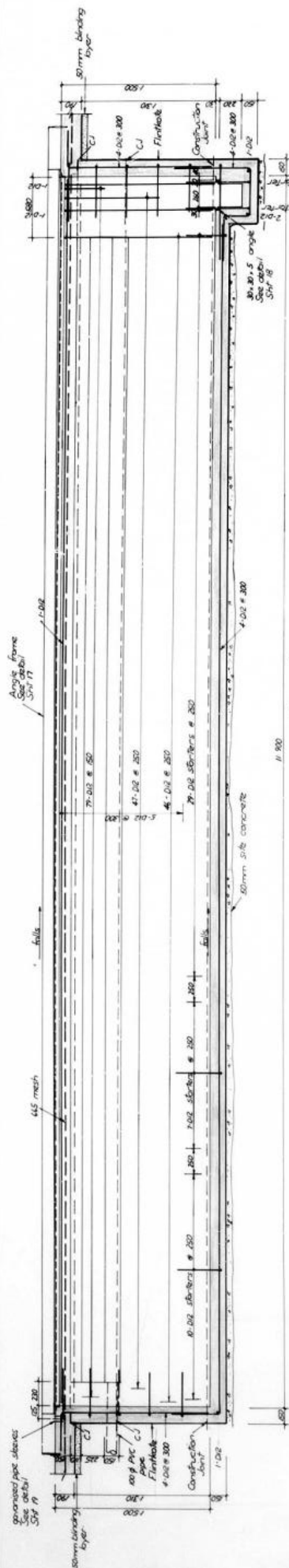
SECTION 4
Scale 1/20



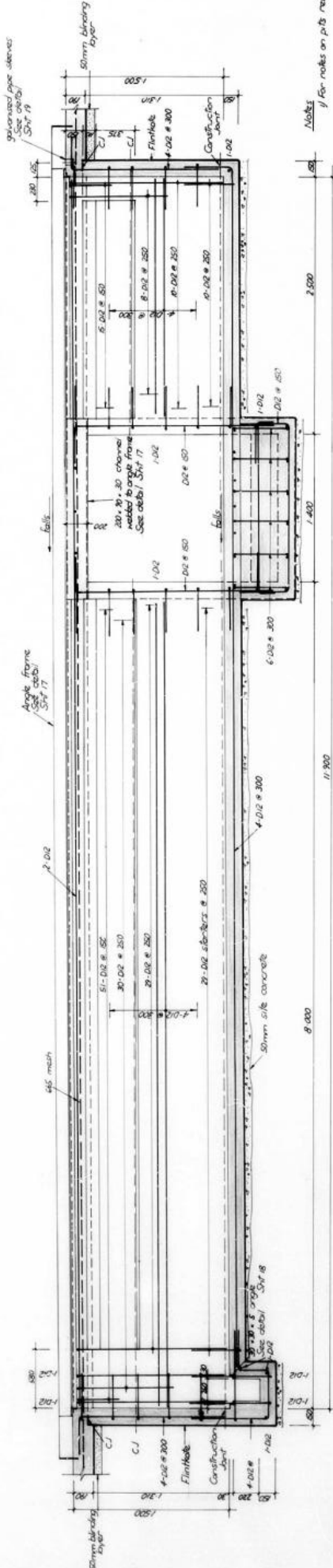
SECTION 5
Scale 1/20

CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT									
NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST									
PITS-HEAVY MAINTENANCE WORKSHOP									
Drawn	Checked	Reviewed	Approved	Scale	Sheet	D2278			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			
1/19	2/19	2/19	2/19	1/20	1/50	1/20			

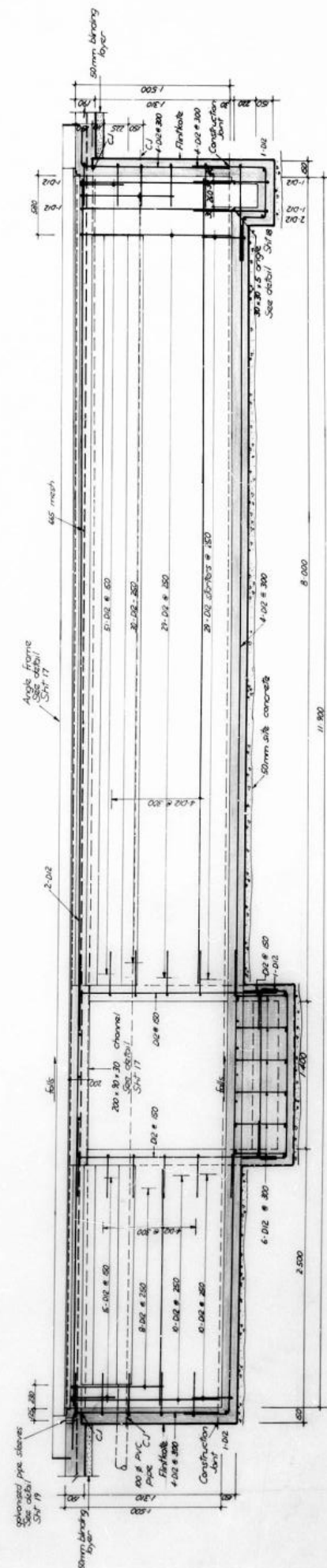




SECTION 1
Scale 1:20

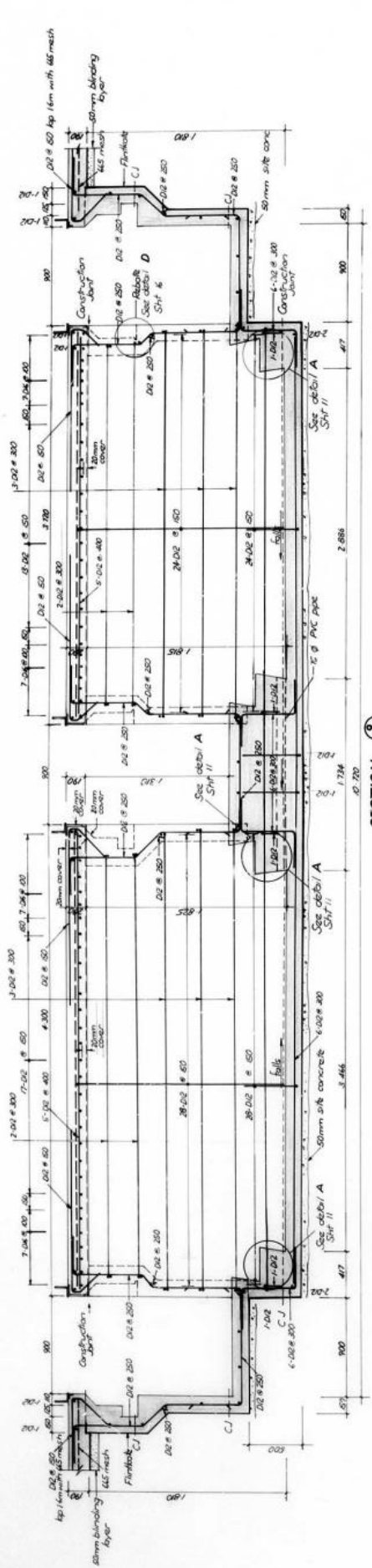


SECTION 2
Scale 1:20

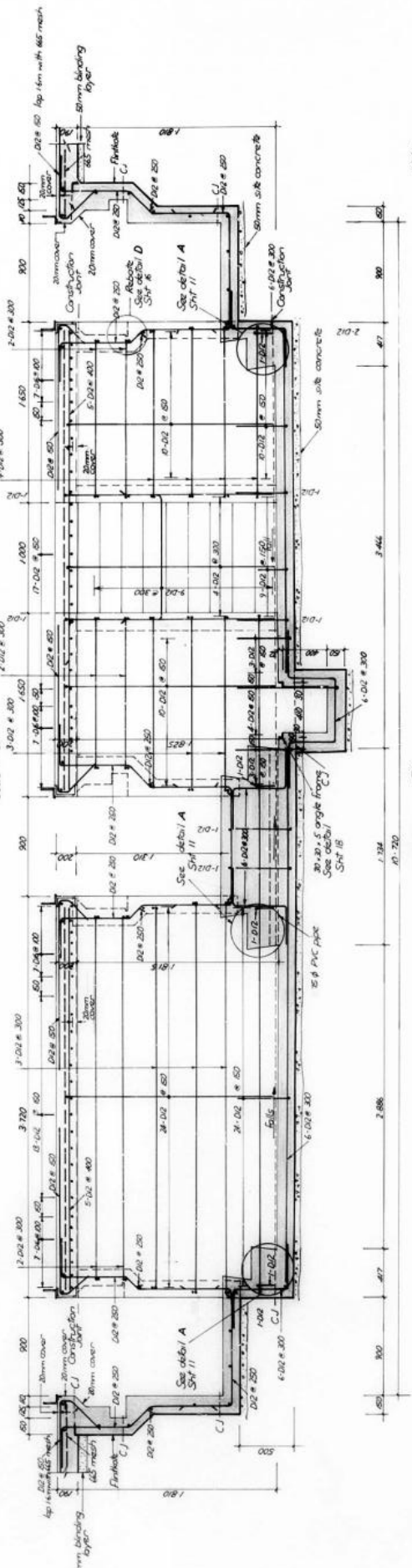


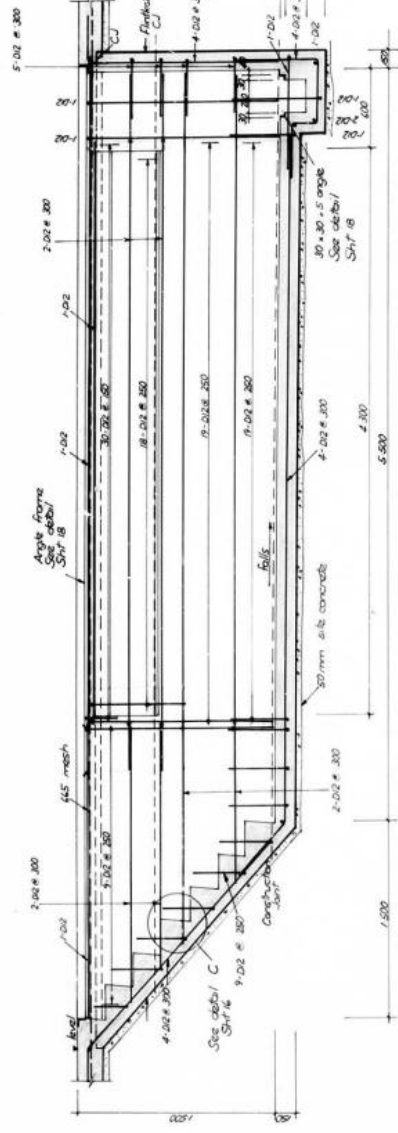
SECTION 3
Scale 1:20

SHEET NO. 81/1910 PROJECT NO. D2278	
DATE 1/20	
PROJECT NAME NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST	
PROJECT LOCATION PITS - HEAVY MAINTENANCE WORKSHOP	
CITY CHRISTCHURCH	
DEPARTMENT CITY ENGINEER'S DEPARTMENT	
DRAWN BY [Signature]	
CHECKED BY [Signature]	
APPROVED BY [Signature]	
TITLE SECTION 1	
SCALE 1:20	
MATERIALS	
REINFORCEMENT	CONCRETE
BARS	GRADE
DIA.	LENGTH
NO.	VOLUME
WEIGHT	COST
TOTAL	TOTAL

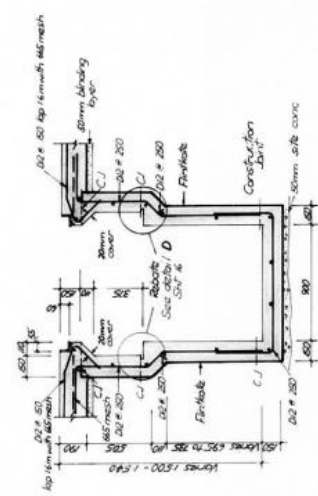


SECTION 1
Scale 1/20

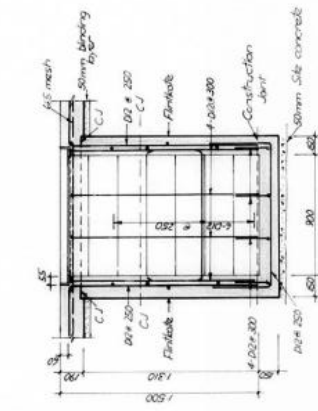




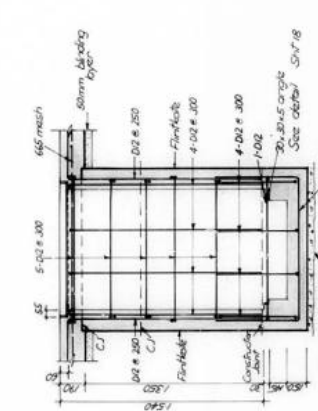
SECTION 1
Scale 1/20



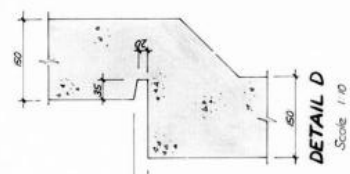
SECTION 2
Scale 1/20



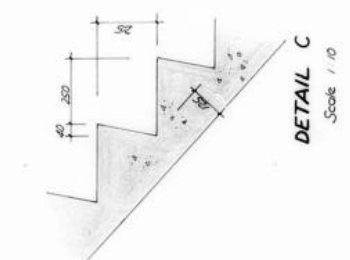
SECTION 3
Scale 1/20



SECTION 4
Scale 1/20



DETAIL D
Scale 1/10



DETAIL C
Scale 1/10

NOTES FOR PITS

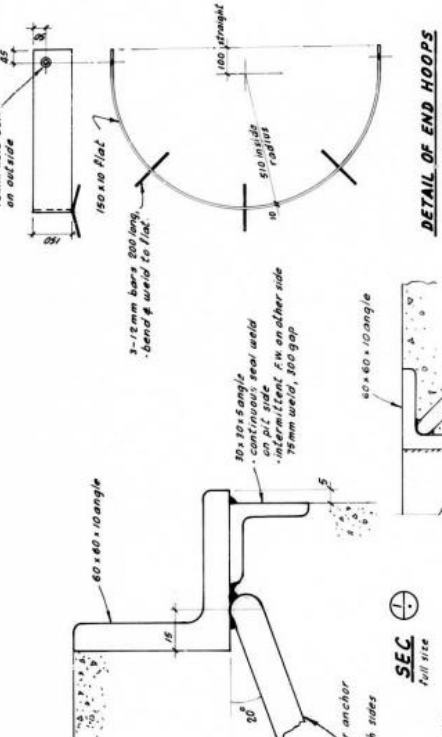
- Concrete Strength $f_c = 25 \text{ MPa}$
- Reinforcing (a) All bars to be deformed Grade 235 (b) Reinforcing to be continuous throughout (c) Cover - All reinforcing to be in centre of walls & floor slabs except where shown otherwise
- Reinforcing (a) All bars to be deformed Grade 235 (b) Reinforcing to be continuous throughout (c) Cover - All reinforcing to be in centre of walls & floor slabs except where shown otherwise
- Reinforcing (a) All bars to be deformed Grade 235 (b) Reinforcing to be continuous throughout (c) Cover - All reinforcing to be in centre of walls & floor slabs except where shown otherwise
- Reinforcing (a) All bars to be deformed Grade 235 (b) Reinforcing to be continuous throughout (c) Cover - All reinforcing to be in centre of walls & floor slabs except where shown otherwise

All pits shall be fully lined with Flathole and floorless according to the Specification

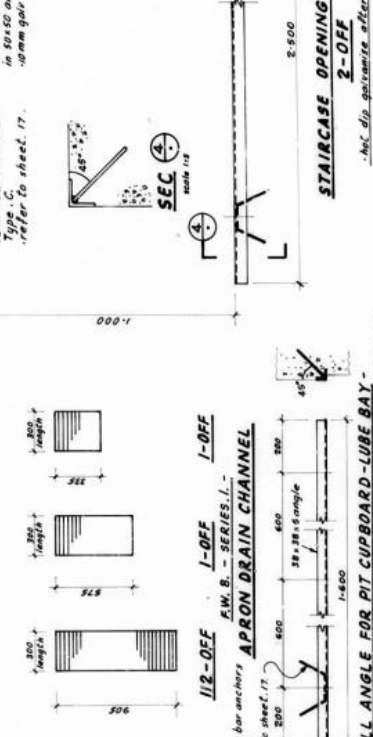
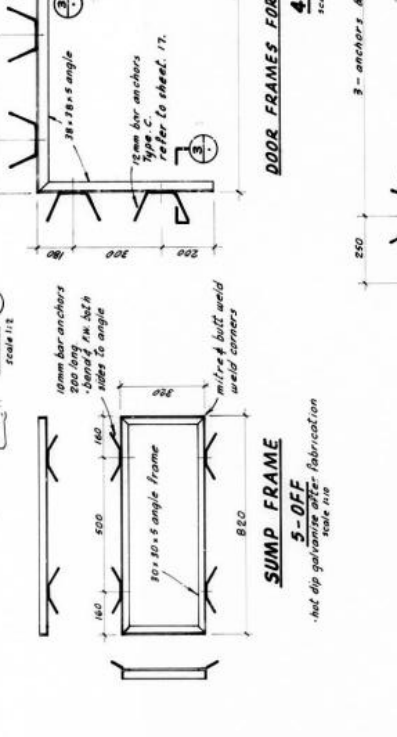
CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT									
Project No.	2018/10	Drawn	15/17	Checked	15/17	Scale	1/10	1/20	1/50
NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST									
PITS - FITTING AND TURNING WORKSHOP									
Author	15/17	Design Engineer	15/17	Scale	1/10	1/20	1/50	D2278	
Project No.	2018/10	Drawn	15/17	Checked	15/17	Scale	1/10	1/20	1/50





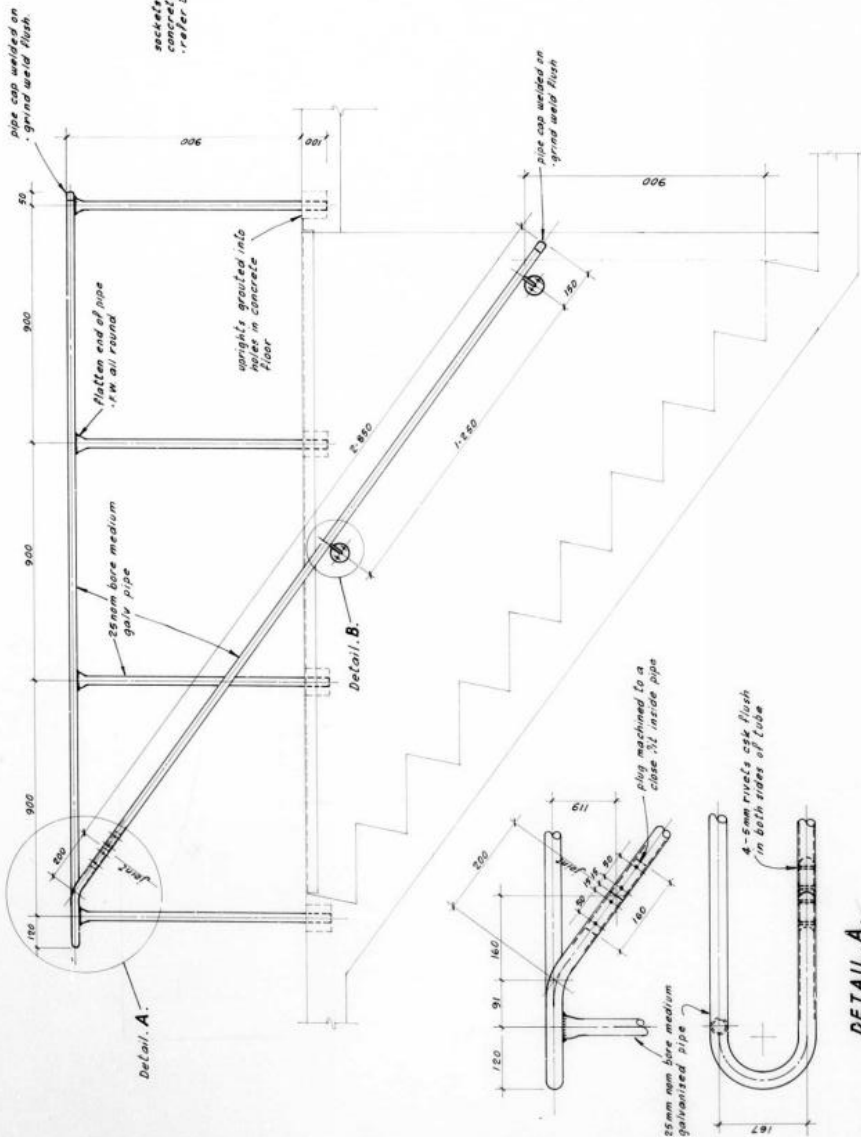


epistadoun wa plam / ees



FF
SERIES. I. -
STORE

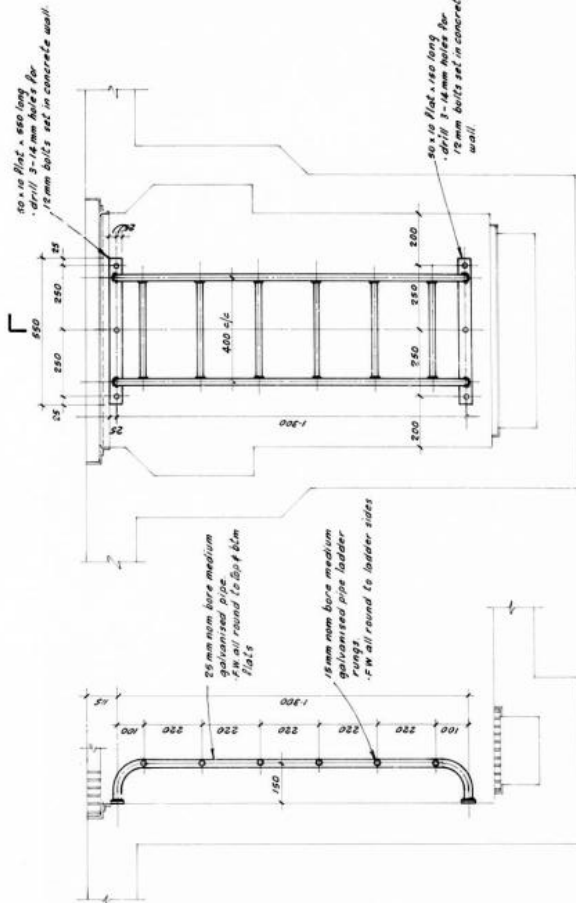
NEW CENTRA
DETAILS OFNEW CENTRA
DETAILS OF



SEC 7

DETAILS OF LADDER FOR LUBE BAY & HEAVY MAINTENANCE WKSP PITS

scale 100

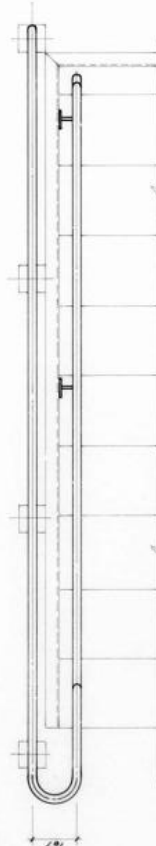


SEC 2

DETAILS OF LADDER FOR FITTING & TURNING WKSP PIT

1-OFF

- Notes
1. All welds to be 6mm fillet welds.
 2. All ungalvanised parts to be painted with Dry Galv paint.
All welds & areas of galvanising damaged by welding to be painted with Dry Galv paint.

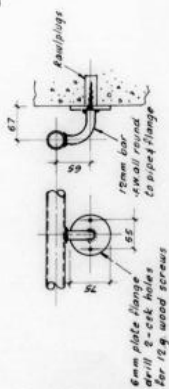


DETAILS OF PIT STAIRCASE HANDRAIL

2-OFF as drawn

2-0FF opposite hand

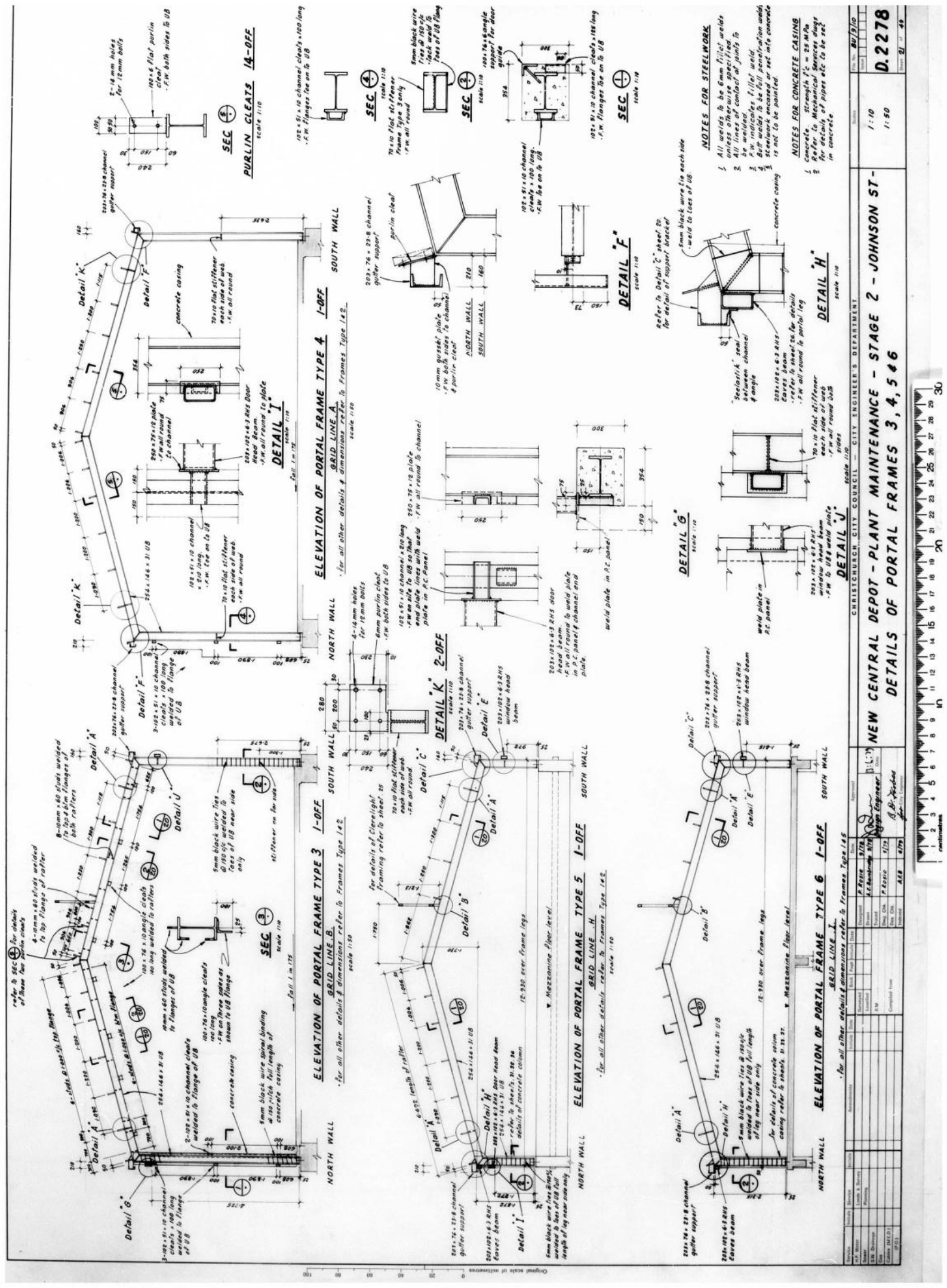
scale 1100

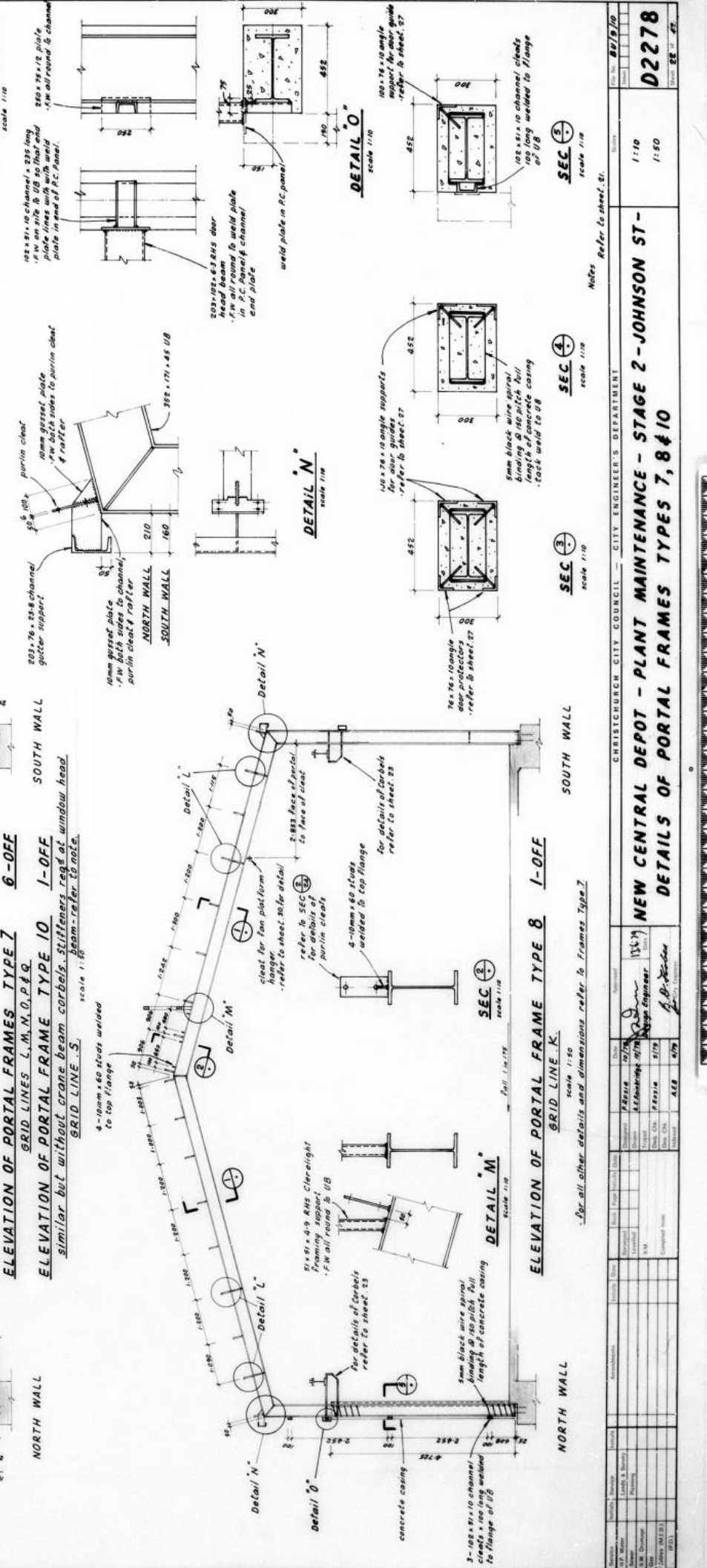
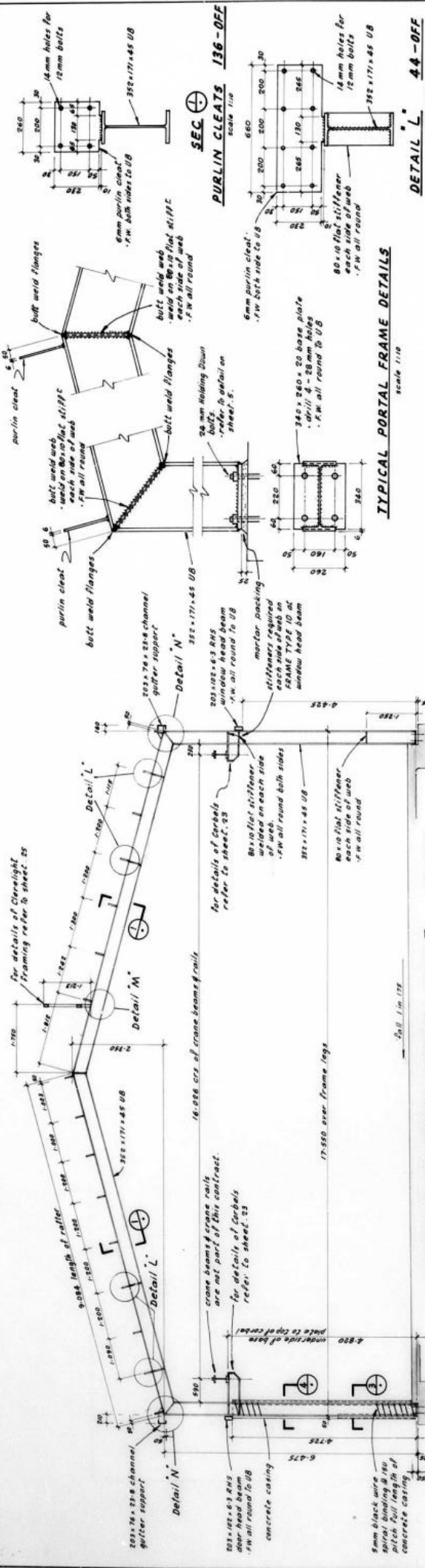


DETAIL: B.

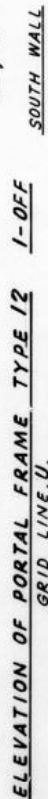
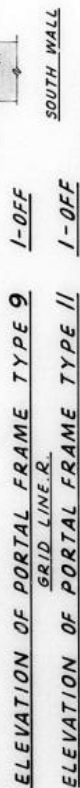
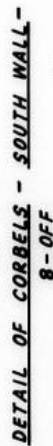
12000 115

[illegible]





CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT									
Drawn	Checked	Reviewed	Approved	Date	Scale	Sheet	Of	Project	Notes
J.P. Walker	L. J. Bailey			10/10	1:10	1	10	NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST -	Refer to sheet 2.
J.P. Walker	L. J. Bailey			10/10	1:10	2	10	DETAILS OF PORTAL FRAMES TYPES 7, 8 & 10	

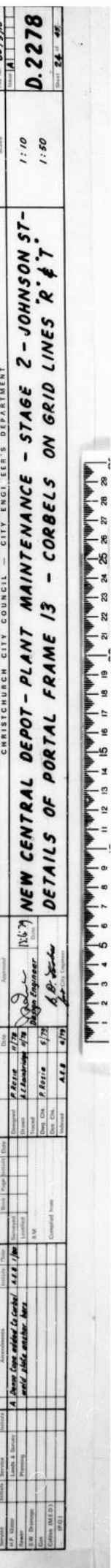


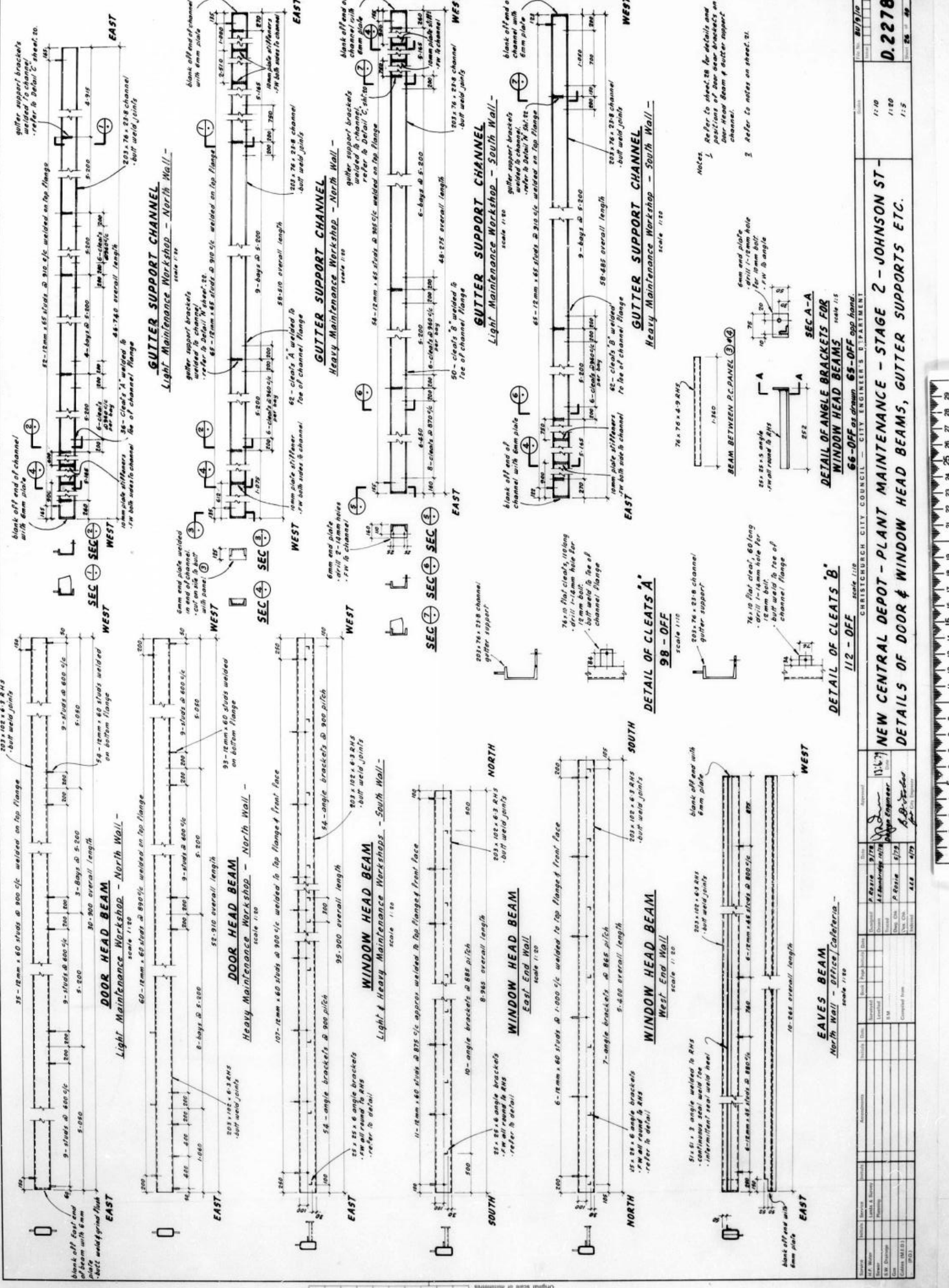
Scale 1:50
For all other details & dimensions refer to Frames Type 7.

Element	Unit	Quantity	Unit Price	Amount	Remarks	Drawings	Design	Check	Approval
1. F.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
2. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
3. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
4. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
5. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
6. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
7. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
8. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
9. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
10. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
11. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
12. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
13. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
14. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
15. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
16. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
17. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
18. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
19. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
20. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
21. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
22. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
23. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
24. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
25. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
26. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
27. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
28. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
29. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
30. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
31. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
32. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
33. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
34. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
35. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
36. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
37. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
38. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
39. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
40. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
41. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
42. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
43. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
44. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
45. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
46. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
47. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
48. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
49. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
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51. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
52. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
53. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
54. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
55. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
56. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
57. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
58. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
59. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
60. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
61. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
62. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
63. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
64. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
65. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
66. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
67. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
68. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
69. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
70. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
71. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
72. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
73. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
74. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
75. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
76. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
77. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
78. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
79. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
80. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
81. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
82. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
83. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
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86. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
87. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
88. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
89. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
90. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
91. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
92. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
93. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
94. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
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96. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
97. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
98. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
99. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100
100. S.W. Work	Sq. Mtr	100	100	10000	100	100	100	100	100

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST -
DETAILS OF PORTAL FRAMES TYPES 9, 11 & 12







- Notes
1. Refer to sheet 20 for details and positions of door head beams on door head beam & gutter support channel.
 2. Refer to notes on sheet 21.

DETAIL OF ANGLE BRACKETS FOR WINDOW HEAD BEAMS
scale 1:5

DETAIL OF CLEATS 'A'
scale 1:5

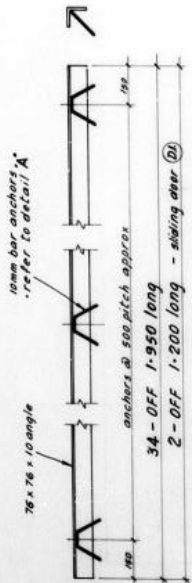
DETAIL OF CLEATS 'B'
scale 1:5

EAVES BEAM
North Wall - Office/Cafeteria -
scale 1:20

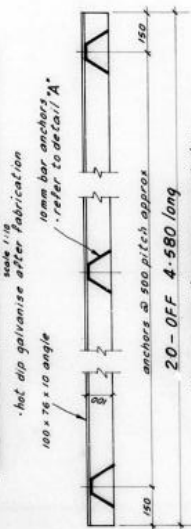
Rev.	By	Date	Checked	Date	Approved
1	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
2	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
3	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
4	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
5	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
6	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
7	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
8	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
9	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown
10	J.P. Brown	2/1/78	J.P. Brown	2/1/78	J.P. Brown

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST -
DETAILS OF DOOR & WINDOW HEAD BEAMS, GUTTER SUPPORTS ETC.

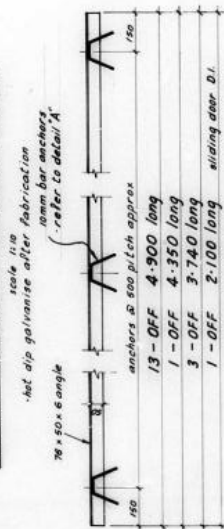
D.2278



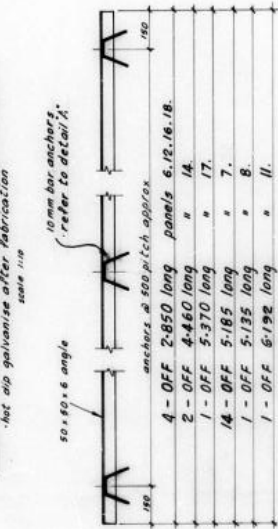
DOOR PROTECTOR ANGLES - NORTH WALL -



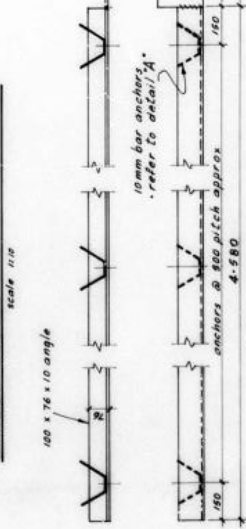
ANGLE SUPPORTS FOR DOOR GUIDES



WEATHER BARS FOR NORTH WALL DOORS

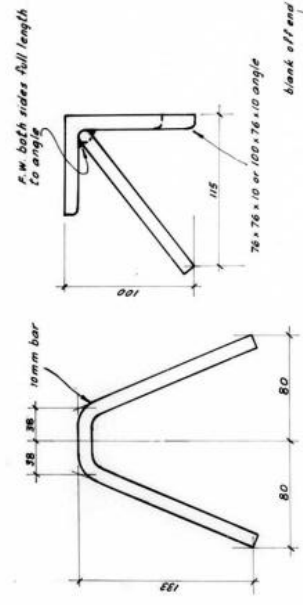


WINDOW ANGLES CAST IN R.C. PANELS

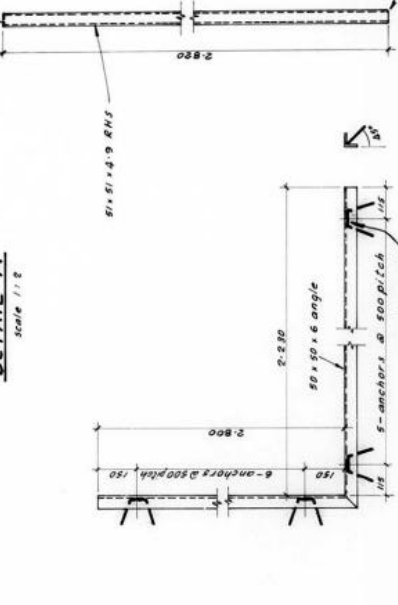


ANGLE SUPPORTS FOR DOOR GUIDES

Drawn	Checked	Reviewed	Approved	Date	By
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.



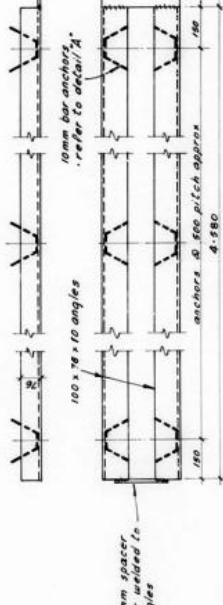
DETAIL "A"



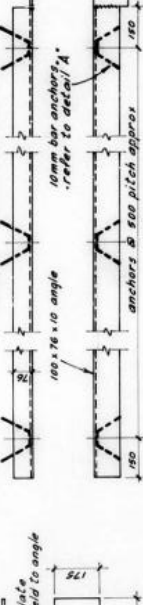
END POSTS FOR WINDOW SURROUNDS



WINDOW ANGLE

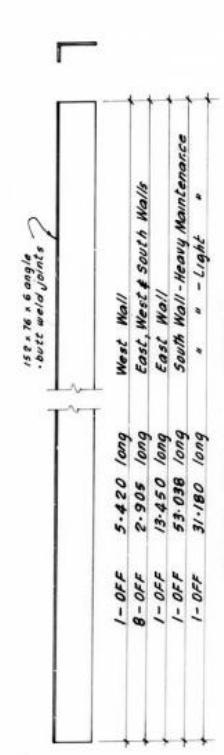


4 - OFF as drawn Grid Lines C & F

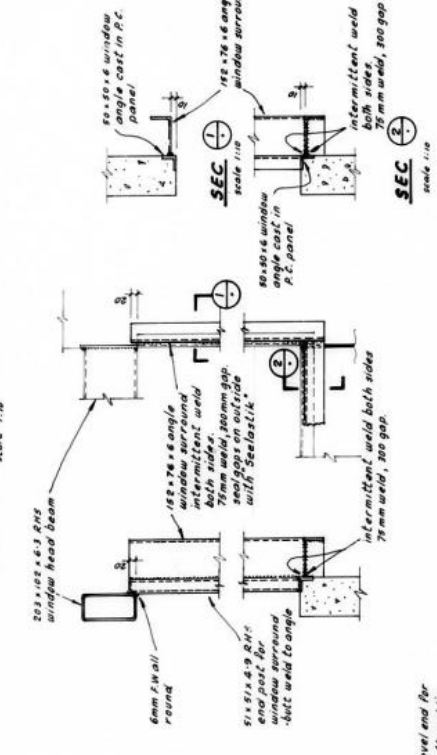


1 - OFF as drawn Grid Line G-D

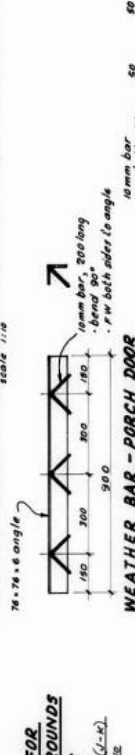
Drawn	Checked	Reviewed	Approved	Date	By
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.



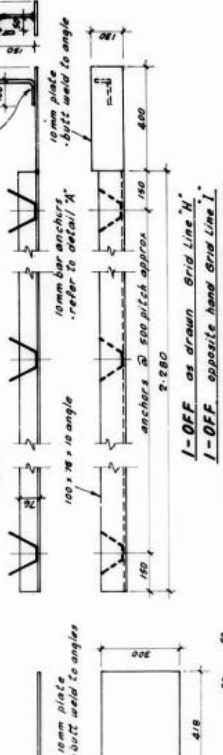
ANGLE WINDOW SURROUNDS



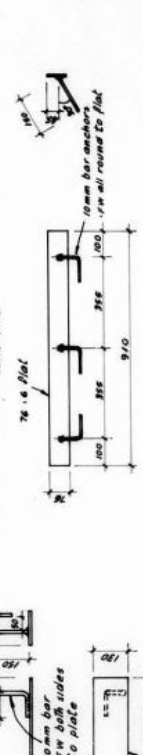
TYPICAL WINDOW DETAILS - SOUTH, EAST & WEST WALLS -



WEATHER BAR - PORCH DOOR



1 - OFF as drawn Grid Line N



1 - OFF as drawn Grid Line I

Drawn	Checked	Reviewed	Approved	Date	By
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.

WEATHER BARS FOR NORTH WALL DOORS

Drawn	Checked	Reviewed	Approved	Date	By
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.
P. B. B. B.	P. B. B. B.	P. B. B. B.	P. B. B. B.	1/1/18	P. B. B. B.
A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	A. E. B. B. B.	1/1/18	A. E. B. B. B.

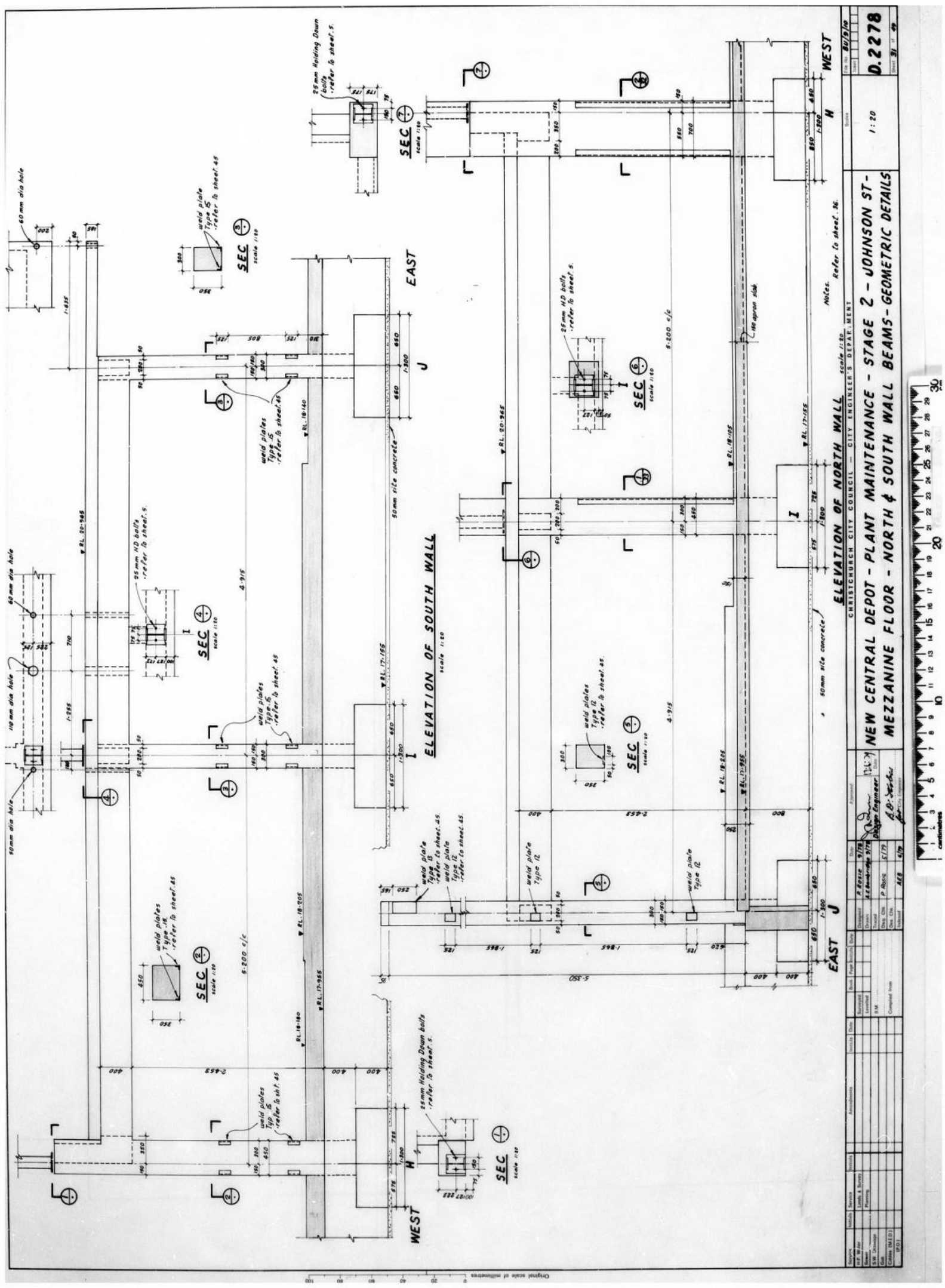
NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST -

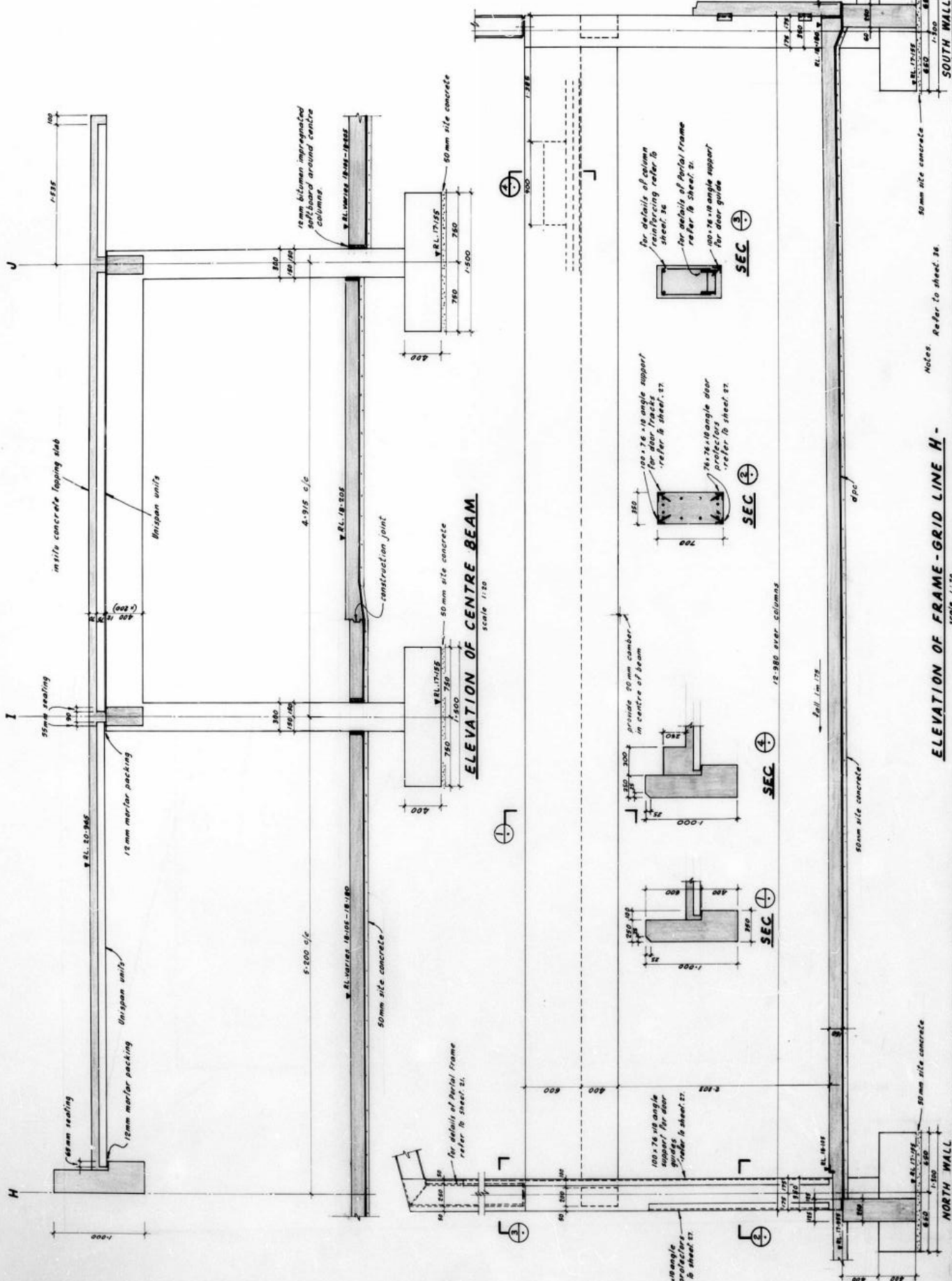
DETAILS OF DOOR & WINDOW ANGLES

[illegible]



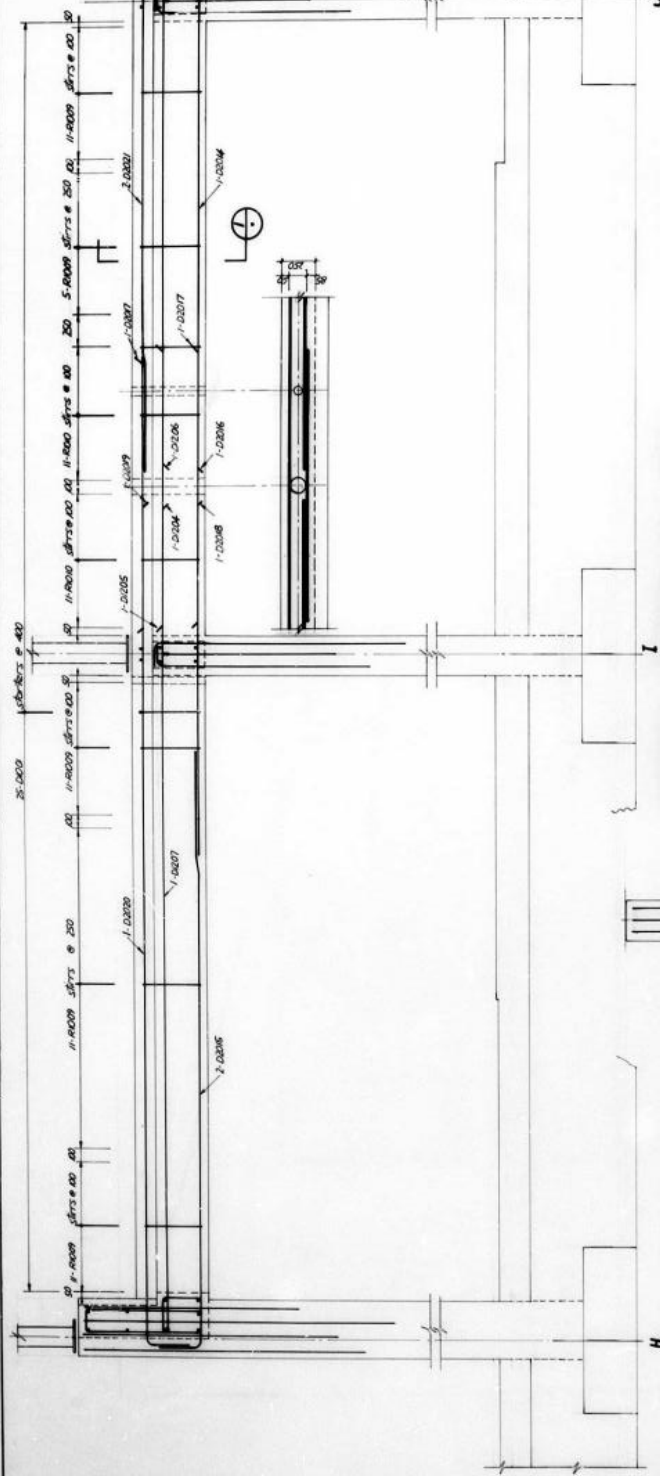
Project Name	Location	Service	Priority	Remarks	Contract	Draw	Spec	Prop	Unit	Time	Approval	Scale	Draw No.	Date
NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST - DETAILS OF PLATFORM FOR EXHAUST EXTRACTION FAN		Structural	High							1:5		1:5	0.2278	8/19/10
		Structural	High							1:10		1:10		



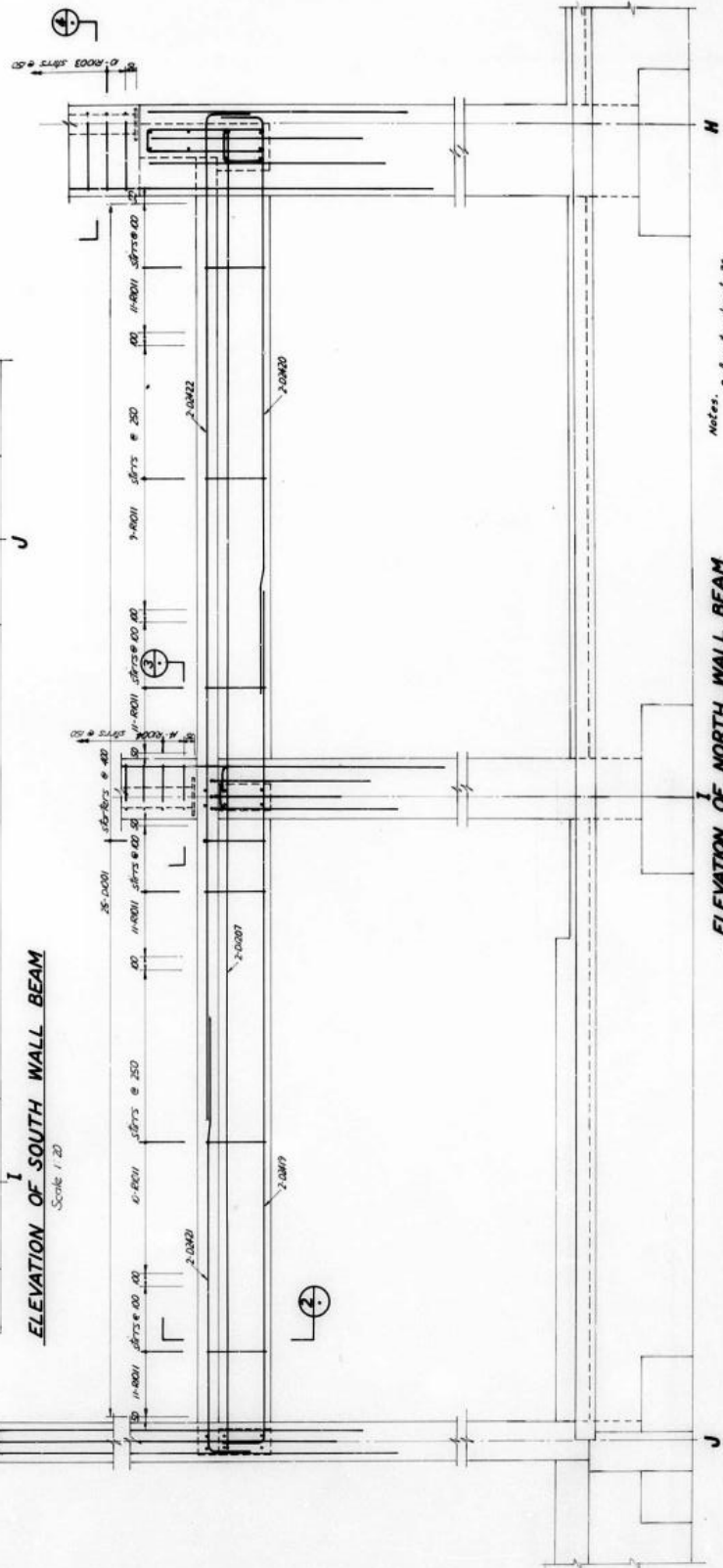


ELEVATION OF FRAME - GRID LINE H - H										NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST - MEZZANINE FLOOR - CENTRE BEAM & FRAME H - GEOMETRIC DETAILS -									
Scale 1:20										Notes: Refer to sheet 36.									
CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT										SOUTH WALL									
Scale 1:20										Scale 1:20									
Author: [Signature]										Check: [Signature]									
Date: 10/10/10										Date: 10/10/10									
Project: [Signature]										Project: [Signature]									
Drawn: [Signature]										Drawn: [Signature]									
Checked: [Signature]										Checked: [Signature]									
Approved: [Signature]										Approved: [Signature]									
Title: [Signature]										Title: [Signature]									
Scale: 1:20										Scale: 1:20									
Sheet: 10 of 10										Sheet: 10 of 10									





ELEVATION OF SOUTH WALL BEAM



ELEVATION OF NORTH WALL BEAM

Notes. Refer to sheet 36.

Scale 1:20

CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST
MEZZANINE FLOOR - NORTH & SOUTH WALL BEAMS - REINFORCING

1:20

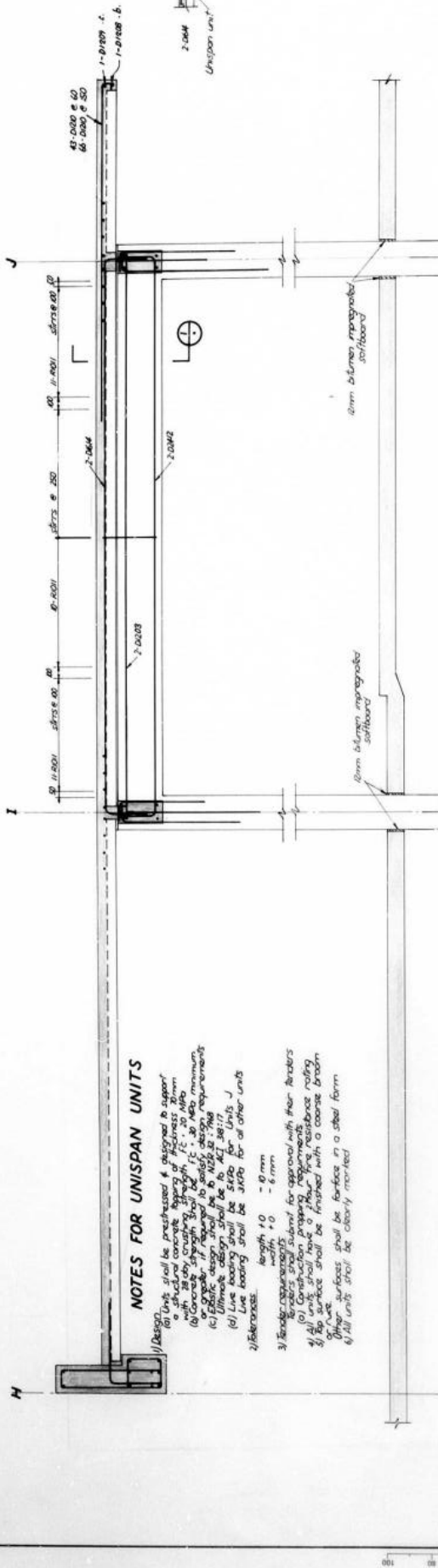
D2278

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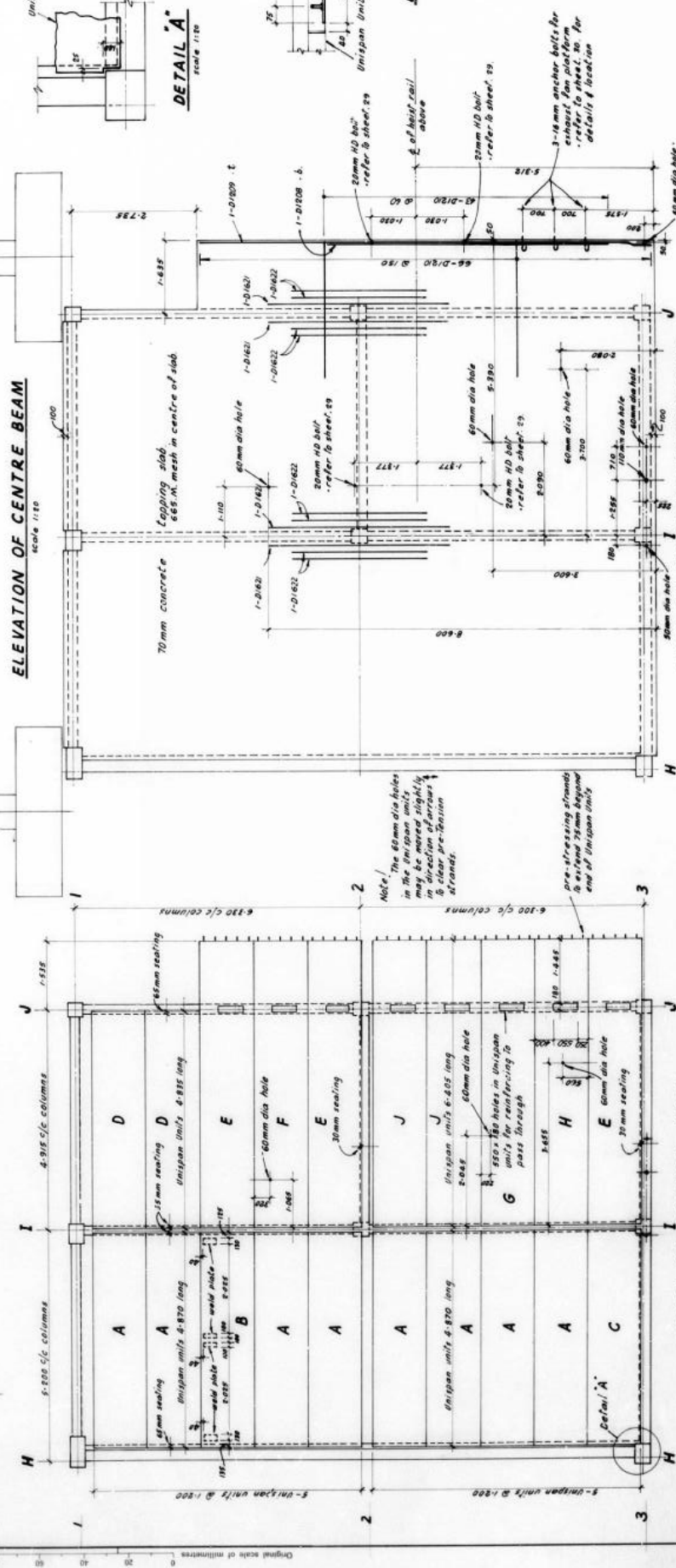
1 2 3
Cautions:

Original scale of millimetres



NOTES FOR UNISPAN UNITS

- 1) Design units shall be prestressed & designed to support a structural concrete topping of thickness 70mm with 80% minimum strength at 28 days. The units shall be designed to carry a load of 15 kN/m² over a 1m x 1m area. The units shall be designed to carry a load of 15 kN/m² over a 1m x 1m area. The units shall be designed to carry a load of 15 kN/m² over a 1m x 1m area.
- 2) Tolerances: length ± 0 - 6mm
- 3) Reinforcement: reinforcement shall be approved with their anchors.
- 4) All units shall have a 10mm diameter reinforcement.
- 5) Top surface shall be finished with a coarse sand.
- 6) All units shall be clearly marked.

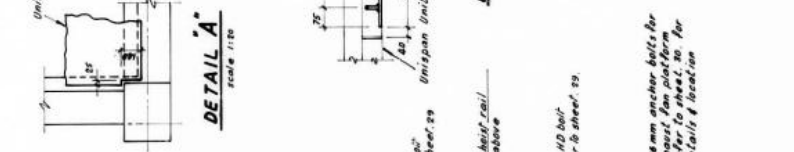


PLAN ON UNISPAN UNITS

Scale 1:10

PLAN ON CONCRETE TOPPING SLAB

Scale 1:10



DETAIL A

Scale 1:10

DETAIL OF WELDED PLATES

2-OFF 100mm wide

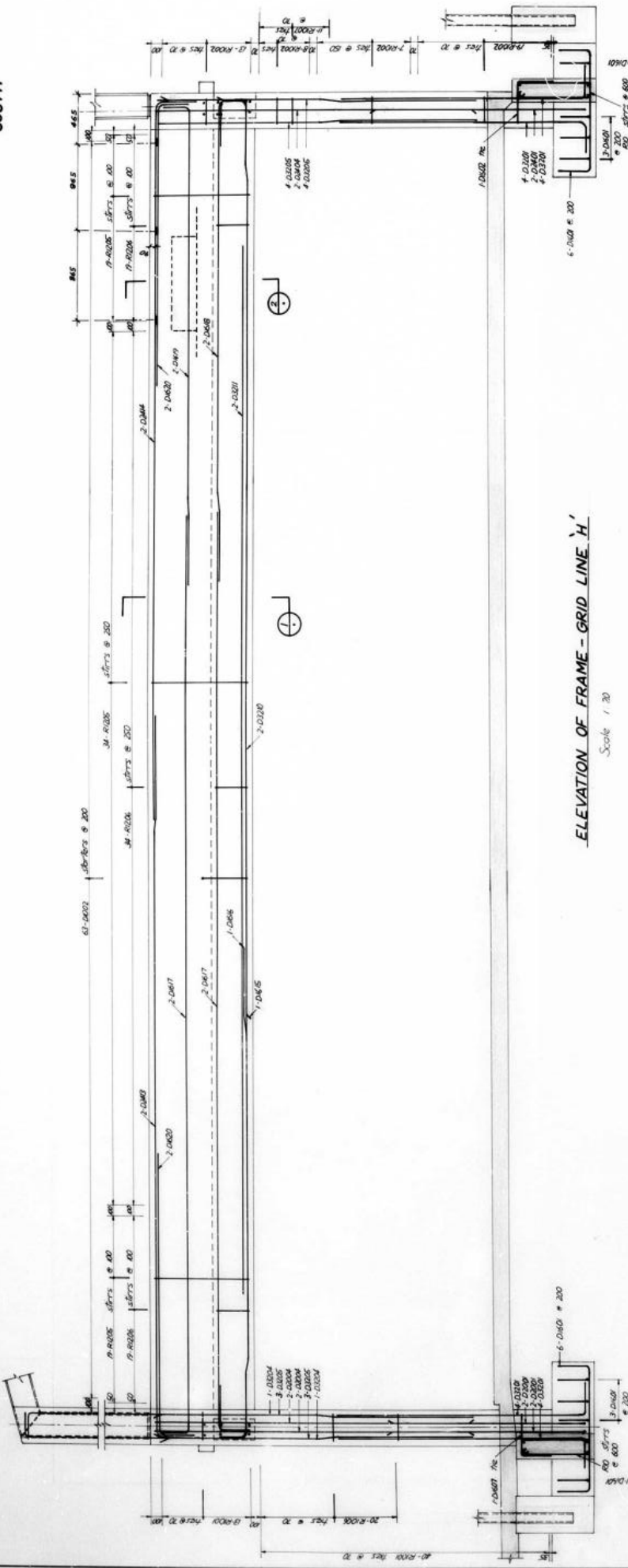
2-OFF 130mm wide

Scale 1:10

Notes: Refer to sheet No.

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST MEZZANINE FLOOR - CENTRE BEAM & FLOOR SLAB - REINFORCING		Date: 20/10/10 Scale: 1:20	D2278
Design: [Signature] Drawn: [Signature] Check: [Signature]	P. Base: 1/10 A/F: 1/10 P. Base: 1/10 A/F: 1/10	Date: 20/10/10 Scale: 1:20	Date: 20/10/10 Scale: 1:20
1. Design units shall be prestressed & designed to support a structural concrete topping of thickness 70mm with 80% minimum strength at 28 days. The units shall be designed to carry a load of 15 kN/m ² over a 1m x 1m area. The units shall be designed to carry a load of 15 kN/m ² over a 1m x 1m area. The units shall be designed to carry a load of 15 kN/m ² over a 1m x 1m area.	2. Tolerances: length ± 0 - 6mm	3. Reinforcement: reinforcement shall be approved with their anchors.	4. All units shall have a 10mm diameter reinforcement.
5. Top surface shall be finished with a coarse sand.	6. All units shall be clearly marked.	7. The 60mm dia holes in the reinforcement may be covered tightly in direction of stress to clear pre-tension strands.	8. pre-stressing strands to extend 25mm beyond end of unspan units.

NORTH

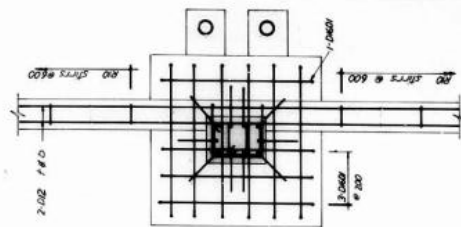


ELEVATION OF FRAME - GRID LINE 'H'

Scale 100

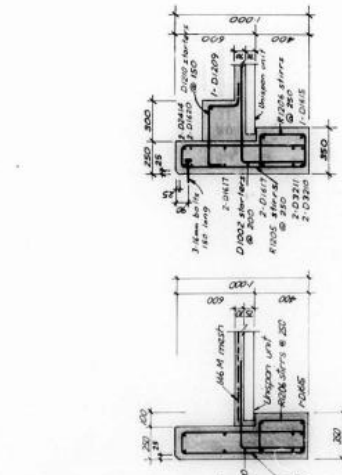
NOTES FOR MEZZANINE FLOOR

1. Concrete
- (a) Concrete strength shall be :-
 $f'c = 10 \text{ MPa}$ - Sile concrete
 $f'c = 20 \text{ MPa}$ - Columns & Beams
 $f'c = 25 \text{ MPa}$ - Structural topping to Usonian units
 - Concrete casing to Portal frame legs
- (b) Refer to bending schedule for bar lengths
- (c) $R =$ plain round bar Grade 375
 $D =$ deformed bar Grade 375
 - First two numbers shall be diameter
 - Last two numbers shall be tensile strength
 - Reinforcing to be continuous throughout unless scheduled otherwise
 - Laps not scheduled shall be :-
 10mm = 450
 12mm = 550
 16mm = 650
 20mm = 800
 24mm = 1000
 Mesh = 300
- (d) Refer to Architects & Mechanical Services drawings for details of bolts, nuts, washers, gaskets, etc. to be cast into or fastened to concrete.



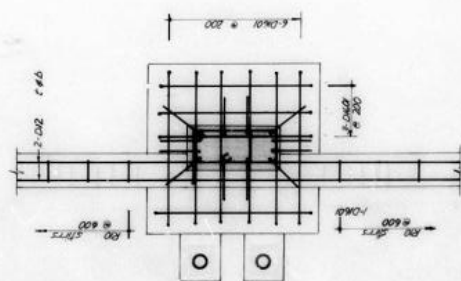
PLAN OF FOOTING H3

Scale 1:20



SECTION $\odot \frac{2}{1}$

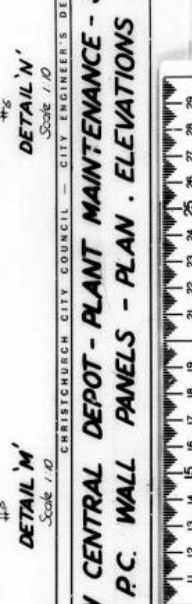
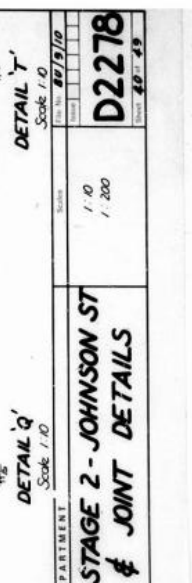
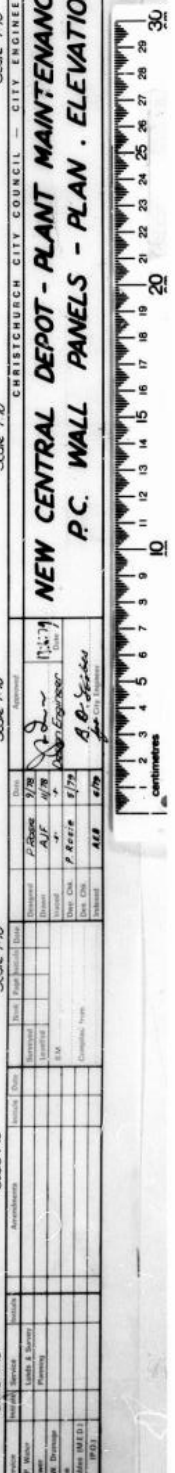
Scale 120

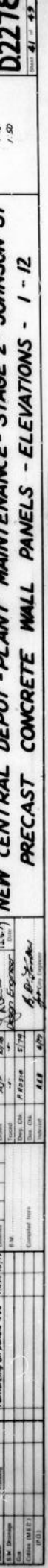
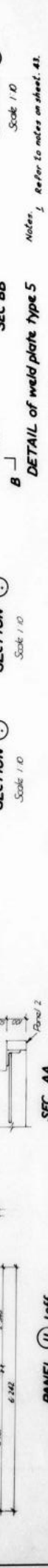
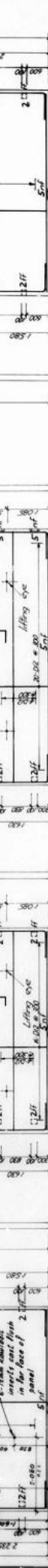
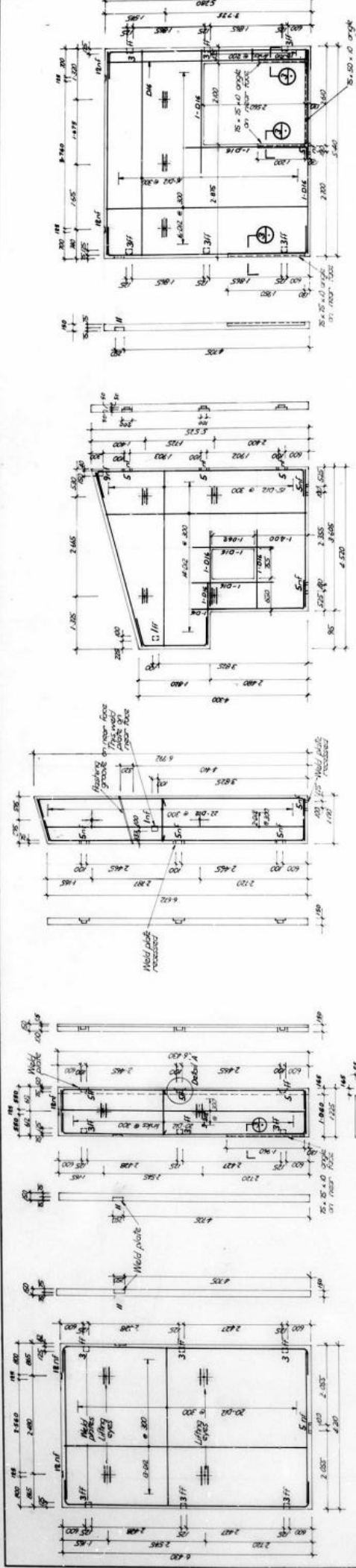


PLAN OF FOOTING H/

Books 1-30

[illegible]





Original scale of millimetres

Notes: 1. Refer to notes on sheet 41.

SECTION 10 Scale 1/10

SECTION 11 Scale 1/10

SECTION 12 Scale 1/10

SECTION 13 Scale 1/10

SECTION 14 Scale 1/10

SECTION 15 Scale 1/10

SECTION 16 Scale 1/10

SECTION 17 Scale 1/10

SECTION 18 Scale 1/10

SECTION 19 Scale 1/10

SECTION 20 Scale 1/10

SECTION 21 Scale 1/10

SECTION 22 Scale 1/10

SECTION 23 Scale 1/10

SECTION 24 Scale 1/10

SECTION 25 Scale 1/10

SECTION 26 Scale 1/10

SECTION 27 Scale 1/10

SECTION 28 Scale 1/10

SECTION 29 Scale 1/10

SECTION 30 Scale 1/10

SECTION 31 Scale 1/10

SECTION 32 Scale 1/10

SECTION 33 Scale 1/10

SECTION 34 Scale 1/10

SECTION 35 Scale 1/10

SECTION 36 Scale 1/10

SECTION 37 Scale 1/10

SECTION 38 Scale 1/10

SECTION 39 Scale 1/10

SECTION 40 Scale 1/10

SECTION 41 Scale 1/10

SECTION 42 Scale 1/10

SECTION 43 Scale 1/10

SECTION 44 Scale 1/10

SECTION 45 Scale 1/10

SECTION 46 Scale 1/10

SECTION 47 Scale 1/10

SECTION 48 Scale 1/10

SECTION 49 Scale 1/10

SECTION 50 Scale 1/10

SECTION 51 Scale 1/10

SECTION 52 Scale 1/10

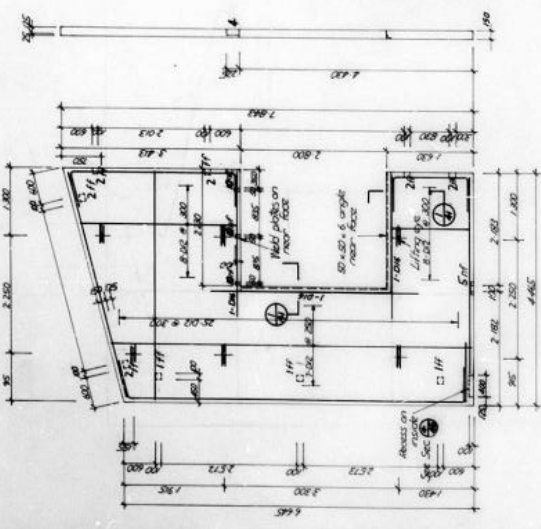
SECTION 53 Scale 1/10

SECTION 54 Scale 1/10

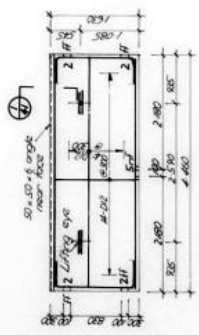
SECTION 55 Scale 1/10

SECTION 56 Scale 1/10

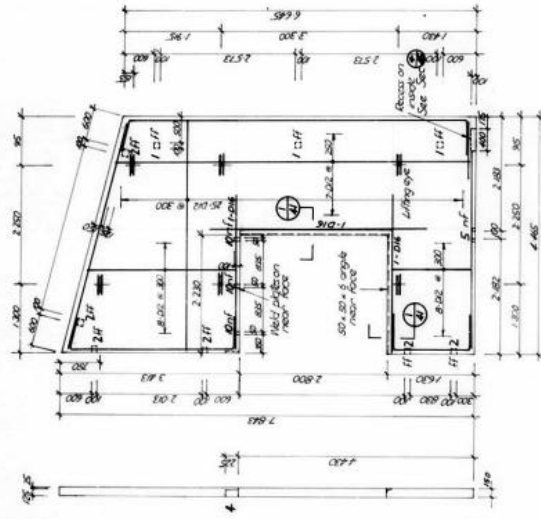
SECTION 57 Scale 1/10



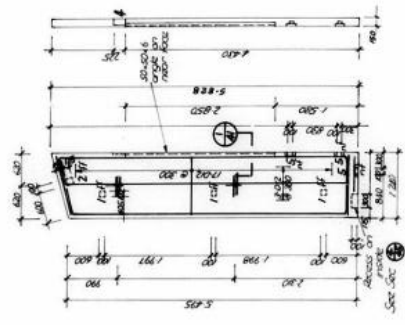
PANEL (3) 1 off
Scale 1:50



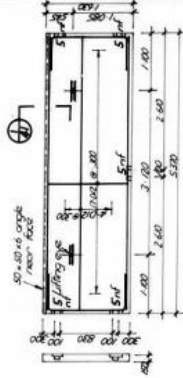
PANEL (4) 2 off
Scale 1:50



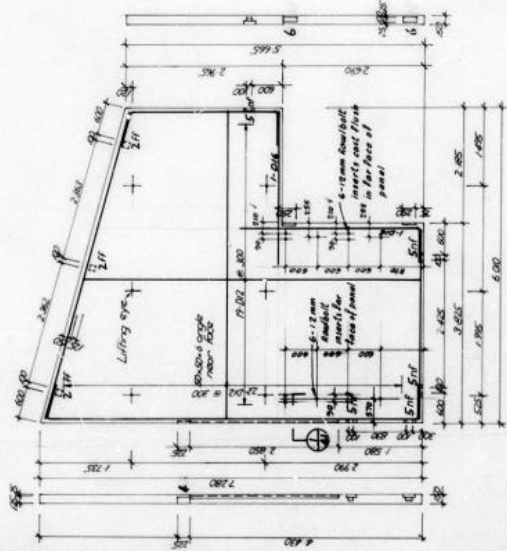
PANEL (5) 1 off
Scale 1:50



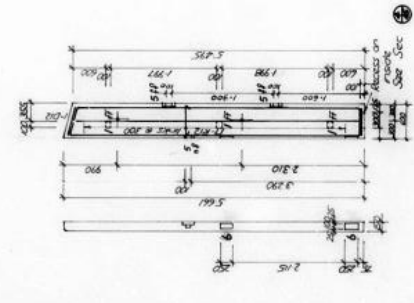
PANEL (6) 1 off
Scale 1:50



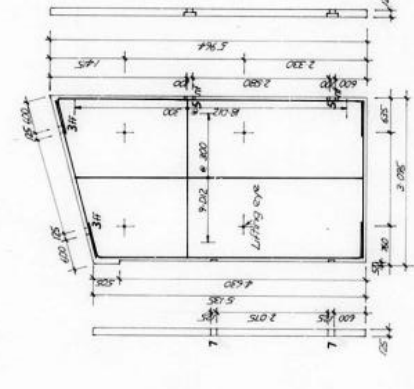
PANEL (7) 1 off
Scale 1:50



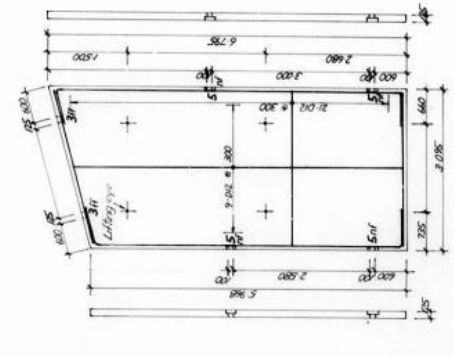
PANEL (8) 1 off
Scale 1:50



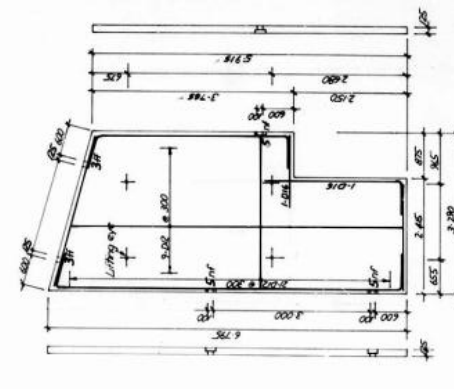
PANEL (9) 1 off
Scale 1:50



PANEL (20) 2 off
Scale 1:50



PANEL (21) 2 off
Scale 1:50



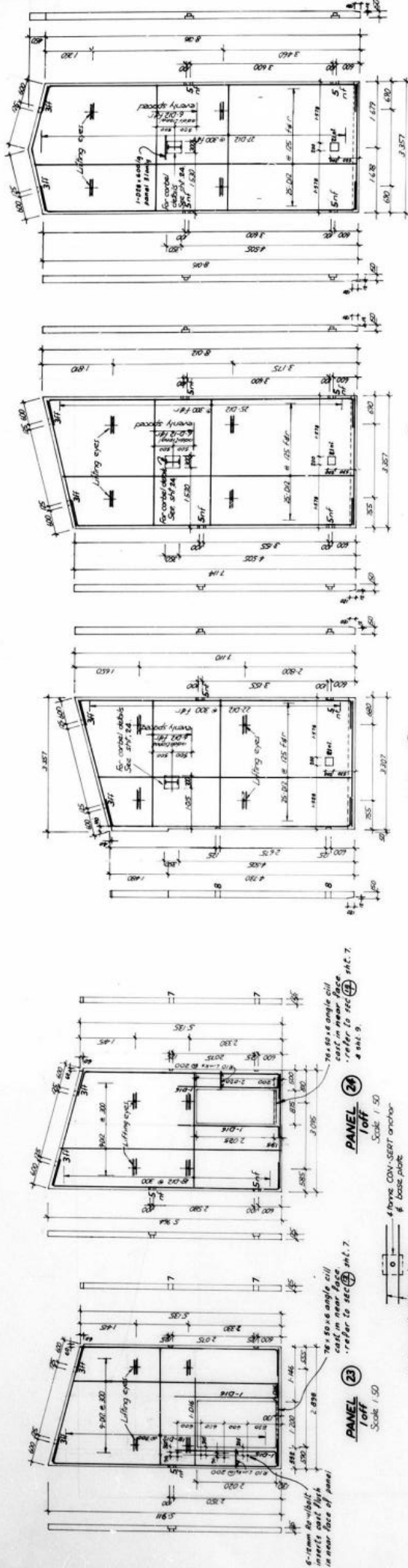
PANEL (22) 1 off
Scale 1:50

Notes
Refer to notes on sheet 43

CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT									
Drawn	Checked	Reviewed	Approved	Project	Sheet	Of	Scale	Date	Notes
P. Budge	P. Budge	P. Budge	P. Budge	NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST	1	1	1:50	10/10/10	
<p>1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29.</p>									
CENTIMETRES									

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST PRECAST CONCRETE WALL PANELS - ELEVATIONS - B - 22

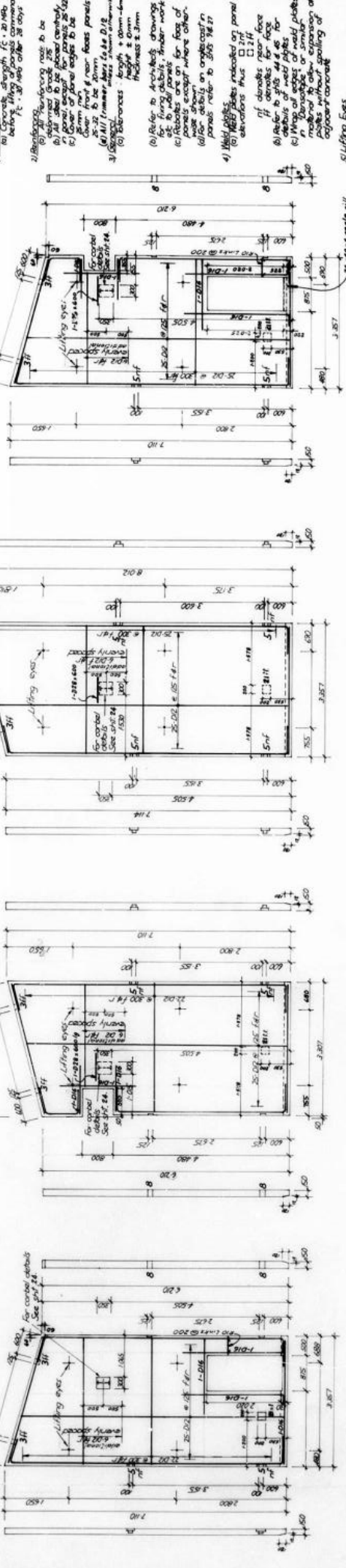
D2278



PANEL 23 1 off Scale 1:50
PANEL 24 1 off Scale 1:50
PANEL 25 1 off Scale 1:50
PANEL 26 1 off Scale 1:50
PANEL 27 1 off Scale 1:50
PANEL 28 1 off Scale 1:50

NOTES FOR PC PANELS
 1) Cast in situ concrete strength f_{cu} = 30 N/mm²
 2) Reinforcing steel to be as per BS 4449
 3) All steel to be protected with 20mm thick concrete
 4) Cover to reinforcement to be as per BS 8661
 5) All dimensions to be in mm unless otherwise stated
 6) All dimensions to be in mm unless otherwise stated
 7) All dimensions to be in mm unless otherwise stated
 8) All dimensions to be in mm unless otherwise stated
 9) All dimensions to be in mm unless otherwise stated
 10) All dimensions to be in mm unless otherwise stated

LIFTING EYE ANCHOR DETAIL
 161 OFF



PANEL 29 1 off Scale 1:50
PANEL 30 1 off Scale 1:50
PANEL 31 1 off Scale 1:50
PANEL 32 1 off Scale 1:50
PANEL 33 1 off Scale 1:50

SECTION 1/20
 Scale 1:20

SECTION 5/20
 Scale 1:20

SECTION 6/20
 Scale 1:20

SECTION 7/20
 Scale 1:20

SECTION 8/20
 Scale 1:20

SECTION 9/20
 Scale 1:20

SECTION 10/20
 Scale 1:20

SECTION 11/20
 Scale 1:20

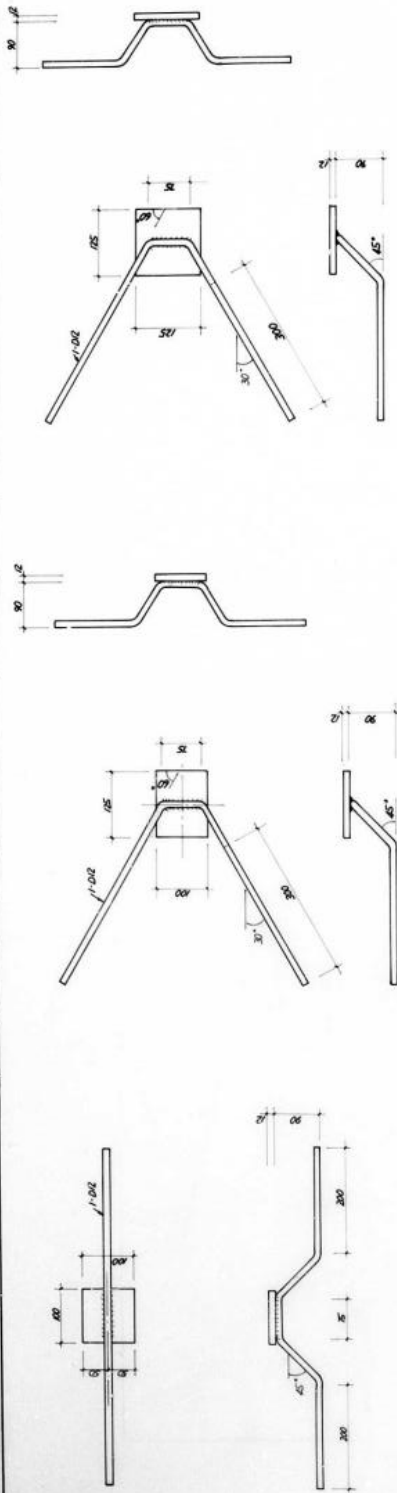
SECTION 12/20
 Scale 1:20

SECTION 13/20
 Scale 1:20

SECTION 14/20
 Scale 1:20

Section	Panel	Quantity	Unit	Material	Remarks
1	23	1	m ²	Concrete	
2	24	1	m ²	Concrete	
3	25	1	m ²	Concrete	
4	26	1	m ²	Concrete	
5	27	1	m ²	Concrete	
6	28	1	m ²	Concrete	
7	29	1	m ²	Concrete	
8	30	1	m ²	Concrete	
9	31	1	m ²	Concrete	
10	32	1	m ²	Concrete	
11	33	1	m ²	Concrete	

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2-JOHNSON ST
PRECAST CONCRETE WALL PANELS - ELEVATIONS - 23 - 32

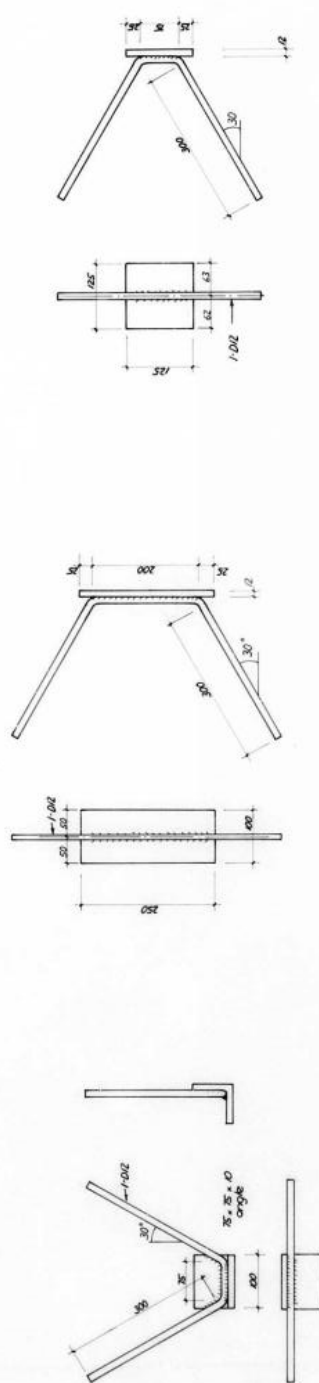


WELD PLATE - TYPE 1
1/6 off

WELD PLATE - TYPE 2
1/4 off

WELD PLATE - TYPE 3
5/1 off

WELD PLATE - TYPE 4
6 off

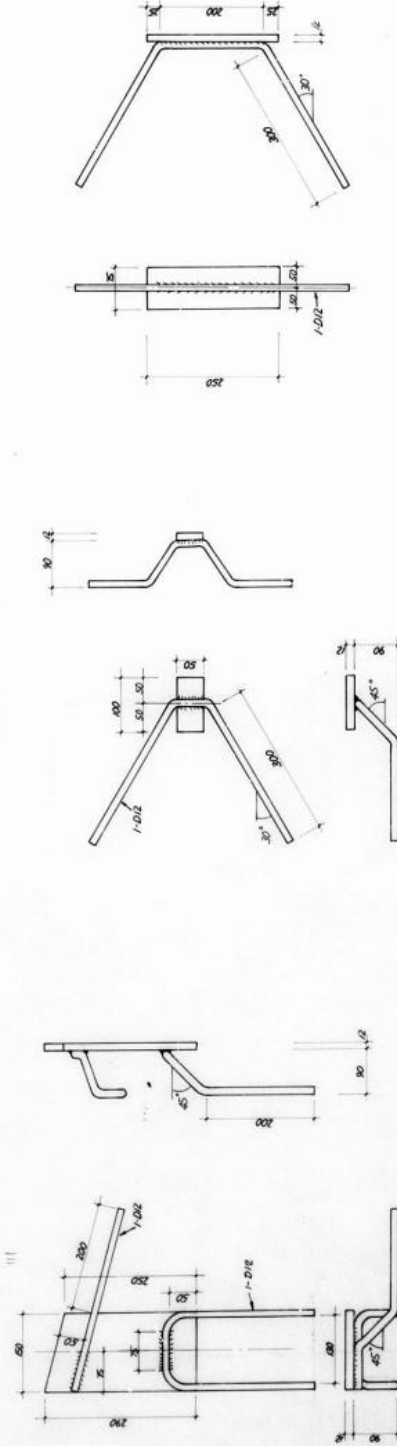


WELD PLATE - TYPE 5
1/13 off

WELD PLATE - TYPE 6
4 off

WELD PLATE - TYPE 7
8 off

WELD PLATE - TYPE 8
8 off



WELD PLATE - TYPE 9
1 off

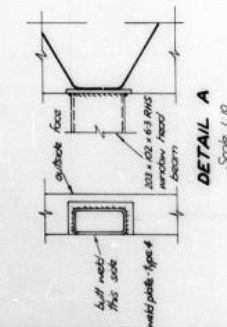
WELD PLATE - TYPE 10
6 off

WELD PLATE - TYPE 11
3 off

NOTES FOR WELD PLATES.
1) Bend radii not to scale. Inside radii shall be 40mm
2) Anchor bars shall be 12mm dia deformed bars
3) All welds to be 6mm fillet welds, lengths as detailed but not less than 75mm each side.

Rev	By	App'd	Check	Date	Remarks	Scale	Sheet No.	Total Sheets
1	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
2	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
3	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
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6	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
7	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
8	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
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28	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
29	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18
30	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18	11/11/18

NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST
DETAILS OF WELD PLATES
1:5
D2278
11/11/18



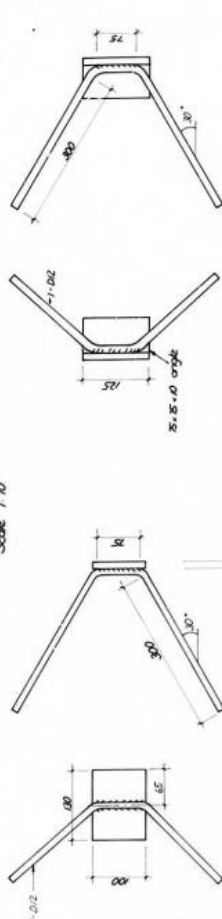
DETAIL A

DETAIL B
Scale 1/10

DETAIL C
Scale 1:10

**FIXING OF F
NORTH**

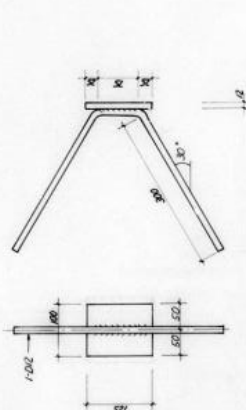
FIXING OF PC PANELS TO FOUNDATION WALLS
NORTH SOUTH, EAST & WEST



WELD PLATE - TYPE 13
1 off

WELD PLATE - TYPE 14
1 off

WELD PLATE - TYPE 15
12 off



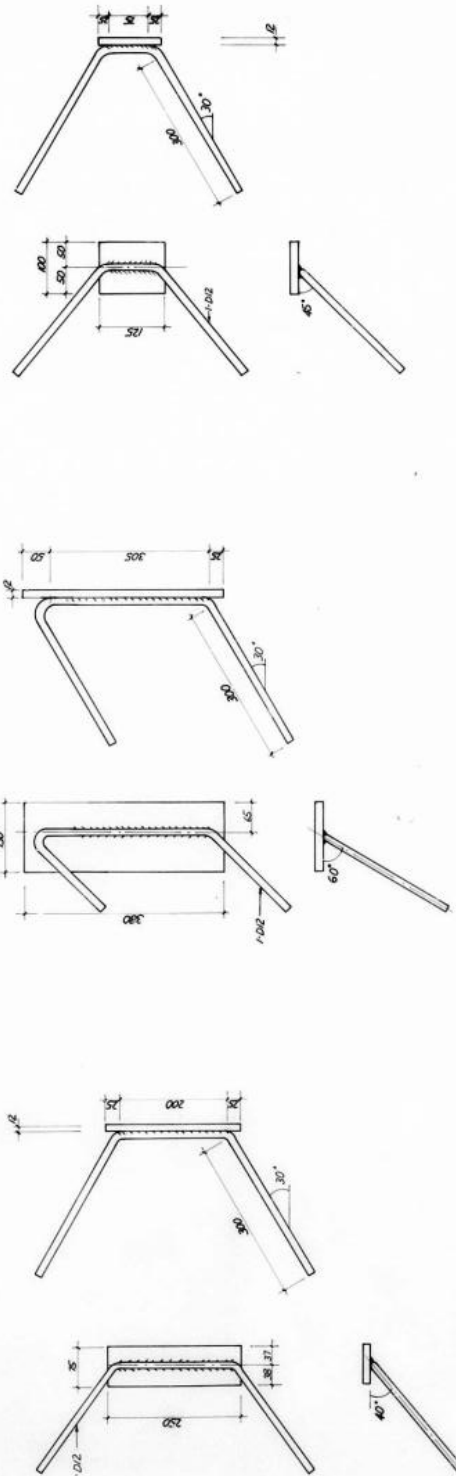
WELD PLATE - TYPE 12
12 off

WELD PLATE - TYPE 19
7-OFF

WELD PLATE - TYPE 16
1 off

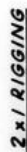
WELD PLATE - TYPE 17
I off

WELD PLATE - TYPE 18
30 off

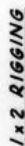


Notes: Refer to notes on slide 44

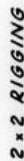
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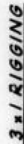
to be used for
PANELS 7 8 9 10 11 14 17.



to be used for
PANELS 2.3.16.19.



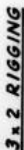
PANELS 1. 4. 6. 20. 21. 21x. 22. 23.
24. 25. 26. 26x. 27. 28. 29.
30. 30x. 31. 32.



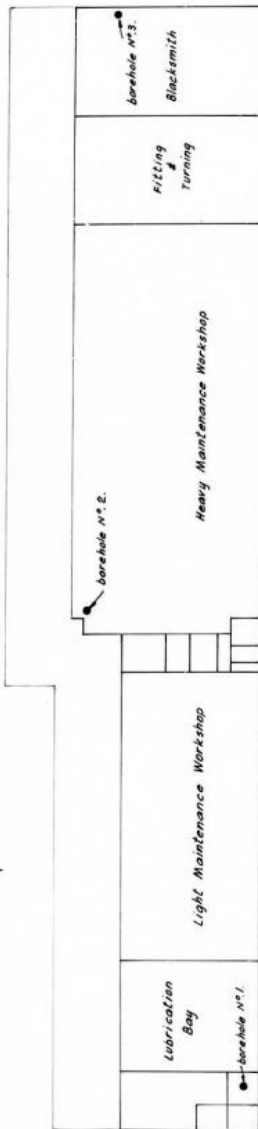
to be used for PANEL 5.



to be used for PANELS 13.15

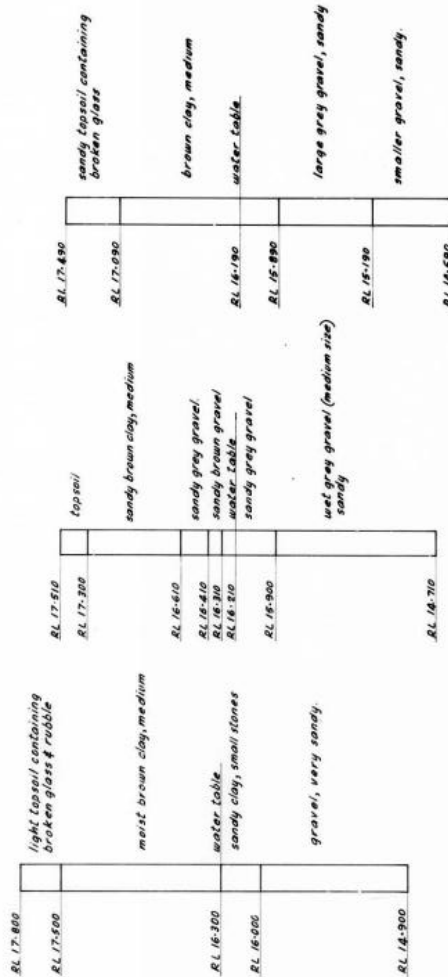


to be used for PANELS 12.18



BOREHOLE LOCATIONS

053 11 01033



Note! All topsoil has been removed by others & the site has been backfilled with pitrun hardfill to RL 17.600 by others.

BOREHOLE No 1.

vertical scale 1:20

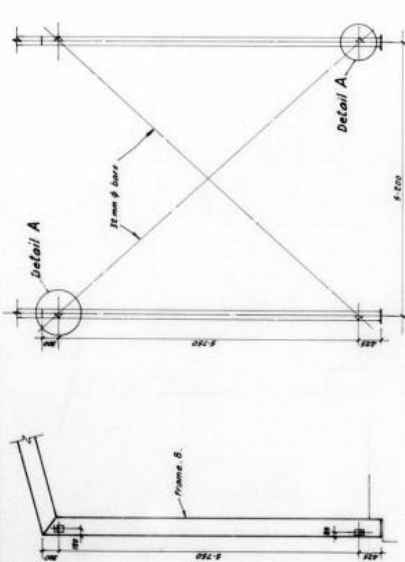
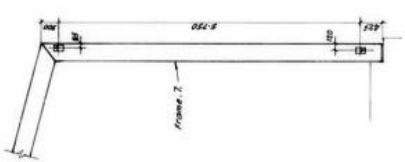
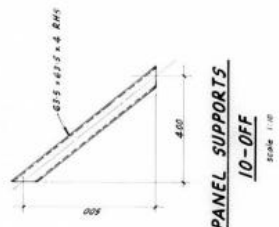
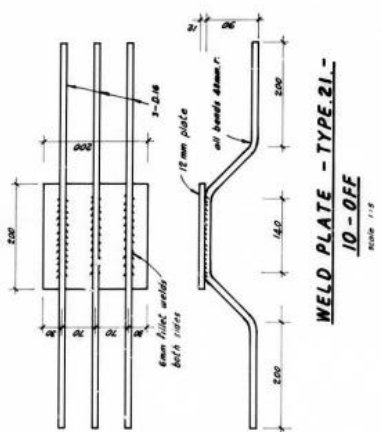
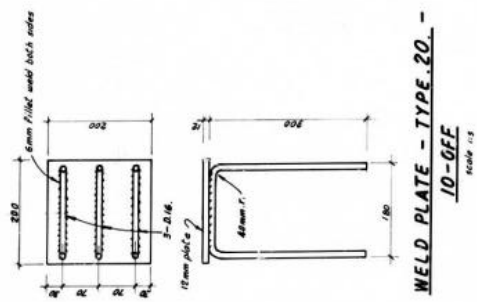
BOREHOLE N° 2:

vertical scale 1:20

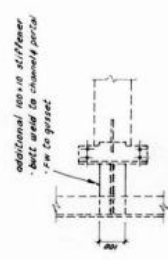
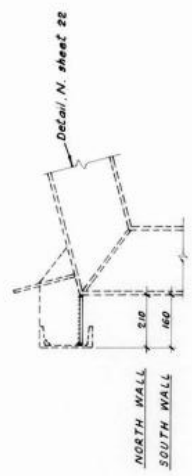
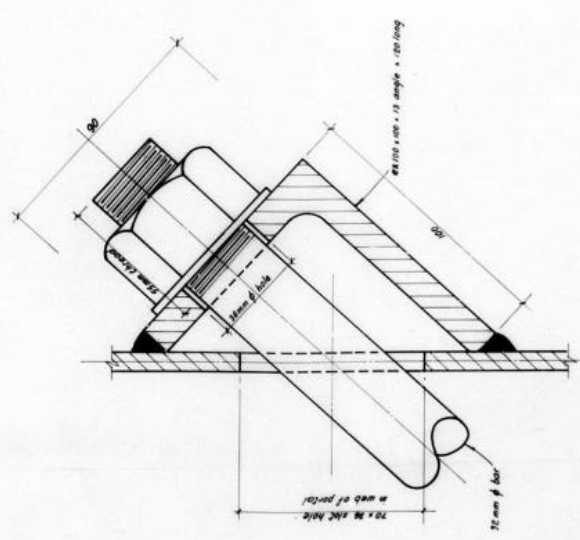
BOREHOLE N° 3.

vertical scale 1:20

[illegible]



ELEVATION OF DIAGONAL BRACING
NORTH WALL
South wall similar
Scale 1:10



ADDITIONAL STIFFENER TO DETAIL N
GRID LINES K & L ONLY
Scale 1:10

Notes
Refer to sheets 43/44

Drawn	Checked	Reviewed	Approved	Scale	Sheet	Drawn	Checked	Reviewed	Approved	Scale	Sheet
A	A	A	A	1:10	43	A	A	A	A	1:10	44
NEW CENTRAL DEPOT - PLANT MAINTENANCE - STAGE 2 - JOHNSON ST - DETAILS OF DIAGONAL BRACING ETC											
CHRISTCHURCH CITY COUNCIL - CITY ENGINEER'S DEPARTMENT											
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Appendix C

CERA DEE Summary Data

Detailed Engineering Evaluation Summary Data

V1.11

Location	
Building Name: Milton St Depot - Plant Maintenance Workshop	Reviewer: David Whittaker
Unit: No. Street	CPEng No: 123089
Building Address: 245 Milton Street	Company: Beca
Legal Description:	Company project number: 5323355
	Company phone number: 03 3663521
GPS south: Degrees Min Sec	Date of submission: 1/02/2012
GPS east:	Inspection Date: 1/02/2012
Building Unique Identifier (CCC): BU 1411-002 EQ2	Revision:
	Is there a full report with this summary? yes

Site	Site slope: flat	Max retaining height (m): 0
	Soil type:	Soil Profile (if available):
	Site Class (to NZS1170.5): D	
	Proximity to waterway (m, if <100m):	If Ground improvement on site, describe:
	Proximity to cliff top (m, if < 100m):	
	Proximity to cliff base (m, if <100m):	Approx site elevation (m):

Building	No. of storeys above ground: 1	single storey = 1	Ground floor elevation (Absolute) (m):
	Ground floor split?: no		Ground floor elevation above ground (m): 0.00
	Storeys below ground: 0		
	Foundation type: other (describe)		If Foundation type is other, describe:
	Building height (m): 5.00		height from ground to level of uppermost seismic mass (for IEP only) (m): 4.5
	Floor footprint area (approx): 545		Date of design: 1976-1992
	Age of Building (years): 32		
	Strengthening present?: no		If so, when (year)?
	Use (ground floor): other (specify)		And what load level (%g)?
	Use (upper floors): commercial		Brief strengthening description: N/A
	Use notes (if required): Workshop and offices upstairs		
	Importance level (to NZS1170.5): IL2		

Gravity Structure	Gravity System: frame system	
	Roof: steel framed	steel portal, timber purlins and profiled metal
	Floors: timber	joist depth and spacing (mm)
	Beams: steel non-composite	beam and connector type
	Columns: structural steel	typical dimensions (mm x mm)
	Walls: non-load bearing	0

Lateral load resisting structure	other (note)	Note: Define along and across in detailed report!	
Lateral system along:	1.25	0.00	describe system: Precast panels and steel cross bracing, with concrete frame mezzanine.
Ductility assumed, μ :	0.40		estimate or calculation? estimated
Period along:			estimate or calculation?
Total deflection (ULS) (mm):			estimate or calculation?
maximum interstorey deflection (ULS) (mm):			
Lateral system across:	other (note)		describe system: steel portal frames with concrete frame mezzanine
Ductility assumed, μ :	3.00	0.00	for governing concrete frame, 1.25 for portals
Period across:	0.40		estimate or calculation? estimated
Total deflection (ULS) (mm):			estimate or calculation?
maximum interstorey deflection (ULS) (mm):			estimate or calculation?

Separations:	north (mm):	leave blank if not relevant
	east (mm):	
	south (mm):	
	west (mm):	

Non-structural elements	Stairs: timber	describe supports: concrete wall adjacent
	Wall cladding: exposed structure	describe: concrete walls and glazing
	Roof Cladding: Metal	describe: corrugated iron
	Glazing: aluminium frames	
	Ceilings: light tiles	
	Services(list): lighting, roller door mechanical	

Available documentation	Architectural: none	original designer name/date: none available
	Structural: none	original designer name/date: none available
	Mechanical: none	original designer name/date: none available
	Electrical: none	original designer name/date: none available
	Geotech report: none	original designer name/date: none available

Damage	Site performance: slight	Describe damage: some liquefaction and pavement cracking
Site: (refer DEE Table 4-2)		
	Settlement: none observed	notes (if applicable):
	Differential settlement: none observed	notes (if applicable):
	Liquefaction: 0-2 m ³ /100m ³	notes (if applicable): estimated from 24th Feb aerial photo
	Lateral Spread: none apparent	notes (if applicable):
	Differential lateral spread: none apparent	notes (if applicable):
	Ground cracks: 0-20mm/20m	notes (if applicable): cracking to pavement observed
	Damage to area: slight	notes (if applicable):

Building:	Current Placard Status: green	
Along	Damage ratio: 0%	Describe how damage ratio arrived at:
	Describe (summary):	
Across	Damage ratio: 0%	$\text{Damage Ratio} = \frac{(\% \text{ NBS (before)} - \% \text{ NBS (after)})}{\% \text{ NBS (before)}}$
	Describe (summary):	
Diaphragms	Damage?: no	Describe: roof diaphragm not able to be seen
CSW's:	Damage?: no	Describe:
Pounding:	Damage?: no	Describe: N/A
Non-structural:	Damage?: no	Describe:

Recommendations	Level of repair/strengthening required: minor structural	Describe: concrete wall crack repair
	Building Consent required: no	Describe:
	Interim occupancy recommendations: full occupancy	Describe:
Along	Assessed %NBS before: 35%	##### %NBS from IEP below
	Assessed %NBS after: 35%	
Across	Assessed %NBS before: 70%	##### %NBS from IEP below
	Assessed %NBS after: 70%	

If IEP not used, please detail assessment methodology: Forced-based quantitative assessment

IEP

Use of this method is not mandatory - more detailed analysis may give a different answer, which would take precedence. Do not fill in fields if not using IEP.

Period of design of building (from above): 1976-1992

h_n from above: 4.5m

Seismic Zone, if designed between 1965 and 1992:

not required for this age of building
not required for this age of buildingPeriod (from above):
(%NBS)_{nom} from Fig 3.3:along
0.4
across
0.4Note:1 for specifically design public buildings, to the code of the day: pre-1965 = 1.25; 1965-1976, Zone A =1.33; 1965-1976, Zone B = 1.2; all else 1.0
Note 2: for RC buildings designed between 1976-1984, use 1.2
Note 3: for buildings designed prior to 1935 use 0.8, except in Wellington (1.0)Final (%NBS)_{nom}:along
0%
across
0%

2.2 Near Fault Scaling Factor

Near Fault scaling factor, from NZS1170.5, cl 3.1.6:

Near Fault scaling factor (1/N(T,D), Factor A:

along
#DIV/0!
across
#DIV/0!

2.3 Hazard Scaling Factor

Hazard factor Z for site from AS1170.5, Table 3.3:

Z_{max} from NZS4203:1992

Hazard scaling factor, Factor B:

#DIV/0!

2.4 Return Period Scaling Factor

Building Importance level (from above):
Return Period Scaling factor from Table 3.1, Factor C:

2.5 Ductility Scaling Factor

Assessed ductility (less than max in Table 3.2)
Ductility scaling factor: =1 from 1976 onwards; or =k_u, if pre-1976, from Table 3.3:

Ductility Scaling Factor, Factor D:

along
1.00
across
1.00

2.6 Structural Performance Scaling Factor:

Sp:

Structural Performance Scaling Factor Factor E:

#DIV/0!
#DIV/0!2.7 Baseline %NBS, (NBS%)_b = (%NBS)_{nom} x A x B x C x D x E%NBS_b:#DIV/0!
#DIV/0!

Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)

3.1. Plan Irregularity, factor A:

1

3.2. Vertical irregularity, Factor B:

1

3.3. Short columns, Factor C:

1

3.4. Pounding potential

Pounding effect D1, from Table to right
Height Difference effect D2, from Table to right

Therefore, Factor D:

0

3.5. Site Characteristics

1

Table for selection of D1	Severe	Significant	Insignificant/none
	0<sep<.005H	.005<sep<.01H	Sep>.01H
Separation			
Alignment of floors within 20% of H	0.7	0.8	1
Alignment of floors not within 20% of H	0.4	0.7	0.8

Table for Selection of D2	Severe	Significant	Insignificant/none
	0<sep<.005H	.005<sep<.01H	Sep>.01H
Separation			
Height difference > 4 storeys	0.4	0.7	1
Height difference 2 to 4 storeys	0.7	0.9	1
Height difference < 2 storeys	1	1	1

3.6. Other factors, Factor F

For ≤ 3 storeys, max value =2.5, otherwise max value =1.5, no minimum
Rationale for choice of F factor, if not 1Along
Across

Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)

List any:

Refer also section 6.3.1 of DEE for discussion of F factor modification for other critical structural weaknesses

3.7. Overall Performance Achievement ratio (PAR)

0.00
0.004.3 PAR x (%NBS)_b:

PAR x Baseline %NBS:

#DIV/0!
#DIV/0!

4.4 Percentage New Building Standard (%NBS), (before)

#DIV/0!

Official Use only:

Accepted By:
Date:

Appendix D

Previous Reports and Assessments

Job File: