



Christchurch City Council
Cranford Basin
Geotechnical Investigation Report

September 2015

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- Appendix B – (Existing Investigation Logs)
- Appendix C – (Further Investigation Results)
- Appendix D – (Laboratory Results)
- Appendix E - (Liquefaction Analysis)

1. Introduction

1.1 Background and Scope

The Christchurch City Council (CCC) is presently conducting a review of the District Plan. During this process some areas of the Cranford Basin have been considered for development as residential land use. Several investigations and reports in the area have been provided to the CCC by landowners (or their representatives) regarding the ground conditions at their property and the suitability of the land for residential land use.

GHD has been engaged by the CCC to undertake geotechnical investigations and reporting to outline the findings of the geotechnical investigations in relation to future residential development potential of the site to accompany the Section 32 report for rezoning of the area as part of Phase 3 of the District Plan Review. Specific comment was also requested regarding geotechnical implications of potential housing density for potential foundation types and relevant constraints to development of the area.

A previous desktop study produced by GHD (February 2015) identified the potential for significant organic materials (peat and organic silts) to be present across the majority of the area in question. Due to the potential settlement issues of organic material on building foundations further intrusive investigations have been undertaken to provide undisturbed samples of organic material. One-dimensional consolidation testing was undertaken on the undisturbed samples to provide estimations of potential settlement. Investigations were also undertaken in areas where previous investigations or information pertaining to ground conditions was not available.

1.2 Site Location

The proposed rezoning would involve the development of residential houses around some of the perimeter of the Cranford Basin, and a storm water detention area as illustrated by the Draft Papanui/Cranford Basin Planning Constraint Map provided in Appendix A.

The site is situated 4 km north of the Christchurch Central Business District. It is relatively flat at approximately 5 m above sea level. It is approximately 2.5 km south of Styx River and 7 km west of the coast (Pegasus Bay).

2. Supplied Geotechnical Investigations

CCC supplied GHD with a number of geotechnical investigation reports provided to them by land owners regarding the zoning of the land.

- Geotechnical Report for Proposed Plan Change, 340 Cranford St and 60 Croziers Rd, St Albans, Christchurch, prepared by Eliot Sinclair 30 June 2015.
- Site Appraisal – Geotechnical Report, Cranford Street, Christchurch, prepared by Connell Wagner 18 February 2007.
- Proposed Subdivision Development, 340/341 Cranford Street. Preliminary Geotechnical Evaluation, prepared by Tonkin & Taylor Ltd April 2013.
- Desktop Geotechnical Review, Proposed Christchurch Replacement District Plan for the Case Family at 340 Cranford Street, Saint Albans, prepared by Eliot Sinclair 15 April 2015.

- Geotechnical Report, Proposed 12.5-hectare Residential Subdivision, Grants Road, Papanui, prepared by Bell Geoconsulting Ltd April 2013.

3. Published Information on Ground Conditions

3.1 Published Geology

As shown in Figure 1, Brown & Weeber¹ (1992) indicates that the site geology comprises two different units. The majority of the site is overlying peat swamp, now drained. The north eastern end of the section is overlying dominantly alluvial sand and silt overbank deposits. Both units are alluvial soils of the Yaldhurst Member, sub-group of the Springston Formation, Holocene in age.

Brown and Webber (1992) also shows the Riccarton gravels are located approximately 10-15 m bgl and groundwater is likely within 1-2 m of ground level.

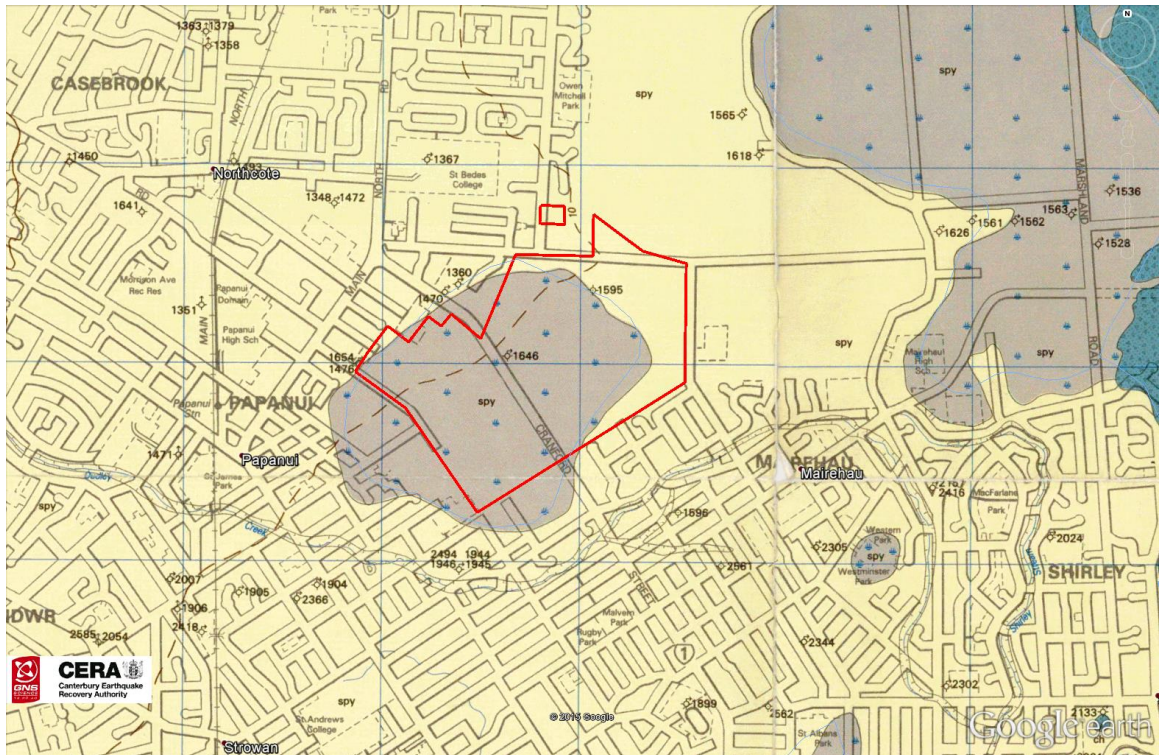


Figure 1 Geology Map Excerpt

3.2 Environment Canterbury Logs

A search of the Environment Canterbury (ECan) groundwater wells identified many wells with lithographic bore logs present in the proposed area. Several of the logs located around the site are summarised in Table 1. Location of investigations is provided in Appendix B. Full logs are provided in Appendix B.

¹ Brown, L. J. & Weeber, J.H. (1992): Geology of the Christchurch Urban Area. Institute of Geological and Nuclear Sciences 1:25,000 Geological Map 1. IGNS Limited: Lower Hutt.

Table 1 Ecan Well Logs

Bore Name	Log Depth	Groundwater	Location	Log Summary
M35/12374	3.2 m	0.5 m bgl	Southern corner	0.0 – 0.5 m Peat soil 0.5 – 3.2 m Peat
M35/15178	6.0 m	Not recorded	Southern edge	0.0 – 2.5 m Peat soil 2.5 – 6.0 m Grey silt
M35/15177	6.0 m	Not recorded	Southern edge	0.0 – 2.45 m Peat and silt 2.45 – 6.0 m Grey silt
M35/14948	3.0 m	Not recorded	Southern edge	0.0 – 0.8 m Topsoil and peat 0.8 – 3.0 m Silt
M35/14966	3.9 m	Not recorded	South-eastern corner	0.0 – 0.2 m Topsoil 0.2 – 2.4 m Sandy silt 2.4 – 3.2 m Peat 3.2 – 3.9 m Silt
M35/13183	3.09 m	Not recorded	Eastern edge	0.0 – 1.52 m Gravelly topsoil 1.52 – 2.99 m Peat 2.99 – 3.09 m Sandy Silt
M35/12573	1.2 m	0.55 m bgl	Eastern edge	0.0 – 0.3 m Topsoil some silt 0.3 – 0.8 m Clayey silt 0.8 – 1.2 m Peat
M35/18347	23.0 m	Not recorded	Northern edge	0.0 – 0.3 m Topsoil 0.3 – 3.2 m Silt 3.2 – 6.3 m Peat 6.3 – 19.1 m Sand 19.1 – 23.0 m Sandy gravel
M35/12643	15.2 m	Not recorded	Northern edge	0.0 – 0.76 m Topsoil, sand 0.76 – 1.37 m Peat 1.37 – 5.18 m Sandy silt and peat 5.18 – 15.2 m Sand some gravel
M35/10866	15.0 m	Not recorded	North western edge	0.0 – 0.7 m Topsoil 0.7 – 7.0 m Silt with organics 7.0 – 15.0 m Sand/silty sand
M35/15699	5.2 m	0.7 m bgl	North western edge	0.0 – 0.4 m Topsoil 0.4 – 0.9 m Sand

Bore Name	Log Depth	Groundwater	Location	Log Summary
				0.9 – 1.6 m Peat 1.6 – 2.7 m Silt 2.7 – 3.4 m Peat 3.4 – 4.4 m Sandy silt 4.4 – 5.2 m Peat
M35/14022	12.2 m	Not recorded	Western corner	0.0 – 3.05 m Peat and clay 3.05 – 12.2 m Sand some silt
M35/14021	7.32 m	1.42 m bgl	Western edge	0.0 – 4.27 m Peat and clay 4.27 – 5.79 m Sand and silt 5.79 – 7.32 m Gravel
M35/14019	5.18 m	Not recorded	Western edge	0.0 – 3.05 m Peat and clay 3.05 – 4.88 m Sand 4.88 – 5.18 m Gravel
M35/1646	25.4 m	3.7 m	Centre	0.0 – 0.6 m Topsoil 0.6 – 6.3 m Peat 6.3 – 14.6 m Gravel 14.6 – 17.8 m Sand 17.8 – 18.3 m Peat 18.3 – 25.4 m Gravel

It should be noted that the logs have been written by the well driller and not a geotechnical professional or to a standard. In addition strength data is not recorded.

3.3 Canterbury Geotechnical Database Investigations

Multiple investigations are present on the Canterbury Geotechnical Database (CGD) around the proposed site. A summary of pertinent logs is provided in Table 2, full logs are provided in Appendix A.

Table 2 Canterbury Geotechnical Database Investigations

Bore Name	Location	Depth	Log Summary
BH_27476	Eastern edge	22.0 m	0.0 – 3.0 m Fill 3.0 – 5.5 m Organic SILT (SPT-N 0,1) 5.5 – 7.0 m Sandy SILT and SAND (SPT-N 14) 7.0 – 17.5 m SAND & GRAVEL (SPT-N 14-46) 17.5 – 18.0 m PEAT 18.0 – 22.0 m Sandy GRAVEL (SPT-N 50)
BH_23510	Southern	11.15 m	0.0 – 3.0 m Sandy SILT (SPT-N 0-17)

Bore Name	Location	Depth	Log Summary
	corner		3.0 – 6.0 m SILT some organics (SPT-N 0-4) 6.0 – 11.15 m SAND & GRAVEL (SPT-N 14-36)
BH_20993	Southern edge	10.95 m	0.0 – 1.5 m SAND 1.5 – 5.7 m PEAT & Organic SILT (SPT-N 0 -7) 5.7 – 10.95 m SAND & GRAVEL (SPT-N 18-24)
BH_35483	Northern point	21.61 m	0.0 - 2.0 m PEAT & organic CLAY (SPT-N 0) 2.0 – 5.8 m CLAY & organic CLAY (SPT-N 0-4) 5.8 – 17.8 m SAND some silt (SPT-N 15-36) 17.8 – 18.2 m ORGANIC SILT 18.2 – 21.6 m SAND & GRAVEL (SPT-N 50-69)
BH_23908	North-eastern edge	18.5 m	0.0 – 1.3 m SAND 1.3 – 6.5 m SILT & PEAT (SPT-N 0-2) 6.5 – 8.5 m Silty SAND (SPT-N 9-18) 8.5 – 17.5 m SAND (SPT-N 12-41) 17.5 – 18.5 m PEAT & SAND with peat

3.3.1 Crack data

No cracks were recorded on the proposed site in the CGD post-earthquake crack data layer. Several <10 mm cracks have been identified 100 m south of the southern corner of the site.

3.3.2 Post Earthquake Land Observations

The aerial photography interpretation of observed liquefaction identifies the northern portion of the site as having experienced minor liquefaction with some moderate to severe liquefaction observed in the north-eastern corner of the site following the 4 September 2010 earthquake.

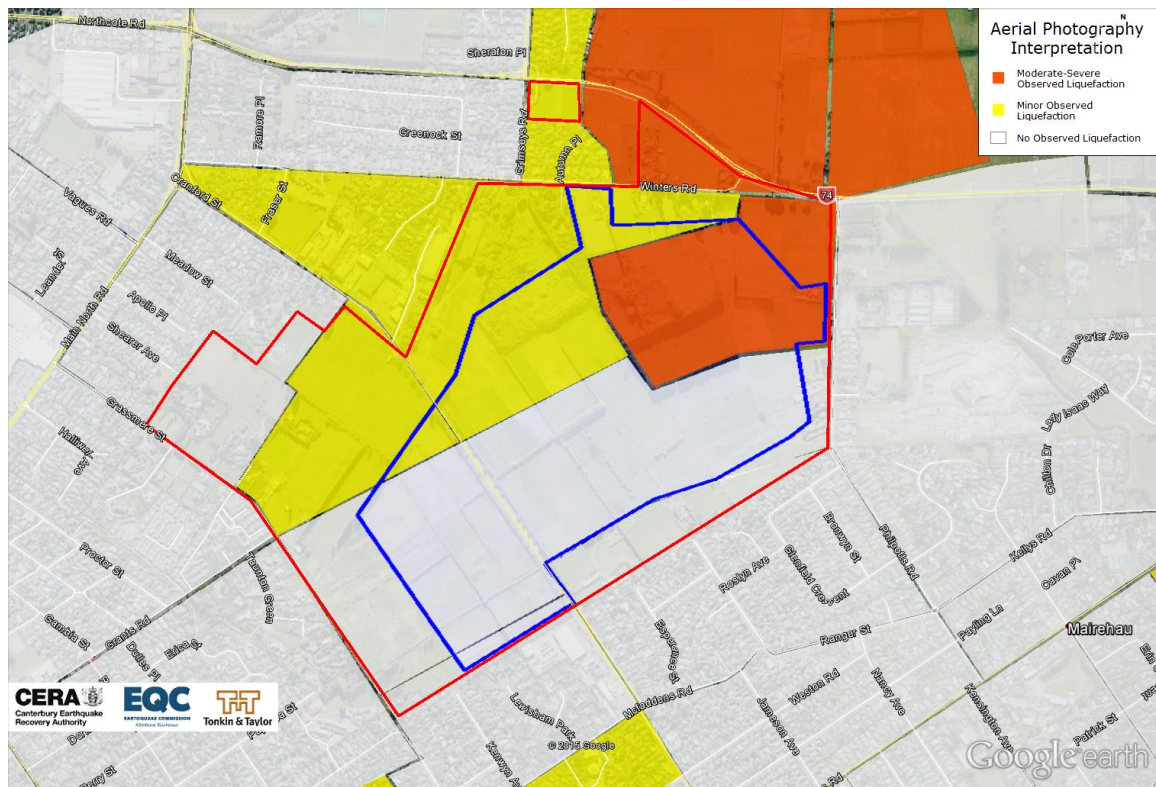


Figure 2 Aerial Photography Liquefaction Interpretation, 4 September 2010

3.3.3 Shallow Foundation Hazard Map, August 1990

The shallow foundation hazard map² provided in the CGD identifies the area as being a high risk area where investigation is essential due to peat areas and old swamps or lakes.

3.4 CERA Landing Zoning

Canterbury Earthquake Recovery Authority (CERA) has indicated the site is situated within the Green Zone, indicating that repair and rebuild may take place.

Land in the CERA green zone has been divided into three technical categories. These categories describe how the land is expected to perform in future earthquakes.

The site has been categorised as “N/A” – Urban Non-residential”. However, surrounding residential properties to the north, west and east have been categorised as TC2 (yellow), indicating minor to moderate land damage from liquefaction is possible in future significant earthquakes. Some neighbouring properties to the south have been categorised as TC3 (blue) zone³. This means that moderate to significant land damage from liquefaction is possible in future significant earthquakes.

3.5 Historic Aerials

Historic aerials available on the ECan GIS database show snapshots of the land use of the site from 1941 until present. The earliest aerial available (1941) shows the site being used for agricultural production of fruit and vegetables. The land use has not changed much from 1941 to the present, some roading has been added through the site and residential houses constructed around the perimeter.

² Canterbury Geotechnical Database (2012) "Shallow Foundation Hazard Map - 1990", Map Layer CGD5132 - 20 Nov 2012, retrieved 11/02/2015 from <https://canterburygeotechnicaldatabase.projectorbit.com/>

³ CERA Landcheck website, <http://cera.govt.nz/my-property>

3.6 Listed Land Use Register

A brief search of the Environment Canterbury List Land Use Register (LLUR) identified several properties have HAIL (List of Hazardous Activities and Industries) activities including:

- A8 – Livestock dip or spray race operations
- A10 – Persistent pesticide bulk storage or use (multiple properties)
- A17 – Storage tanks or drums for fuel, chemicals or liquid waste.

If the land use is to be changed from its current land use to residential land use it is recommended a Preliminary Site Investigation and subsequent Detailed Site Investigation are undertaken in accordance with the National Environmental Standards..

4. Seismicity

4.1.1 Nearby Faults

There are many faults in the Canterbury region, however only those considered most likely to have an adverse effect on the site are detailed below.

Table 3 Summary of Known Active Faults^{4,5}

Known Active Fault	Distance from Site	Direction from Site	Max Likely Magnitude	Avg Recurrence Interval
Alpine Fault	120 km	NW	~8.3	~300 years
Greendale Fault (2010)	22 km	W	7.1	~15,000 years
Hope Fault	105 km	N	7.2~7.5	120~200 years
Kelly Fault	105 km	NW	7.2	~150 years
Porters Pass Fault	60 km	NW	7.0	~1100 years
Port Hills Fault (2011)	10 km	N	6.3	Not Estimated

The recent earthquake sequence since 4 September 2010 has identified the presence of a previously unmapped active fault system underneath the Canterbury Plains. This includes the Greendale Fault and Port Hills Fault listed in Table 3 above. Research and published information on this system is in development and the average recurrence interval is yet to be established for the Port Hills Fault.

4.1.2 Ground Shaking Hazard

New Zealand Standard NZS 1170.5:2004 quantifies the Seismic Hazard factor for Christchurch as 0.30, being in a moderate to high earthquake zone. This value has been upgraded recently (from 0.22) to reflect the seismicity hazard observed in the earthquakes since 4 September 2010.

The recent seismic activity has produced earthquakes of Magnitude 6.3 with significant peak ground accelerations (PGA) across large parts of the city.

Conditional PGA's from the CGD⁶ indicate the PGA to be 0.20 g during the 4 September 2010 earthquake, 0.26 g on 22 February 2011, and 0.15 g on 13 June 2011.

⁴ Stirling, M.W, McVerry, G.H, and Berryman K.R. (2002): "A New Seismic Hazard Model for New Zealand", Bulletin of the Seismological Society of America, Vol. 92 No. 5, June 2002, pp. 1878-1903.

⁵ GNS Active Faults Database, <http://maps.gns.cri.nz/website/af/viewer>

⁶ Canterbury Geotechnical Database (2012): "Conditional PGA for Liquefaction Assessment", Map Layer CGD5110 - 27 Sept 2012, retrieved 11/02/2015 from <https://canterburygeotechnicaldatabase.projectorbit.com/>

5. Further Geotechnical Investigations

A previous desktop study produced by GHD (February 2015) identified the potential for significant organic materials (peat and organic silts) to be present across the majority of the area to be investigated. Due to the potential settlement issues of organic material on building foundations investigations have been undertaken to provide undisturbed samples of organic material. Investigations were also undertaken in areas where previous investigations or information pertaining to ground conditions was not available.

Five sonic boreholes with standard penetration tests (SPT), collection of undisturbed samples, and five cone penetrometer tests were scheduled. One borehole and CPT were not undertaken as access to the property was not provided.

The ground conditions encountered in the GHD investigations are summarised in this section. Table 4 and Table 5 provide summaries of the ground materials encountered in the investigations. Detailed logs can be found in Appendix B.

5.1 Machine Drilled Boreholes Summary

The GHD machine drilled boreholes (BH101 to BH102) shows that the subsurface geology is relatively consistent across the area investigated (Table 4).

Table 4 Summary of Machine Drilled Boreholes

Soil Unit	BH101	BH102	BH103	BH104
Topsoil	0.0 – 0.3 m	0.0 – 0.8 m	0.0 – 0.5 m	0.0 – 0.6 m
Upper Alluvium	0.3 – 1.1 m	0.8 – 2.9 m	0.5 – 2.5 m	0.6 – 1.4 m
Swamp Deposits	1.1 – 2.0 m	2.9 – 3.8 m	2.5 - 4.3 m	1.4 – 2.9 m
Lower Alluvium	2.0 – 15.08 m	3.8 – 12.49 m	4.3 – 17.05 m	2.9 – 10.97 m

Groundwater was encountered between 0.83 m bgl and 0.85 m agl

The boreholes investigations were scheduled to a target depth of 20 m below ground level, however risk of significant artesian pressures meant holes were terminated before this depth.

5.2 CPT Investigations

The soil behaviour type encountered by the GHD CPT's investigations is summarised in Table 5. Groundwater depths were recorded at the completion of each from 0.5 to 1.3 m bgl.

Table 5 Summary of CPT-Inferred Lithology for CPT101 to CPT104

Soil Behaviour Type	CPT101	CPT102	CPT103	CPT104
Clays and sand mixtures	0.5 – 4.8 m	0.0 – 0.6 m	0.0 – 5.6 m	0.0 – 1.6 m
Organic	-	0.6 – 3.7 m	-	1.6 – 3.1 m
Sand mixtures	4.8 – 8.0 m	-	5.6 – 8.4 m	3.1 – 4.8 m
Sands	8.0 – 15.7 m	3.7 – 8.6 m	-	4.8 – 14.5 m
Clays and sand mixtures	15.7 – 17.4 m	8.6 – 10.0 m	-	14.5 – 16.7 m
Sands	17.4 – 17.78 m	10.0 – 16.1 m	8.4 – 14.3 m	16.7 – 17.02 m

Soil Behaviour Type	CPT101	CPT102	CPT103	CPT104
Clays and sand mixtures		16.1 – 17.2 m	14.3 – 16.3 m	
Sands		17.2 – 18.09 m	16.3 – 17.13 m	

6. Laboratory Testing

Undisturbed samples were recovered from each of the boreholes, the materials targeted for sampling were high in organic content as this is the most likely to cause the greatest consolidation. One-dimensional consolidation testing was undertaken on the undisturbed samples to provide estimations of potential settlement.

Four undisturbed samples were sent to the Geotechnics Auckland Laboratory to undertake one-dimensional consolidation test. The tests were undertaken in accordance with NZS 4402:1986 Test 7.1. This procedure involves the incremental loading of the sample and calculation of the void ratio (consolidation) of the sample at each incremental load. The sample is then unloaded and elastic rebound is then measured. Three of the samples were loaded up to 483 kPa, the remaining sample was loaded up to 241 kPa as this sample may have begun to plastically deform under the higher load.

A summary of the results is provided in Table 6, full test results are provided in Appendix C.

Table 6 One Dimensional Consolidation Test Summary

Specimen	Description	Maximum Pressure	Coefficient of Volume Compressibility M_v (m^2/MN)
BH101 2.5 – 2.55 m	Sandy SILT, trace clay	483 kPa	0.055 to 0.090
BH102 3.65 – 3.70 m	Organic SILT, minor clay	241 kPa	1.0 to 2.5
BH103 3.05 – 3.10 m	SILT, minor organics	483 kPa	0.35 to 1.4
BH104 3.10 – 3.15 m	SILT, minor clay	483 kPa	0.15 to 1.2

7. Summary of Ground Conditions

A location plan showing all the ground condition information considered in this report has been provided in Appendix D.

The proposed site is an area that is well known to be underlain by swamp derived deposits comprising soft silts, organic silts and peat. From the investigations available from ECan well database, the CGD, and our further investigations the site has been determined to comprise alluvium, underlain by swamp derived deposits. This is further underlain by alluvium, underlain by the Riccarton Gravels.

7.1.1 Upper Alluvium

The upper alluvium is present to depths of 1.0 to 3.0 m bgl. It comprises sand, silty sands, sandy silts and silts. This material has low strengths of very loose to loose and very soft to firm.

7.1.2 Organic Deposits

Previous investigations and further investigations have shown organic deposits are present across the majority of the site, some areas have minimal organic material present. The layer of organic deposits varies in thickness across the site, typically it is at least 1m thick. The material comprises silts, organic silts and peat with strengths varying from very soft to soft.

7.1.3 Lower Alluvium

The lower alluvium is encountered beneath the swamp deposits. It has a similar composition to the upper alluvium with the addition of gravel and a higher sand content in the form of sandy gravel and gravel layers. The gravel content is not present across the entire site. This layer has a higher density (up to dense) than the upper alluvium due to its higher sand and gravel content.

7.1.4 Riccarton Gravels

The Riccarton Gravels are present below the lower alluvium and are encountered approximately 17 to 20 m bgl. This layer comprises dense to very dense sandy gravels.

7.1.5 Groundwater

Groundwater has been recorded in investigation logs between 0.85 m agl and 3.7 m bgl. Typically the upper alluvium and organic deposits act as a confining layer for the underlying sand and gravel lower alluvium.

8. Liquefaction Analysis

8.1 Methodology used for Analysis

Assumptions made for the analysis process are as follows:

- Importance Level 2, 50-year design life, giving peak ground accelerations (PGA's) of:
 - 0.35 g for Ultimate Limit State (ULS), and
 - 0.13 g for Serviceability Limit State (SLS);
- Earthquake Magnitude 7.5; and
- Groundwater levels at 2.0 m bgl.

Liquefaction assessment has been calculated using CLiq⁷ (CPT Liquefaction Assessment Software) using the Boulanger and Idriss 2014 method.

The raw data for the CPT's has been obtained from the CGD, provided by landowners investigations or our own investigations, this data has been reanalysed.

8.2 Results of Liquefaction Analysis

8.2.1 Liquefiable Strata

The results of the liquefaction analysis using the CPT data under ULS conditions (Importance level 2, 0.35g) identified discrete layers of liquefiable material throughout the depth investigated. Further details can be found in the Liquefaction and Settlement Analysis Graphs in Appendix D.

⁷ CLiq v.1.7.1.14 (2006), GeoLogismiki

8.2.2 Calculated Liquefaction-induced Settlements

Estimated ground settlements for ULS (L3), SLS, ULS index, and SLS index events are outlined in Table 7.

Index Values are calculated liquefaction-induced settlements for the top 10 m of subsoils (refer MBIE Guidelines⁸). These values are a key parameter used in the determining TC2 and TC3 ground performance. The ULS index value is calculated using a Importance Level 2 PGA of 0.35g.

⁸ Ministry of Business, Innovation & Employment (2012): *Guidance: Repairing and rebuilding houses affected by the Canterbury earthquakes*; Version 3, Dec 2012. Ministry of Business, Innovation & Employment: Wellington, NZ.

Table 7 Liquefaction-induced Settlements Calculated from CPTs

Investigation Point	Depth Investigated	SLS Index Value	ULS Index Value	Total SLS Settlement	Total ULS Settlement Level 3
		(PGA: 0.13g)	(PGA: 0.35)	(PGA: 0.13g)	(PGA: 0.45g)
CPT101	17.78 m	60 mm	142 mm	93 mm	238 mm
CPT102	18.09 m	22 mm	48 mm	46 mm	138 mm
CPT103	17.13 m	59 mm	98 mm	87 mm	162 mm
CPT104	17.02 m	11 mm	72 mm	33 mm	140 mm
CPT17238	6.70 m	12 mm	31 mm	12 mm	31 mm
CPT23216	19.68 m	14 mm	37 mm	22 mm	108 mm
CPT32136	10.00 m	73 mm	118 mm	73 mm	118 mm
CPT32142	10.00 m	34 mm	92 mm	134 mm	92 mm
CPT32143	10.00 m	44 mm	75 mm	44 mm	75 mm
CPT32145	10.00 m	68 mm	120 mm	68 mm	120 mm
CPT55297	6.37 m	12 mm	32 mm	12 mm	32 mm
CPT55301	7.34 m	19 mm	30 mm	19 mm	30 mm
CPT7836	2.99 m	0 mm	0 mm	0 mm	0 mm
CPT7840	2.99 m	0 mm	1 mm	0 mm	1 mm
CPT9167	7.05 m	12 mm	46 mm	12 mm	46 mm
BGL001	5.61 m	10 mm	42 mm	10 mm	42 mm
BGL002	5.32 m	8 mm	24 mm	8 mm	24 mm
BGL003	5.33 m	5 mm	30 mm	5 mm	30 mm
BGL004	6.23 m	14 mm	28 mm	14 mm	28 mm
BGL005	5.01 m	2 mm	16 mm	2 mm	16 mm
BGL006	3.76 m	8 mm	14 mm	8 mm	14 mm
BGL007	5.33 m	18 mm	46 mm	18 mm	46 mm
BGL008	8.09 m	56 mm	83 mm	56 mm	83 mm
BGL009	4.37 m	9 mm	35 mm	9 mm	35 mm
BGL010	4.79 m	8 mm	21 mm	8 mm	21 mm
BGL011	6.08 m	3 mm	21 mm	3 mm	21 mm
BGL012	6.31 m	17 mm	48 mm	17 mm	48 mm
TC2		0-50 mm	0-100 mm		
TC3		> 50 mm	> 100 mm		

8.3 Interpretation of Liquefaction Assessment

Overall, the site is considered to be of low to moderate liquefaction susceptibility. This is based on:

- Limited observable liquefaction damage from the post-February earthquake aerial photograph;
- Estimated settlements being potentially significant for ULS index (0 to 142 mm) and SLS index (0 to 68 mm), ground performances indicated from CPT analysis range from TC2 to TC3.
- Shallow groundwater levels of approximately 2.0 m; and

The excess pore water pressures that must be developed to liquefy a soil increase with depth below the water table; this typically only occurs in a large-magnitude, long-duration earthquakes. Deeper layers (below 15 m) are not likely to develop this level of pressure. This means susceptible soils are unlikely to liquefy below 15 m depth. In addition, the effects of deeper strata liquefying are not as consequential at the surface.

9. Hydrogeological Assessment

The lithology of the shallow material within the Cranford Basin influences the hydraulic characteristics of the shallow groundwater system. The conceptual geological model for the site describes the presence of thin layer of alluvial material, overlying more dense silts and organic material (i.e. peat), which give way to sand and silt deposits with occasional gravel lenses. The presence of the shallow alluvial material is not consistent across the site, with numerous bore logs describing soils which give way to organic peat deposits. Brown and Weeber¹ (1992) describe the surficial geology as a drained swamp, with organic peats and silts near surface. Historically the Cranford Basin drained to the Avon River catchment to the South (PDP⁹, (2013)). However, the installation of drainage networks by land owners has resulted in the majority of the Cranford basin being drained to the Styx River catchment via the Rhodes Main Drain sub-catchment. The southern part of the basin drains to the Dudley Creek catchment and to the Avon River.

The geological sequence of the deposits is approximated in Table 4, with a summary of Environment Canterbury well logs provided in Table 1. The Riccarton Gravel aquifer (referred to as the first confined aquifer) is located at or about 17-20 m bgl, and was not targeted for this investigation. However, for the purpose of this report it is considered to be hydraulically distinct from the overlying deposits of the Christchurch and Springton deposits. This is consistent with White *et al* (2007)¹⁰, which characterised the extent of the Springston gravel lobes within the Christchurch deposits. The Cranford Basin is within an area classified by White *et al* (2007) as being associated with the Fendalton Gravel lobe. The water bearing units of the Springston and Riccarton gravels were considered to be disconnected based on the information presented in White *et al* (2007).

The variable thickness of the upper alluvium material across the site suggests that the water table aquifer is limited in vertical thickness and lateral extent, with the groundwater within the alluvial material likely to be perched on the underlying silts and organic peat deposits. Drainage of the water table aquifer is likely to occur towards the shallow drainage networks that are located across the site area. The hydraulic properties of the shallow alluvial material are not known. Recharge to the water table is likely to be from rainfall infiltration and possible groundwater seepage from the underlying Springston formation.

The silt and organic peats that are documented across the site at or about 1 m bgl to 4.5 m bgl is associated with the swamp deposits of the Christchurch Formation. The silt material is considered to be of low permeability, with hydraulic conductivity likely to be less than 1×10^{-8} m/s in the horizontal flow direction. However, specific tests on the silt layer were not undertaken in the field. The presence of organic peat material is likely to act as an area of weakness in the confining layer, which may enable groundwater in the lower alluvial deposits to upwell and discharge as spring flow. In addition, where the silt deposits are thin there is the potential for groundwater from the lower alluvial deposits to breach the confining layer and emerge as seepage or spring flow.

9 PDP, 2013: Cranford Basin spring identification. Report for Christchurch City Council. Report Reference: CO2771502, September 2013.

10 White, P.A., Weeber, J.H., Pamer, R., Minni, G. and Cave, S., 2007 Identification of Springston Formation Gravel Lobes in the Christchurch Formation, GNS Science Consultancy Report 2007/195, October 2007.

Below the silt and peat layer(s) are deposits of gravels and sands that are associated with former channels and flood deposits of the Waimakariri River (i.e. Springston gravel lobes). A review of bore logs and the interpretation of the drilling logs discussed in Section 7 indicate that the extent of these deposits varies in thickness and lateral extent. Groundwater contained in these deposits exhibits a positive vertical hydraulic gradient, with static water level measured above ground or just below ground level in the four monitoring wells screened in the lower alluvium. There were no monitoring wells installed as part of this investigation into the Riccarton Gravels. Therefore, no conclusions could be reached regarding the likely degree of hydraulic difference between the water bearing units in the Springston deposits versus the Riccarton Gravel aquifer.

The artesian pressures observed in the monitoring wells indicate a potential for groundwater to flow through zones of weakness in the overlying deposits (i.e. peat deposits and thin silt/sand deposits) to discharge as springs. PDP (2013)⁹ mapped several springs in the basin area. Many of the springs mapped by PDP⁹ (2013) were characterised as CCC drainage springs, with three springs specifically noted as permanent springs (and have an associated ECan spring identification number). Two new springs were identified post the Canterbury earthquakes to the north of Cranford Basin (Aqualinc, 2011)¹¹. There are no further details of the characteristics of the new springs available. Thorley (2015)¹² presented the results of field investigations of the seepage and artesian springs in the Cranford Basin as part of the Notice of Requirement (NoR) for the Northern Arterial Extension hearing.

Appendix 8 of Thorley (2015)¹² describes the nature of the springs and seeps mapped in the Cranford Basin. The majority of the springs were characterised as seepage in shallow depressions within the peat deposits. Some of the seeps are drained via channels which were installed by land owners.

The three permanent springs identified on the Environment Canterbury database had notable flow according to Thorley (2015)¹² (Table 8).

Table 8 - Springs in the Cranford Basin noted on ECan GIS

Spring No.	Type	Flow	Comments
M35/8136	Artesian	>20L/s	Large pool area with a depth of > 1 m bgl
M35/8128	Seepage	Variable	Depth of 0.7m enhanced with drainage
M35/8139	Artesian	Strong	Shallow depression with fast flowing discharge containing silt, gravels, and organic material. Drain is cut to take flow away. Comments from Thorley (2015) note that a hard ruler was inserted into the spring up to 1 m without refusal.

In addition to the mapped springs, there were examples of standpipes of unknown depth intercepting artesian groundwater conditions, which were either capped or partially capped.

In summary based on the geological conceptual model of the site, any excavation that extends into the peat and silts could result in the ingress of groundwater under artesian pressure, even if

11 Aqualinc Research Limited, 2011: Earthquake Related Springs February 2011. Prepared for The Earthquake Commission. Aqualinc Research Limited Report No. C110669

12 Thorley, M., 2015: Statement of evidence of Michael J Thorley for Christchurch City Council and New Zealand Transport Agency (8 April 2015). Notice of Requirement by CCC and NZTA for designations for Northern Arterial, Northern Arterial Extension and Cranford Street upgrade.

the silt layer has not been breached. It is likely that under such circumstances the inflow of groundwater to the excavation would be persistent unless it was capped. Piling through the peat and silt layer for foundations (as discussed in Section 10 below) will need to be mindful of creating a zone of weakness in the confining layer, resulting in new seepage or spring flows.

10. Geotechnical Assessment

The ground conditions show some natural variations across the site. However, the determining factor for foundation design at the site is the presence of significant organic soils and peat that is encountered across the whole site. Therefore the shallow soils do not meet the classification of 'good ground' in accordance with NZS 3604 due to the presence of soft soils and potentially compressible organic material.

Liquefaction analysis of relevant CPTs has indicated liquefaction induced settlement for most of this area as equivalent to TC2 land, with some CPT's indicating TC2/TC3 and TC3 land. TC2 consistent ground conditions for this zone are considered appropriate as minimal liquefaction has been observed following the Canterbury earthquake sequence.

10.1 Organic Material Development Constraints

The organic material identified onsite (peat and organics silts) can cause a number of issues for building foundations. Consolidation of organic can be separated into several phases with different lifespans.

Initial consolidation begins as soon as the soil is loaded, by loading the soil the void spaces are reduced and water is expelled from the soil. Initial settlement occurs for a finite period of time until the load has been equalised, further load is required to compress more.

Long term consolidation from decomposition of the organic material has the potential to occur for the life of the structure. The organic materials mass is reduced as bacteria breakdown the material.

Water fluctuation consolidation typically occurs when water is removed from the organic material. Nearby excavations of foundations or infrastructure trenches that require dewatering are a common cause of ground water fluctuations that cause settlement.

10.1.1 Consolidation Analysis

Potential consolidation of shallow foundations was analysed from the one-dimensional consolidation testing of the undisturbed soil samples. Loads were assumed from a residential building with a TC2 type foundation (gravel raft and with concrete slab on grade) with lightweight roof and lightweight cladding. A conservative load of 12 kPa was assumed for the building type as described previously. A typical soil profile was prepared for the consolidation analysis where the thickness of the organic material was varied from 0.5 to 1.0m. Potential consolidation was analysed to be in the range of 15 to 45 mm. The majority of consolidation occurred in the organic SILT layer.

10.2 Potential Foundation Types

This area is well known to contain peat and organic layers. The previous desktop study identified the potential of these layers to be present in layers up to 5 m thick. Further investigation was undertaken to provide undisturbed samples for one-dimensional consolidation tests with resulting settlements of 15 to 45 mm. Therefore new foundations in this area will require site specific geotechnical investigations and specific engineering design

Foundations for new residential houses need to be designed to mitigate settlement and consolidation from both organic and liquefiable materials. To mitigate against settlement and consolidation it is recommended that residential building foundations are piled through the very soft soils and organic material. The required piling depth will vary, it is likely that the lower alluvium will provide a suitable strata for pile bearing and embedment, therefore piling depths could range from 5-7 m bgl.

The potential consolidation of the organic material under a shallow foundation is likely to be greater than 25 mm. A 25 mm limiting maximum settlement was suggested by Terzaghi and Peck¹³ (1967) that most ordinary structures can withstand. Although shallow foundations can be designed to “float” above the peat this cannot mitigate the long term settlement (total or differential). Differential settlement can cause damage to foundations and service connections. Therefore we do not consider shallow foundation as an appropriate standard solution.

Shallow foundations maybe appropriate for small areas of the site that are identified with higher density intrusive investigations as having no or minimal organic material (combined less than ~300 mm thickness).

10.3 Housing Density

The chosen density of residential development will not influence piled foundation design. Should further investigations identify areas suitable for shallow foundations high density housing will cause increased consolidation effects on foundations.

10.4 Development Considerations and Risks

Services in this area will likely have to be constructed in ground with an allowable bearing capacity less than 50 kPa, therefore a ‘soft ground’ raft would be required.

Any trenching or excavations deeper than ~1 m bgl will most likely require dewatering. Dewatering of organic material can cause settlement and consolidation of adjacent land. Excavations requiring dewatering need an approved temporary earthworks plan and it is recommended a dilapidation survey is undertaken of any nearby structures prior to works beginning.

The area around 117 Philpotts Road is likely to have similar ground conditions to the remainder of the site however there is no nearby geotechnical investigation to confirm this. GHD was unable to obtain access to this site to undertake intrusive investigations.

¹³ Terzahi, K. and Beck, R. B., 1967, Soil Mechanics in Engineering Practice, 2nd ed.; John Wiley, New York.

11. Summary

GHD has been engaged by the Christchurch City Council to undertake a geotechnical study for the proposed development of Cranford Basin. The development involves the potential rezoning of residential houses around some of the perimeter of the Cranford Basin.

The proposed site is an area that is well known to be underlain by swamp derived deposits comprising soft silts, organic silts and peat. From the investigations available from ECan well database, the CGD, and our further investigations the site has been determined to comprise alluvium, underlain by swamp derived deposits. This is further underlain by alluvium, underlain by the Riccarton Gravels. The shallow soils do not meet the classification of 'good ground' in accordance with NZS 3604 due to the presence of soft soils and potentially compressible organic material.

Groundwater was encountered at shallow depths within the upper alluvium and silt and peat layers. The lower alluvial material is water bearing and contains gravel lenses which exhibit artesian pressures. Springs were identified across the site by PDP (2013) and Thorley (2015), many of which are characterised as shallow depression seeps within the peat/organic material. These seeps are drained to CCC drainage networks. Three artesian springs are shown on Environment Canterbury well database, which were noted as having strong and permanent flows. Excavations are likely to encounter groundwater, with deeper excavations at risk of breaching the confining material (silt) which separates the lower alluvial gravel from the surface. Piling through the confining material will need to account for potential for increasing discharge of groundwater from the lower alluvial Springston gravel as seeps/springs.

A brief search of the Environment Canterbury List Land Use Register identified several properties have HAIL activities. If the land use is to be changed from its current land use to residential land use it is recommended a Preliminary Site Investigation and subsequent Detailed Site Investigation are undertaken.

Foundations for new residential houses need to be designed to mitigate settlement and consolidation from both swamp deposits and liquefiable materials. The greatest consolidation will result from settlement of the organic soils and there bio-gradation. Therefore design and construction of new foundations of this area will require site specific geotechnical investigations and specific engineering design.

To mitigate against settlement and consolidation it is recommended that residential building foundations are piled through the very soft soils and organic material. The required piling depth will vary, it is likely that the lower alluvium will provide a suitable strata for pile bearing and embedment, therefore piling depths could range from 5-7 m bgl.

The potential consolidation of the organic material under a shallow foundation is likely to be greater than 25 mm, therefore shallow foundations are not considered appropriate for this site. Shallow foundations maybe appropriate for small areas of the site that are identified with further investigation as having no or minimal organic material.

12. Scope and limitations

This report: has been prepared by GHD for Christchurch City Council and may only be used and relied on by Christchurch City Council for the purpose agreed between GHD and the Christchurch City Council as set out in section 1.1 of this report.

GHD otherwise disclaims responsibility to any person other than Christchurch City Council arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

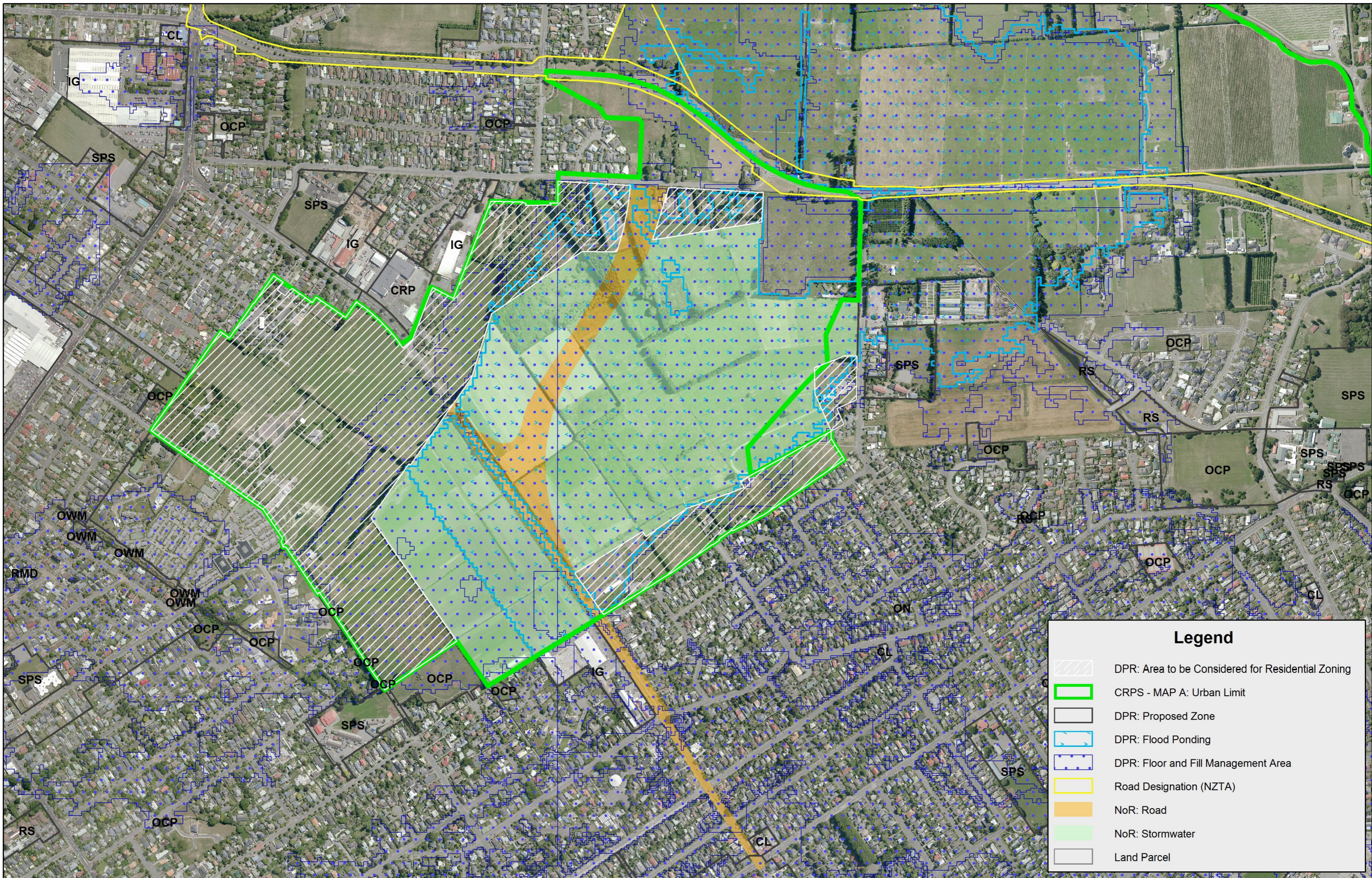
The opinions, conclusions and any recommendations in this report are based on information obtained from, and testing undertaken at or in connection with, specific sample points. Site conditions at other parts of the site may be different from the site conditions found at the specific sample points.

Investigations undertaken in respect of this report are constrained by the particular site conditions, such as the location of buildings, services and vegetation. As a result, not all relevant site features and conditions may have been identified in this report.










Site conditions (including the presence of hazardous substances and/or site contamination) may change after the date of this report. GHD does not accept responsibility arising from, or in connection with, any change to the site conditions. GHD is also not responsible for updating this report if the site conditions change.

Appendices

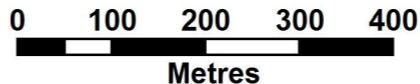
Appendix A – (Location Plan)



Legend

-  DPR: Area to be Considered for Residential Zoning
-  CRPS - MAP A: Urban Limit
-  DPR: Proposed Zone
-  DPR: Flood Ponding
-  DPR: Floor and Fill Management Area
-  Road Designation (NZTA)
-  NoR: Road
-  NoR: Stormwater
-  Land Parcel

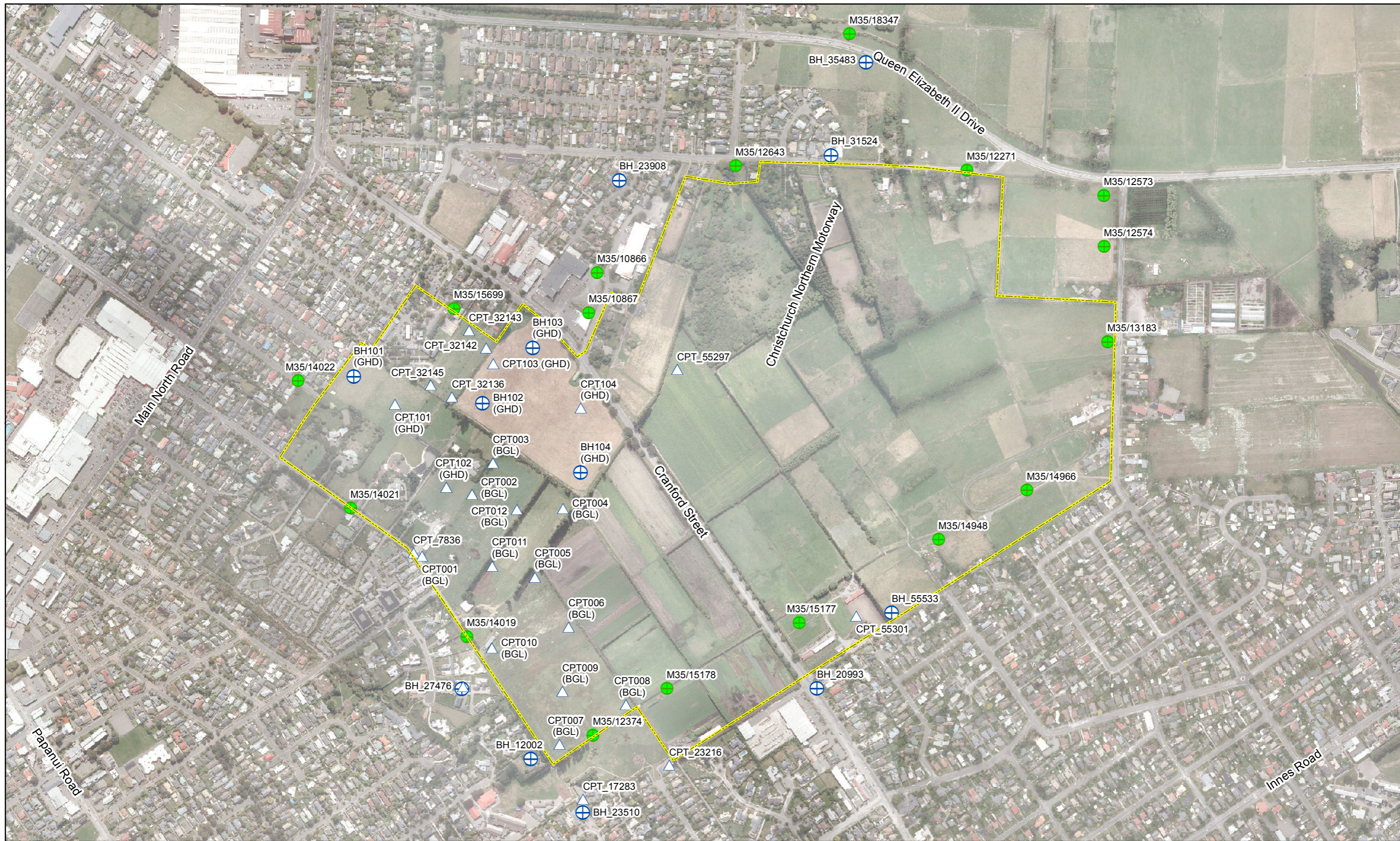
Draft Papanui / Cranford Basin Planning Constraint Map



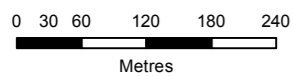
Appendix B – (Existing Investigation Logs)

Environment Canterbury Borehole Logs

Canterbury Geotechnical Database Investigation Logs

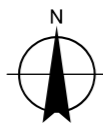






Scale: 1:7,000 (at Paper Size A3)



Map Projection: Transverse Mercator
Horizontal Datum: NZGD 2000

Grid: NZGD 2000 New Zealand Transverse Mercator



-  Borehole
-  CPT
-  Ecan
-  Cranford Basin



**Christchurch
City Council**



Christchurch City Council
Cranford Basin Geotechnical
Investigation and Report

GeoTech Plan

Job Number | 51-33038
Revision | A
Date | 04 Sep 2015

Unknown No: M35/15178

Well Name: CCC BorelogID 4314

Owner: CCC borelog



Street of Well: Dudley Creek

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69647-83869 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569647 - 5183869

Location Description: Dudley Creek Diversion -
200m west of Cranford St

Uses: Geotechnical / Geological
Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date:

Water Level Count: 0

Well Depth: 6.00m -GL

Strata Layers: 2

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.78m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
------------	-------------	---------	------------	---------------	--------------------	----------------	------------------

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
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Aquifer test date(s) where this is an observation bore

Borelog for well M35/15178

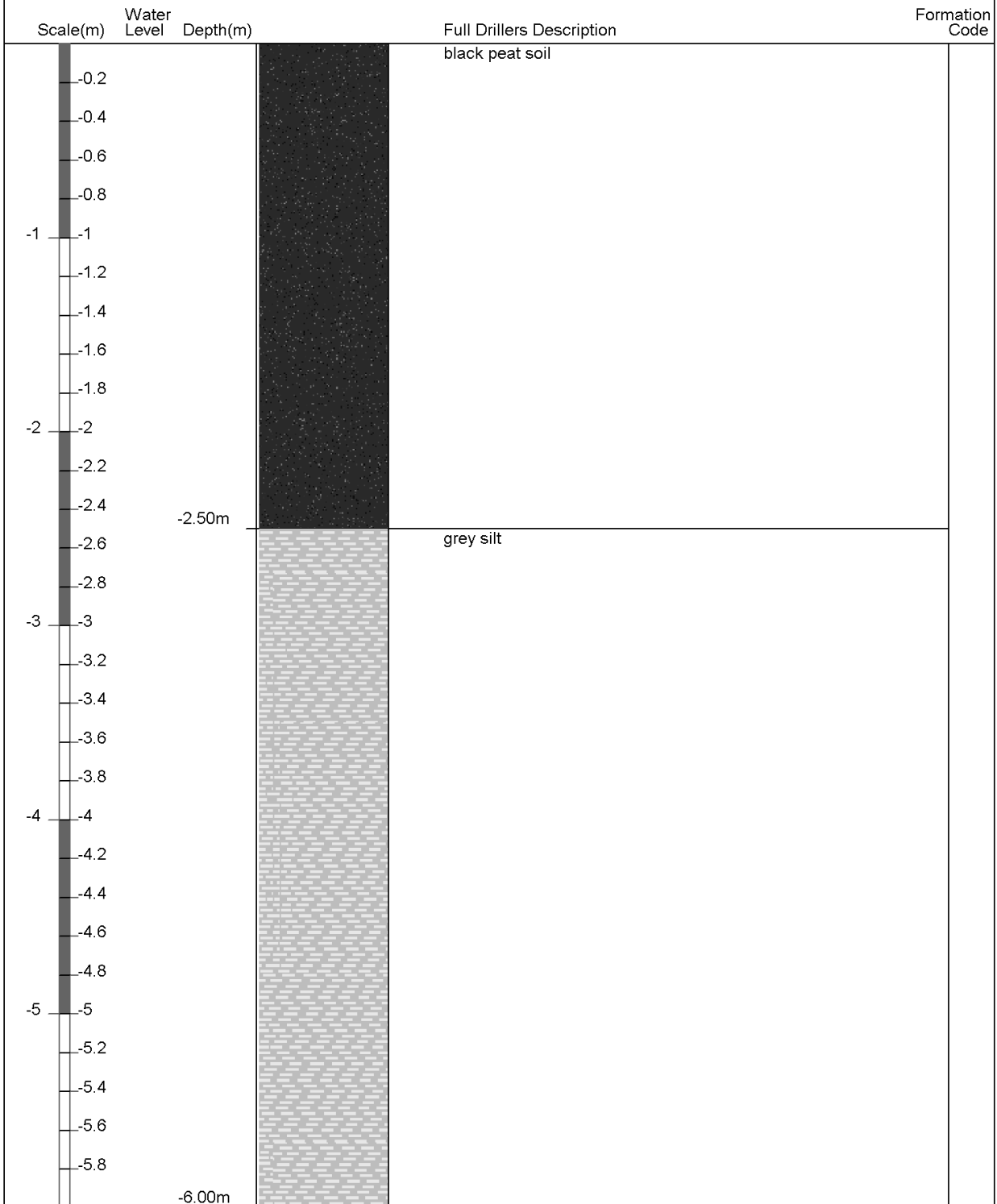
Gridref: M35:79648-45483 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.78 +MSD

Well name : CCC BorelogID 4314

Drill Method : Not Recorded

Drill Depth : -6m Drill Date :



Bore or Well No: M35/1646

Well Name:

Owner: HARRISON, J.



Street of Well: CRANFORD ST

File No:

Locality: PAPANUI

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69699-84386 QAR 4

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569699 - 5184386

Location Description:

Uses:

ECan Monitoring:

Well Status: Not Used

Drill Date: 28 Feb 1972

Water Level Count: 0

Well Depth: 25.40m -GL

Strata Layers: 10

Initial Water Depth: 3.70m -MP

Aquifer Tests: 0

Diameter: 152mm

Yield/Drawdown Tests: 1

Measuring Point Ait: 5.00m MSD QAR 3

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller: A M Bisley & Co

Calc. Min. (Below MP): -0.20m -MP

Drilling Method: Cable Tool

Last Updated: 08 Nov 2013

Casing Material:

Last Field Check:

Pump Type: Unknown

Yield: 19 l/s

Aquifer Type: Flowing Artesian

Drawdown: 3 m

Aquifer Name: Riccarton Gravel

Specific Capacity: 6.33 l/s/m

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
1	Galvanised (Nold)	22.3	25.3				

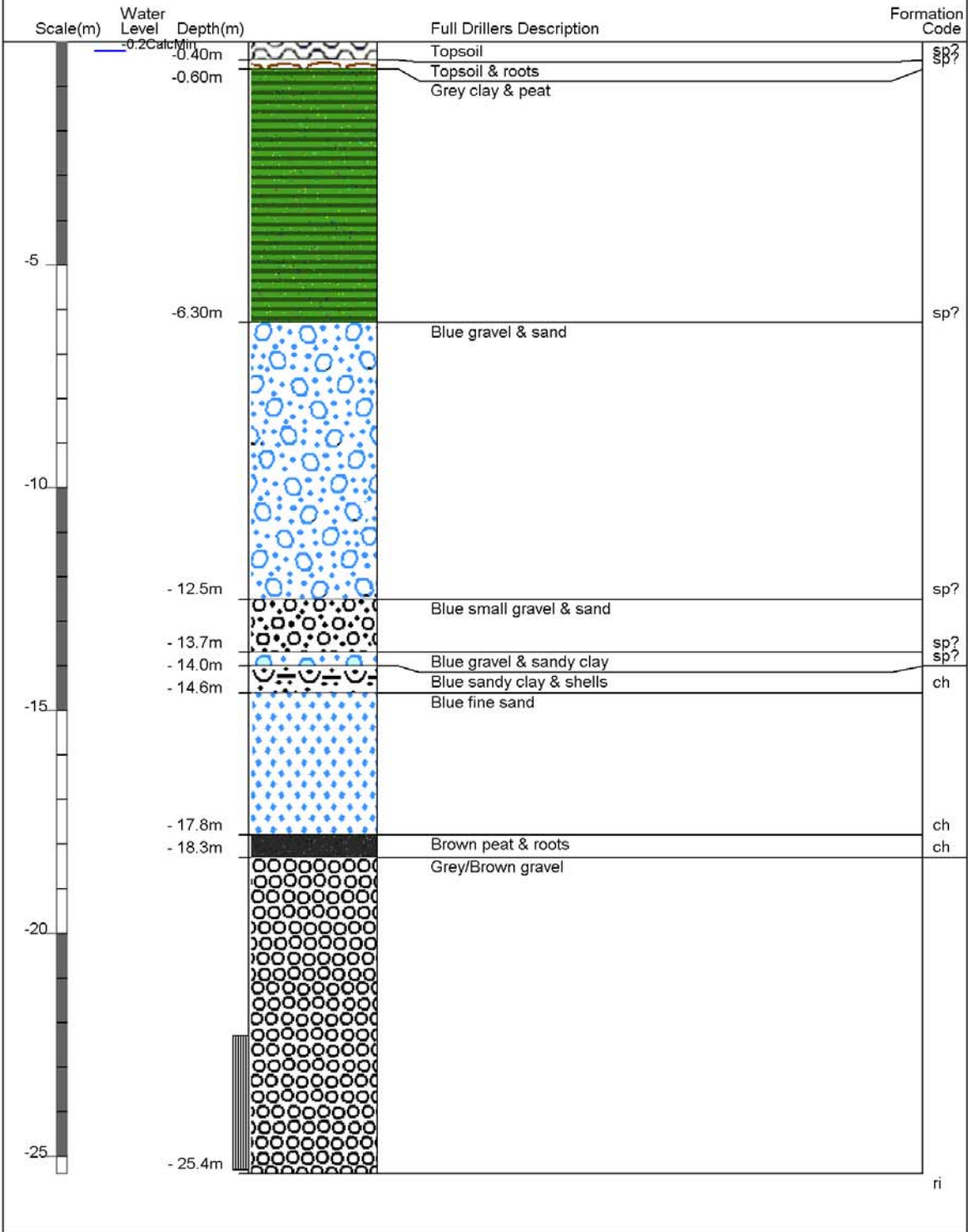
Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
28 Feb 1972	1	19	3	

Aquifer test date(s) where this is an observation bore

Borelog for well M35/1646

Gridref: M35:797-460 Accuracy : 4 (1=high, 5=low)
 Ground Level Altitude : 5 +MSD
 Driller : A M Bisley & Co
 Drill Method : Cable Tool
 Drill Depth : -25.4m Drill Date : 28/02/1972



Unknown No: M35/15178

Well Name: CCC BorelogID 4314

Owner: CCC borelog



Street of Well: Dudley Creek

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69647-83869 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569647 - 5183869

Location Description: Dudley Creek Diversion -
200m west of Cranford St

Uses: Geotechnical / Geological
Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date:

Water Level Count: 0

Well Depth: 6.00m -GL

Strata Layers: 2

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.78m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

Borelog for well M35/15178

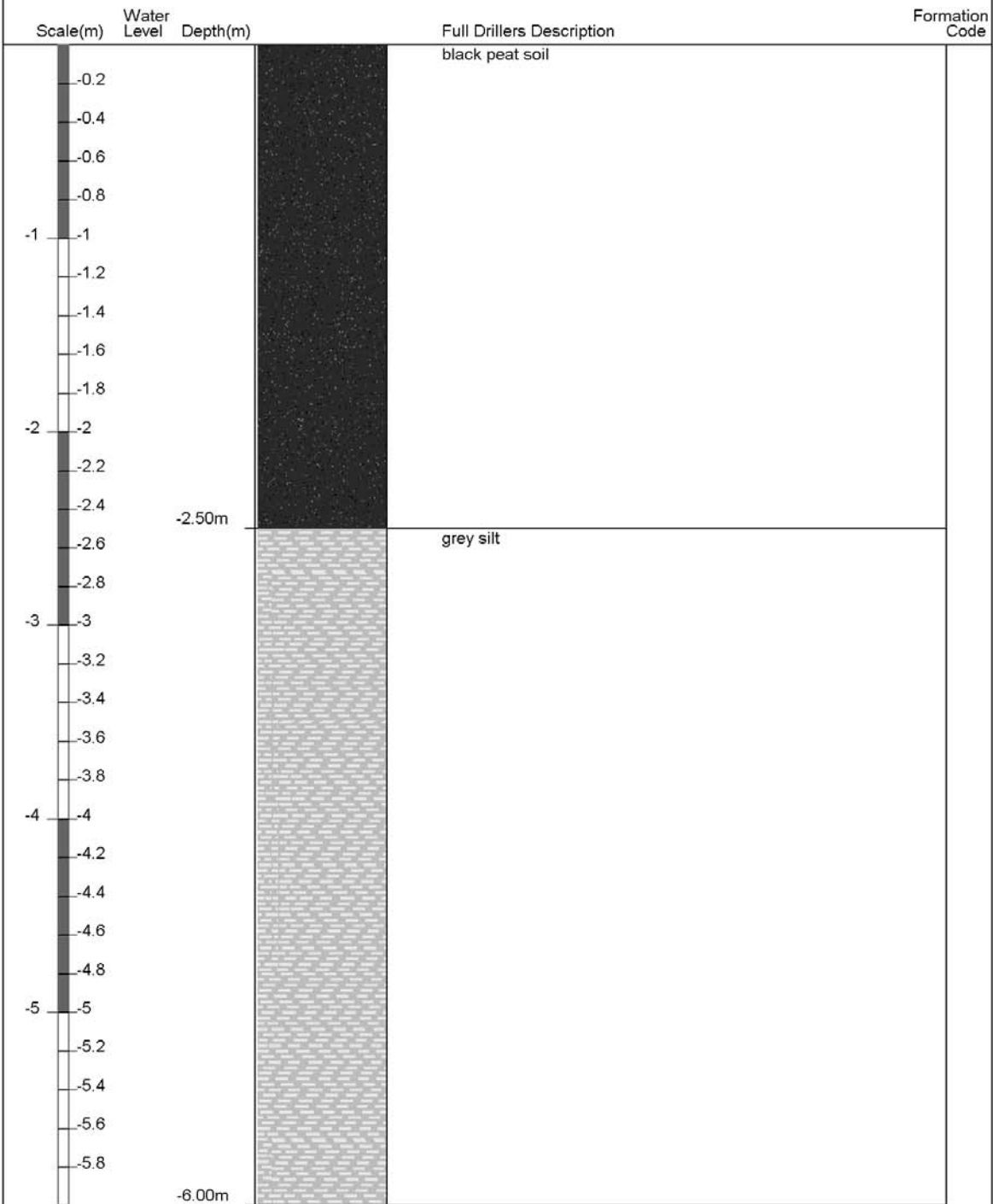
Gridref: M35:79648-45483 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.78 +MSD

Well name : CCC BorelogID 4314

Drill Method : Not Recorded

Drill Depth : -6m Drill Date :



Unknown No: M35/15177

Well Name: CCC BorelogID 4313

Owner: CCC borelog



Street of Well: Dudley Creek

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69914-84004 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569914 - 5184004

Location Description: Dudley Creek Diversion -
100m east of Cranford St

Uses: Geotechnical / Geological
Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date:

Water Level Count: 0

Well Depth: 6.00m -GL

Strata Layers: 2

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.63m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
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Aquifer test date(s) where this is an observation bore

Borelog for well M35/15177

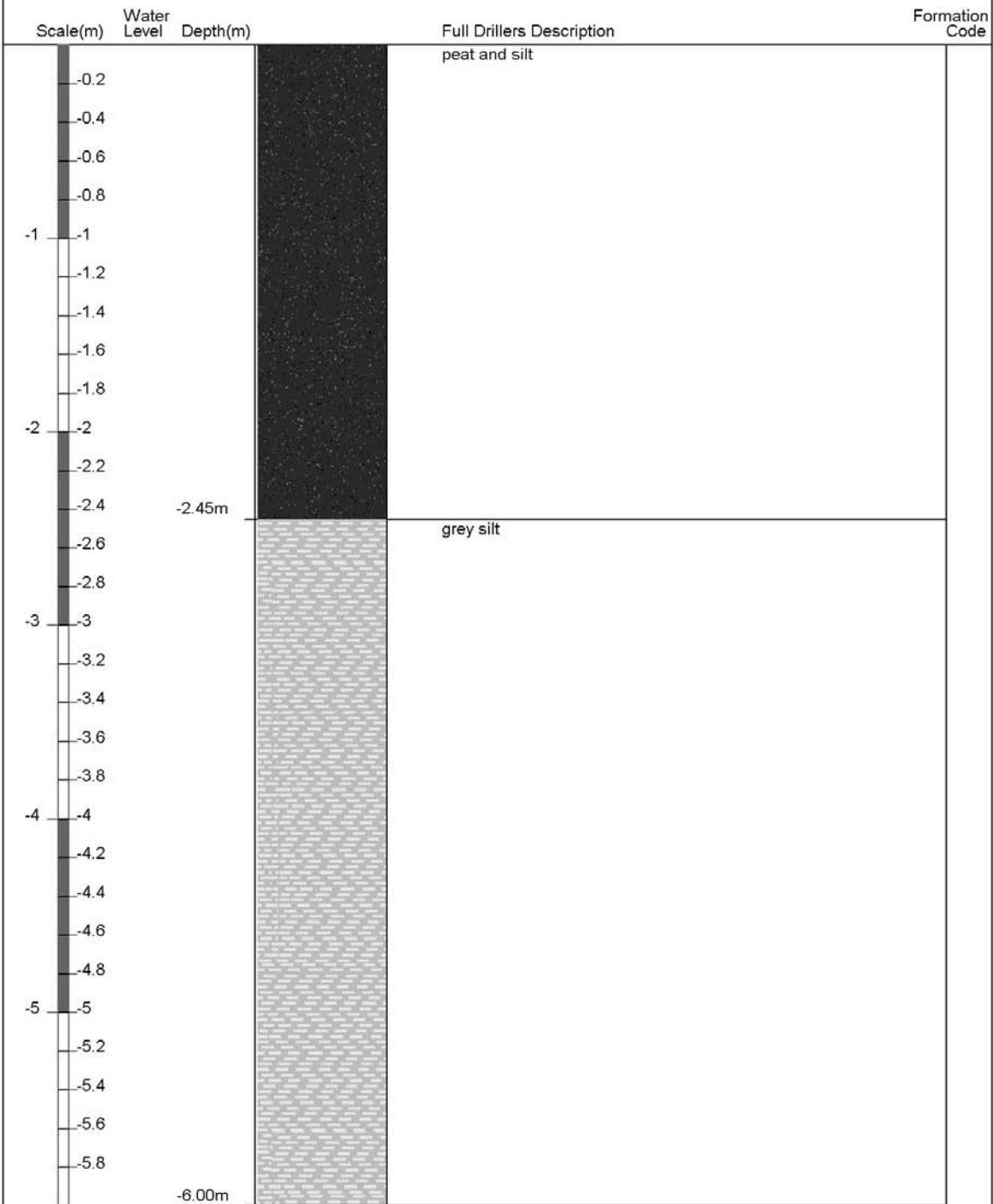
Gridref: M35:79915-45618 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.63 +MSD

Well name : CCC BorelogID 4313

Drill Method : Not Recorded

Drill Depth : -6m Drill Date :



Unknown No: M35/14966

Well Name: CCC BorelogID 3961

Owner: CCC borelog



Street of Well: Philpotts Rd

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:70375-84268 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1570375 - 5184268

Location Description: Philpotts Rd - in paddock west of road about 200m west of road bend ag

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date:

Water Level Count: 0

Well Depth: 3.90m -GL

Strata Layers: 4

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.42m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

Borelog for well M35/14966

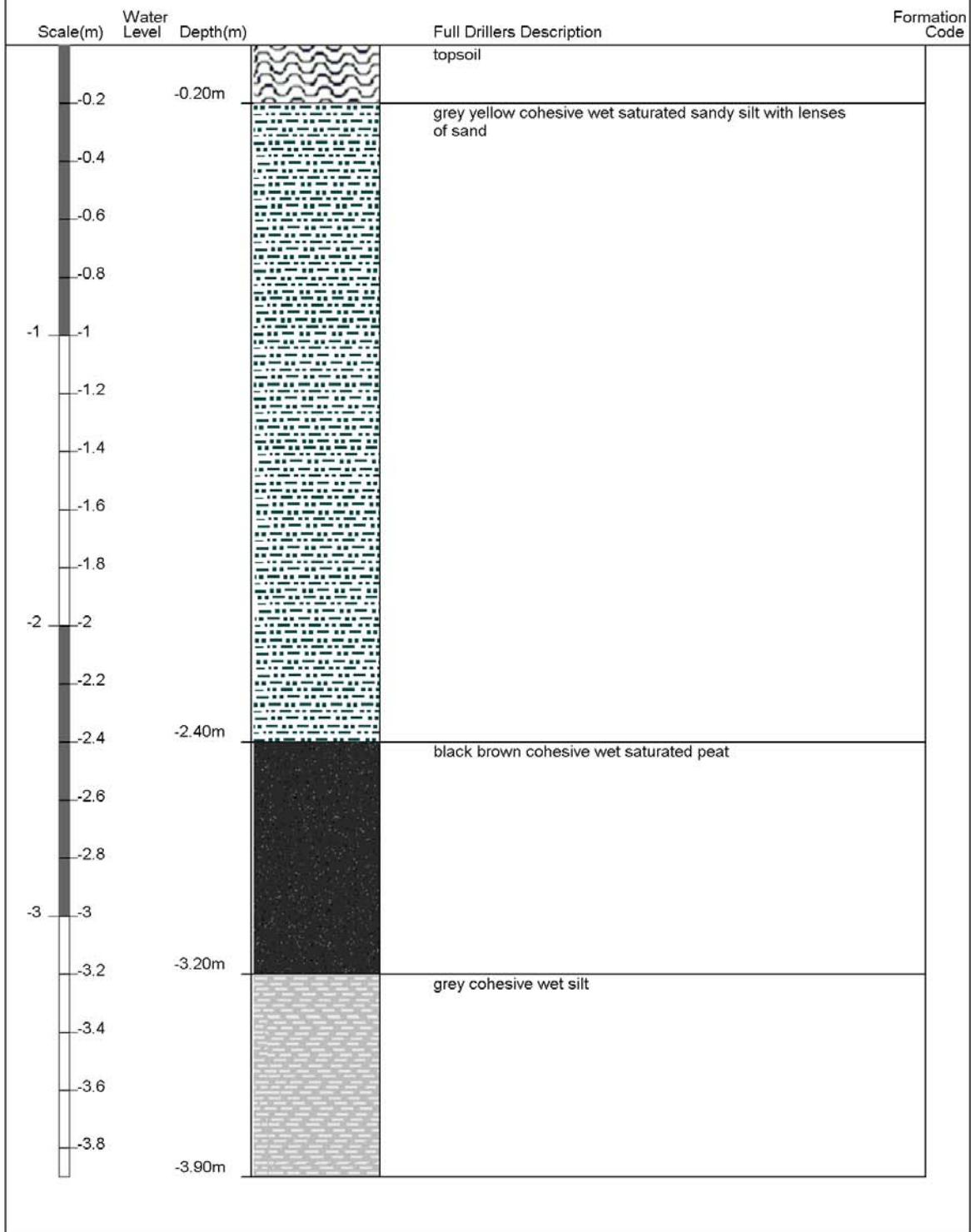
Gridref: M35:80376-45882 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.42 +MSD

Well name : CCC BorelogID 3961

Drill Method : Not Recorded

Drill Depth : -3.9m Drill Date :



Unknown No: M35/14948

Well Name: CCC BorelogID 3943

Owner: CCC borelog



Street of Well: Croziers Rd -

Locality:

NZTM Grid Reference: BX24:70187-84160 QAR 3

NZTM X-Y: 1570187 - 5184160

Location Description: Croziers Rd - in
MWD/Crozier Property 420m
northwest of Croziers Rd an

ECan Monitoring:

Well Status: Filled in

File No:

Allocation Zone: Christchurch/West Melton

CWMS Zone: Christchurch - West Melton

Uses: Geotechnical / Geological
Investigation

Drill Date: 05 Jul 1987

Well Depth: 3.00m -GL

Initial Water Depth:

Diameter:

Measuring Point Ait: 8.47m MSD QAR 4

GL Around Well: 0.00m -MP

MP Description:

Driller:

Drilling Method:

Casing Material:

Pump Type:

Yield:

Drawdown:

Specific Capacity:

Water Level Count: 0

Strata Layers: 2

Aquifer Tests: 0

Yield/Drawdown Tests: 0

Highest GW Level:

Lowest GW Level:

First Reading:

Last Reading:

Calc. Min. (Below MP):

Last Updated: 27 Mar 2008

Last Field Check:

Aquifer Type:

Aquifer Name:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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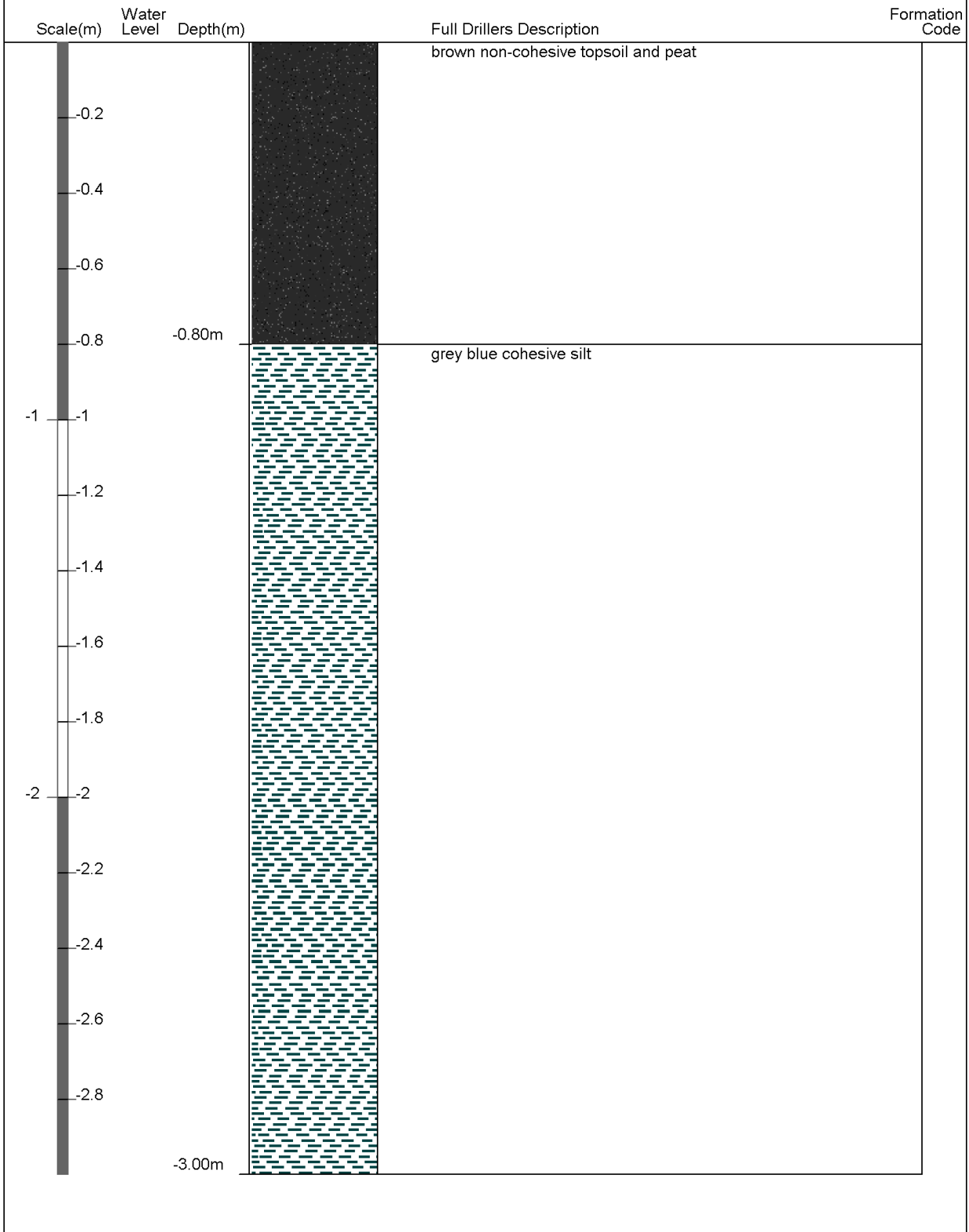
Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
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Aquifer test date(s) where this is an observation bore

Borelog for well M35/14948

Gridref: M35:80188-45774 Accuracy : 3 (1=high, 5=low)
Ground Level Altitude : 8.47 +MSD
Well name : CCC BorelogID 3943
Drill Method : Not Recorded
Drill Depth : -3m Drill Date : 5/07/1987



Unknown No: M35/14021

Well Name: CCC BorelogID 2525

Owner: CCC borelog



Street of Well: Grassmere St

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69013-84235 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569013 - 5184235

Location Description: Grassmere St - 320m northwest of angle

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 01 Jan 1959

Water Level Count: 0

Well Depth: 7.32m -GL

Strata Layers: 3

Initial Water Depth: -1.42m -MP

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 10.28m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

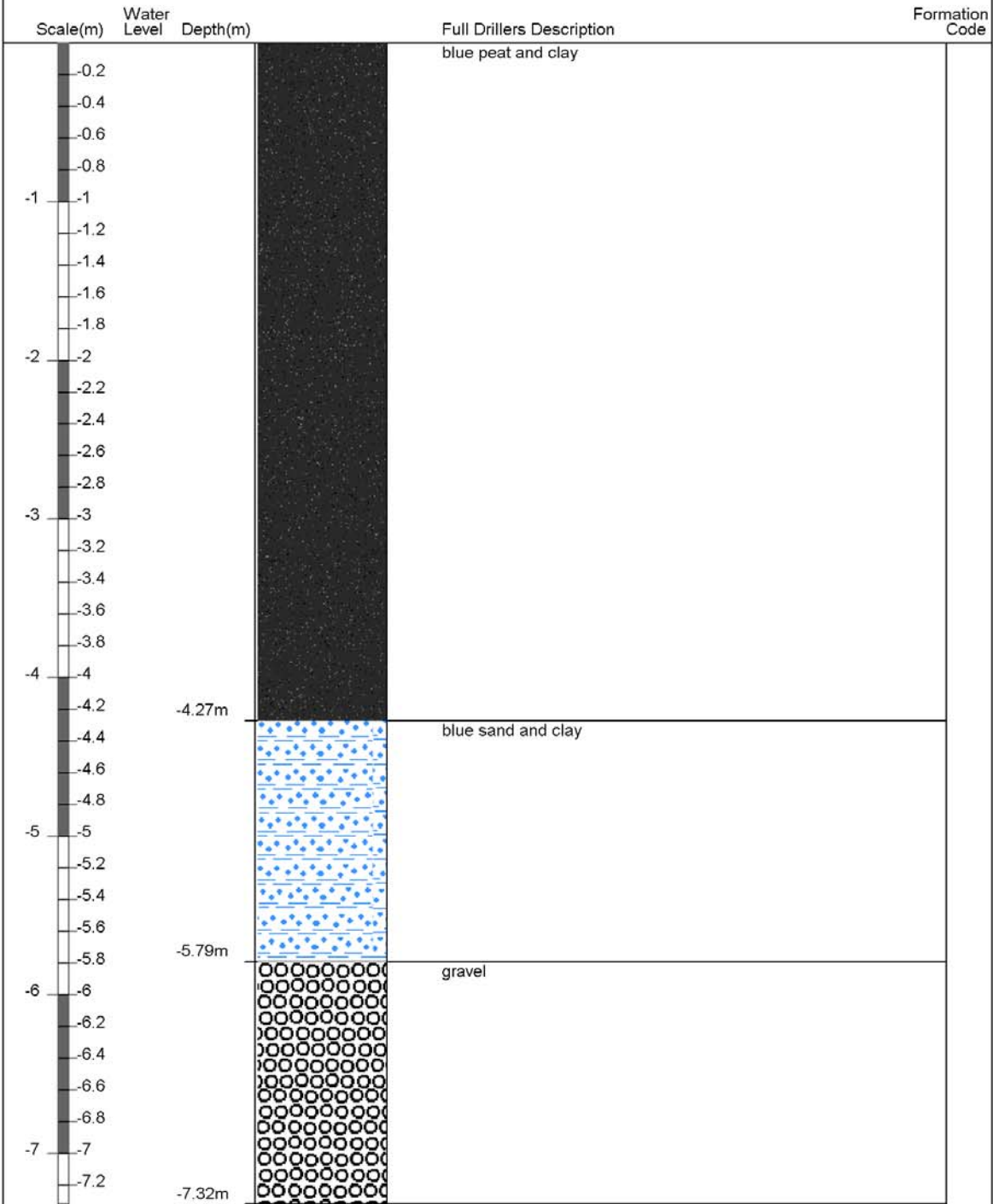
Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

Borelog for well M35/14021

Gridref: M35:79013-45849 Accuracy : 3 (1=high, 5=low)
Ground Level Altitude : 10.28 +MSD
Well name : CCC BorelogID 2525
Drill Method : Not Recorded
Drill Depth : -7.32m Drill Date : 1/01/1959



Unknown No: M35/14019

Well Name: CCC BorelogID 2523

Owner: CCC borelog



Street of Well: Grassmere St

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69246-83977 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569246 - 5183977

Location Description: Grassmere St - 140m southeast of Grants Rd

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 01 Jan 1959

Water Level Count: 0

Well Depth: 5.18m -GL

Strata Layers: 4

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 9.29m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

Borelog for well M35/14019

Map Reference (NZMG): 2479246 mN, 5745591 mE

QAR Accuracy: 3

Ground Level Altitude: 9.3 +MSD

Driller:

Drill Method:

Well Depth: 5.1799982833862m Drill Date: 01/01/1959



Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
1			blue peat and clay	
2				
3		3.05m	blue sand	
4		4.27m	blue sand and clay	
5		4.88m		
		5.18m	brown saturated gravel	
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				
18				
19				
20				
21				
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				

Unknown No: M35/13183

Well Name: CCC BorelogID 1450

Owner: CCC borelog



Street of Well: Philpotts Rd

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:70553-84565 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1570553 - 5184565

Location Description: Philpotts Rd - 300m north of angle - at M.H

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 01 Jan 1956

Water Level Count: 0

Well Depth: 2.99m -GL

Strata Layers: 3

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.53m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
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Aquifer test date(s) where this is an observation bore

Borelog for well M35/13183

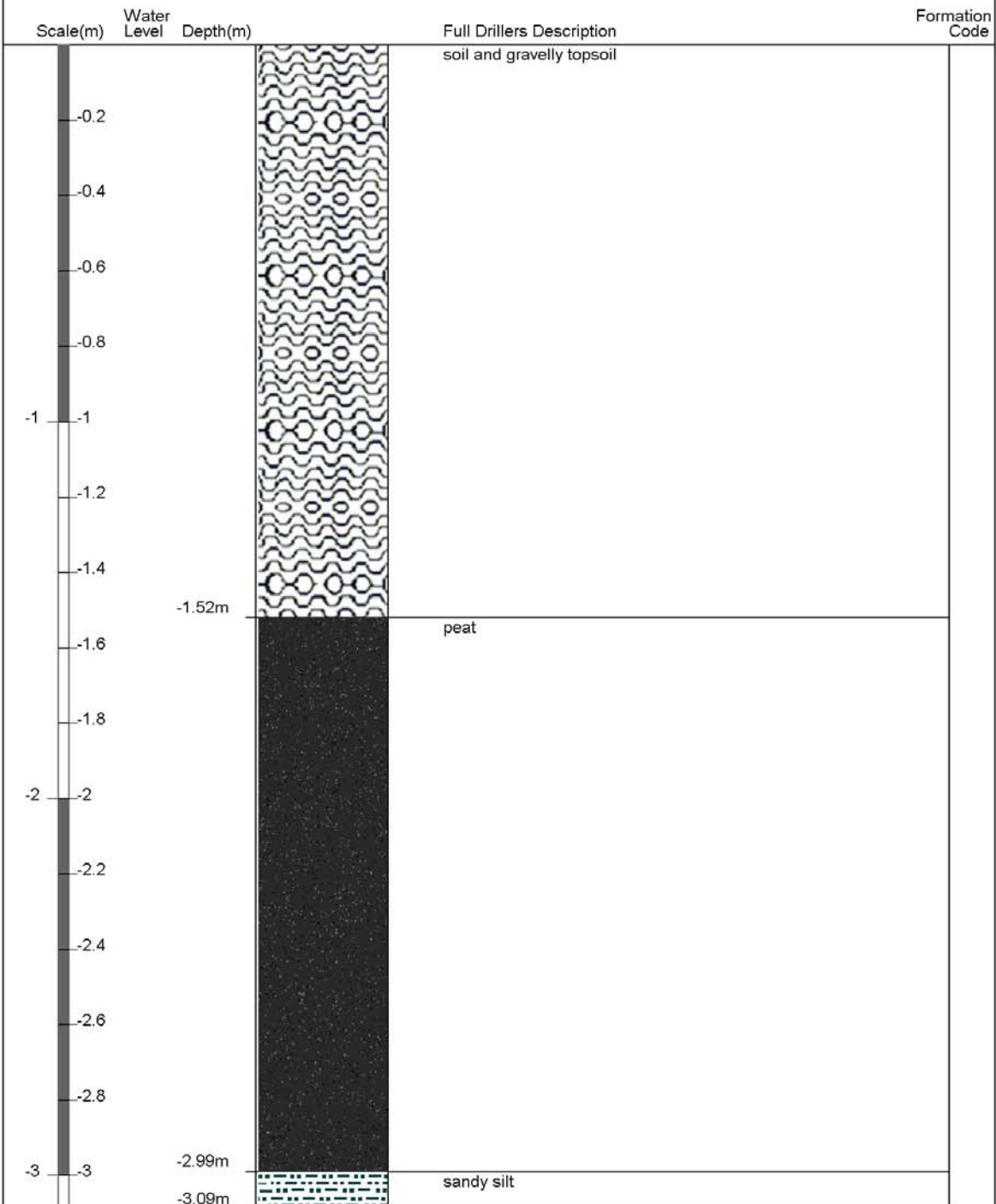
Gridref: M35:80554-46179 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.53 +MSD

Well name : CCC BorelogID 1450

Drill Method : Not Recorded

Drill Depth : -3.09m Drill Date : 1/01/1956



Unknown No: M35/12643

Well Name: CCC BorelogID 769

Owner: CCC borelog



Street of Well: Winters Rd /

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69785-84919 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569785 - 5184919

Location Description: Winters Rd / Grimseys Rd -
at P.S 53 site

Uses: Geotechnical / Geological
Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 08 Jan 1962

Water Level Count: 0

Well Depth: 15.20m -GL

Strata Layers: 9

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 10.72m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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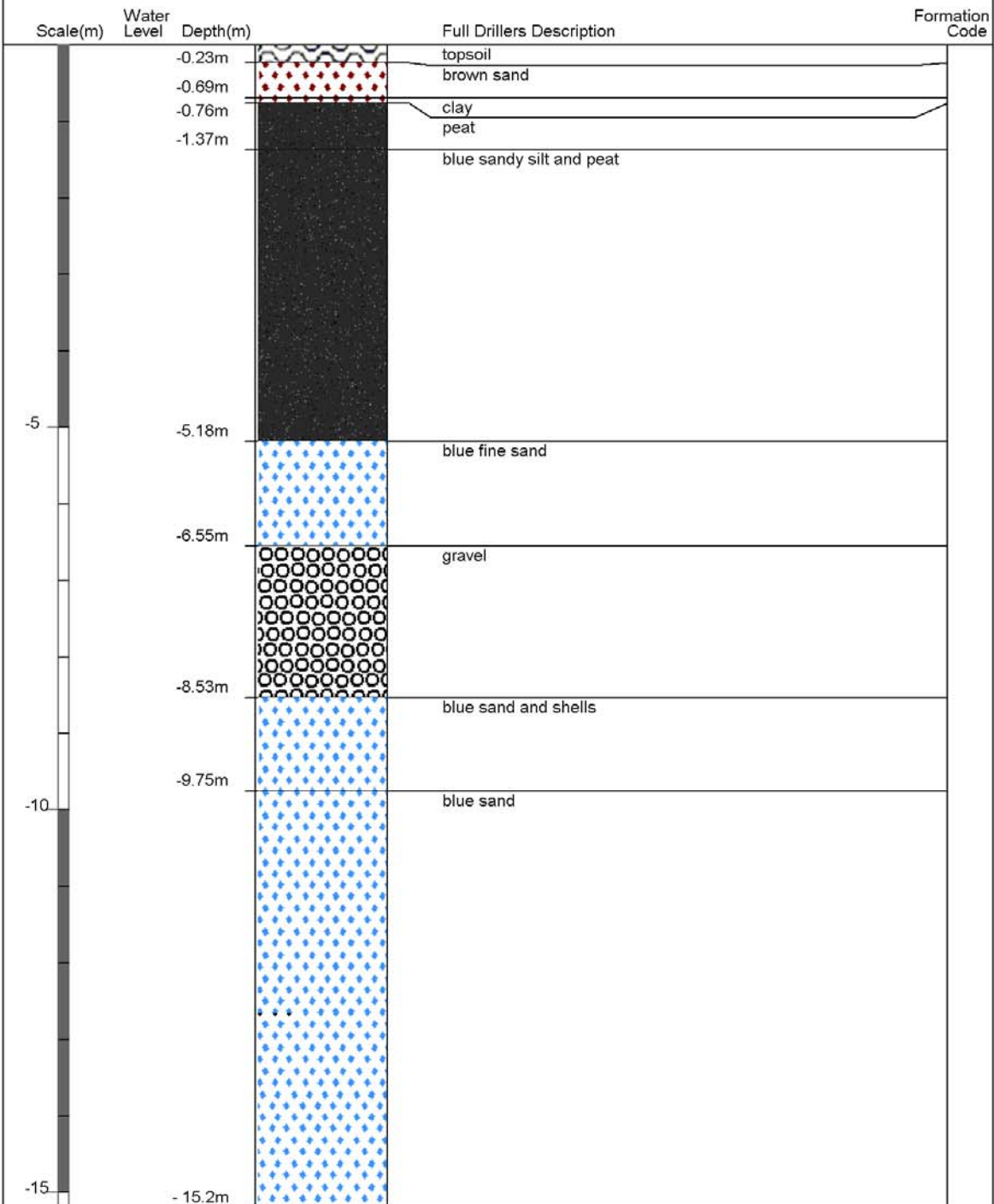
Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
----------------	------	-------------	----------	-----------------

Aquifer test date(s) where this is an observation bore

Borelog for well M35/12643

Gridref: M35:79786-46533 Accuracy : 3 (1=high, 5=low)
 Ground Level Altitude : 10.72 +MSD
 Well name : CCC BorelogID 769
 Drill Method : Not Recorded
 Drill Depth : -15.2m Drill Date : 8/01/1962



Unknown No: M35/12573

Well Name: CCC BorelogID 676

Owner: CCC borelog



Street of Well: Winters Rd /

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:70525-84845 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1570525 - 5184845

Location Description: Winters Rd / Philpotts Rd -
B.H 6 see plan for retention basin

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 09 Apr 1979

Water Level Count: 0

Well Depth: 1.20m -GL

Strata Layers: 3

Initial Water Depth: -0.55m -MP

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 8.68m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

Borelog for well M35/12573

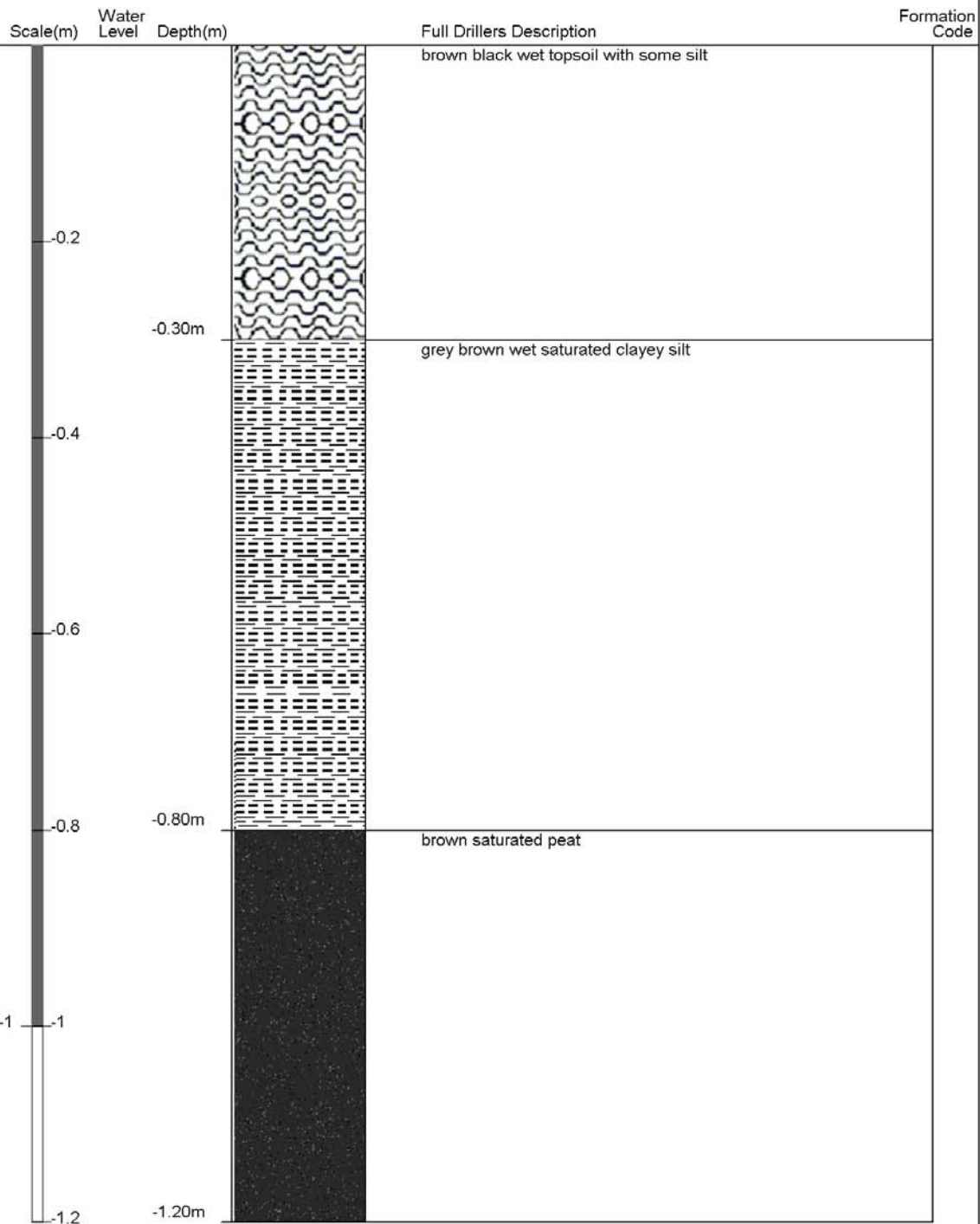
Gridref: M35:80526-46459 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 8.68 +MSD

Well name : CCC BorelogID 676

Drill Method : Not Recorded

Drill Depth : -1.2m Drill Date : 9/04/1979



Bore or Well No: M35/10866

Well Name:

Owner: CRANFORD DEVELOPMENTS LIMITED



Street of Well: 472 CRANFORD STREET

File No: CO6C/23738

Locality: PAPANUI

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69509-84706 QAR 4

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569509 - 5184706

Location Description:

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Active (exist, present)

Drill Date: 02 Aug 2005

Water Level Count: 0

Well Depth: 15.00m -GL

Strata Layers: 4

Initial Water Depth:

Aquifer Tests: 0

Diameter: 125mm

Yield/Drawdown Tests: 0

Measuring Point Ait: 10.86m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller: CWDrill

Calc. Min. (Below MP):

Drilling Method: Concentrics

Last Updated: 08 Apr 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
----------------	------	-------------	----------	-----------------

Date	Comments
26 Jul 2005	Proposed LP location M35:7951-4632

Aquifer test date(s) where this is the pump bore

Aquifer test date(s) where this is an observation bore

Unknown No: M35/15699

Well Name: CCC BorelogID 5002

Owner: CCC borelog



Street of Well:

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:69221-84636 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1569221 - 5184636

Location Description:

Uses: Geotechnical / Geological Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 15 Feb 2005

Water Level Count: 0

Well Depth: 5.20m -GL

Strata Layers: 8

Initial Water Depth: -0.70m -MP

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 11.53m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)
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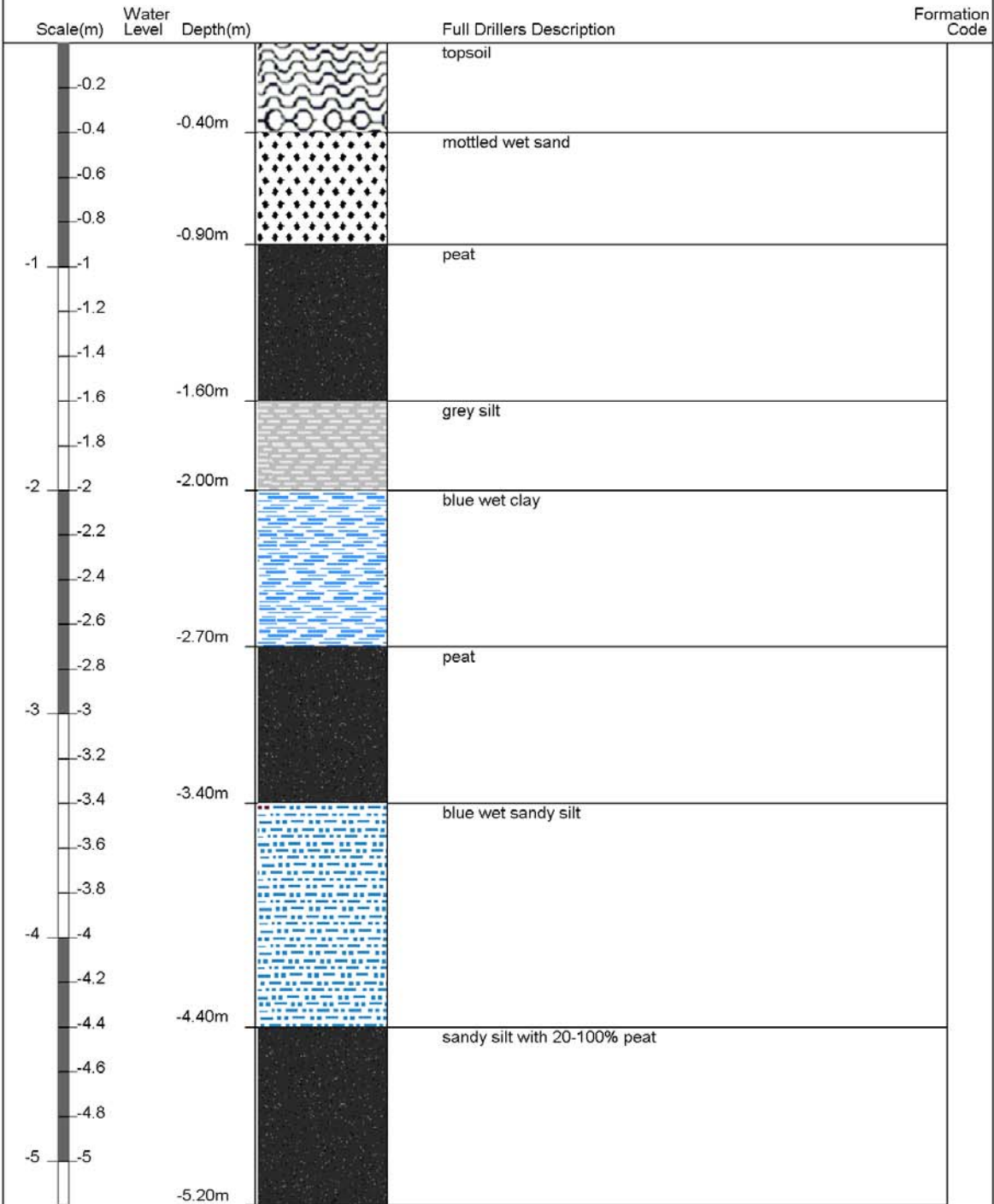
Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)
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Aquifer test date(s) where this is an observation bore

Borelog for well M35/15699

Gridref: M35:79221-46250 Accuracy : 3 (1=high, 5=low)
 Ground Level Altitude : 11.53 +MSD
 Well name : CCC BorelogID 5002
 Drill Method : Not Recorded
 Drill Depth : -5.2m Drill Date : 15/02/2005



Unknown No: M35/14022

Well Name: CCC BorelogID 2526

Owner: CCC borelog



Street of Well: Shearer Ave -

File No:

Locality:

Allocation Zone: Christchurch/West Melton

NZTM Grid Reference: BX24:68906-84489 QAR 3

CWMS Zone: Christchurch - West Melton

NZTM X-Y: 1568906 - 5184489

Location Description: Shearer Ave - 255m
southeast of Main North Rd -
at boundary

Uses: Geotechnical / Geological
Investigation

ECan Monitoring:

Well Status: Filled in

Drill Date: 01 Jan 1959

Water Level Count: 0

Well Depth: 12.19m -GL

Strata Layers: 4

Initial Water Depth:

Aquifer Tests: 0

Diameter:

Yield/Drawdown Tests: 0

Measuring Point Ait: 11.59m MSD QAR 4

Highest GW Level:

GL Around Well: 0.00m -MP

Lowest GW Level:

MP Description:

First Reading:

Last Reading:

Driller:

Calc. Min. (Below MP):

Drilling Method:

Last Updated: 27 Mar 2008

Casing Material:

Last Field Check:

Pump Type:

Yield:

Aquifer Type:

Drawdown:

Aquifer Name:

Specific Capacity:

Screens:

Screen No.	Screen Type	Top (m)	Bottom (m)	Diameter (mm)	Leader Length (mm)	Slot Size (mm)	Slot Length (mm)

Step Tests:

Step Test Date	Step	Yield (l/s)	Drawdown	Duration (mins)

Aquifer test date(s) where this is an observation bore

PROJECT	Northern Arterial Specimen Design	CO-ORD.	E392125 N811604	R.L.	14.63 m	SHEET	1 of 3
LOCATION	Queen Elizabeth II Drive, South Abutment	REF. GRID	Mount Pleasant 2000	DATUM	SCIRT_CCC	DEPTH	21.61 m

GEOLOGY/UNIT	MAIN DESCRIPTION	R.L. (m)	DEPTH (m)	GRAPHIC LOG	TESTS		CORE		DRILLING			ADDITIONAL NOTES	PIEZOMETER DETAILS	OTHER INSTRUMENTATION
					SPT N' VALUE	SPT BLOW COUNTS OR SHEAR VALUE	TOTAL CORE RECOVERY (%)	SAMPLE TYPE	DRILLING METHOD	CASING	BASE OF HOLE & WATER LEVEL			
Springston Formation	SILT with some clay and trace of sand; light brown. Soft, moderate plasticity. Trace of fibrous organic material. Interbedded with: Fibrous PEAT; black. Spongy. Fibrous PEAT; black. Soft, spongy.	0	0	x x x	0	0/0// 0/0/0/0, own weight.	42	HA				a.m. 0.0m 18/06		
	Organic CLAY; light grey. Soft, high plasticity. Trace of fibrous organic material. Fibrous PEAT; brownish black. Soft, spongy.	14	1		0	0/0// 0/0/0/0, own weight.	0	SPT				1310 1.03m 14/06		
	Organic CLAY; brownish grey. Very soft, moderate plasticity. Abundant fibrous organic material. CLAY; grey. Very soft, high plasticity. Abundant fibrous organic material.	12	2				93	Sonic						
	From 3.40 to 3.55m Fibrous PEAT; dark brown. Very soft, plastic.	12	3		0	0/0// 0/0/0/0, own weight.	89	SPT						
	From 3.97 to 4.01m: brown fibrous organic layer, very soft.	12	4				100	Sonic						
	Organic CLAY; brownish grey. Very soft, high plasticity.	10	5		0	0/0// 0/0/0/0, own weight.	111	SPT					LL 78, PL 41, PI 37, WC 280, Org 3	
	CLAY; grey. Soft, high plasticity. Some fibrous organic material.	10	6				73	Sonic						
	Fine to medium SAND with minor silt; grey. Loose, uniformly graded.	6	7		4	1/1// 1/1/1/1	100	SPT					5.96m, light water flow (artesian) 0.7m head	
	At 6.20m: fibrous organic inclusion. From 6.25m: with trace of silt.	8	8				97	Sonic						
	Fine to coarse SAND with trace of silt; grey. 'Very loose', well graded.	8	7		20	2/3// 4/5/5/6	100	SPT					1.2m heave	
At 7.48m: becomes medium dense with trace of shell fragments.	8	8				73	Sonic							
Fine to medium SAND with minor silt; grey. 'Medium dense', well graded. Trace of fibrous organic material.	6	9		18	2/3// 4/4/6/4	100	SPT					SWL 1.03m, casing depth 9.00m 3.1m heave		
Fine to coarse SAND with trace of silt; grey. 'Medium dense', well graded. Trace of shell fragments.	9	9				93	Sonic							
From 9.85 to 9.90m: SILT; grey, mottled brown. Firm, low plasticity.			x x											

NOTES Refer to Site Plans for Location. Safety auto trip hammer #397 used (energy ratio 102%). LOGGED IN ACCORDANCE WITH NZ GEOTECHNICAL SOCIETY GUIDELINES (2005) SEE ATTACHED KEY SHEET FOR EXPLANATION OF SYMBOLS	STARTED	14/06/2013	FINISHED	18/06/2013
	INCLINATION/ AZIMUTH	Vertical; n/a	DRILLING Co.	McMillan Drilling
	LOGGED	F Neeson / S Cooke	DRILLING RIG	Geoprobe 8140LC
	CHECKED	S Cooke	DRILLER	D Berger
	CLIENT	NZ Transport Agency	PROJECT No.	6-DC716.52

PROJECT	Northern Arterial Specimen Design	CO-ORD.	E392125 N811604	R.L.	14.63 m	SHEET	2 of 3
LOCATION	Queen Elizabeth II Drive, South Abutment	REF. GRID	Mount Pleasant 2000	DATUM	SCIRT_CCC	DEPTH	21.61 m

GEOLOGY/UNIT	MAIN DESCRIPTION	R.L. (m)	DEPTH (m)	GRAPHIC LOG	TESTS		CORE		DRILLING			ADDITIONAL NOTES	PIEZOMETER DETAILS	OTHER INSTRUMENTATION
					SPT N' VALUE	SPT BLOW COUNTS OR SHEAR VALUE	TOTAL CORE RECOVERY (%)	SAMPLE TYPE	DRILLING METHOD	CASING	BASE OF HOLE & WATER LEVEL			
Christchurch Formation	From 9.90m: with minor silt. Fine to coarse SAND with trace of silt; grey. 'Medium dense', well graded. Trace of shell fragments. (continued)	10					93	Sonic				SWL 1.03m, casing depth 9.00m 3.1m heave		
	From 10.52m: with trace of silt and trace of shell fragments.	4										2.7m heave		
	From 10.75m: with some shell fragments.		17		2/3// 3/5/5/4		100	SPT						
	From 11.15m: with minor shell fragments.		11											
	From 11.35m: with some shell fragments.						110	Sonic						
	Fine to medium SAND with minor silt; grey. 'Medium dense to dense', poorly graded. Trace of shell fragments.		12										4.0m heave	
	Fine SAND with trace of silt; grey. Medium dense, saturated, uniformly graded. Slightly dilatant.		2											
	From 12.89 to 12.91m: silty fine SAND, 'loose', dilatant.		13				101	Sonic						
	At 14.17m: coarse shell fragment.		14										1.0m heave PSD	
	From 14.50m: with minor silt.		0					101	Sonic					
Riccarton Gravel	From 15.50m: with trace of silt.		15				89	SPT				SWL 0.00m, casing depth 15.08m 1.0m heave		
	From 16.00m: with minor silt.		16											
	From 16.50m: with trace of silt.		-2											
	From 17.70m: with minor silt and trace of fine to medium shell fragments.		17											
	From 17.74m: with trace of silt.													
	From 17.80m: with minor fine gravel, subangular to subrounded. Organic SILT; brown. Firm wet, low plasticity. Slightly dilatant.		18											
	Fine to medium SAND with minor silt; brown. Very dense, saturated, uniformly graded. Dilatant.			60		3/4// 10/15/15/20	122	SPT				18.12m slow artesian flow, 3.4m head. 0.8m heave		
	From 18.50 to 18.55m: with some fine to coarse gravel, subangular to subrounded.		-4											
	Gravelly fine to coarse SAND with minor silt; brown. 'Dense', saturated, well graded. Gravel, fine to medium, subangular to subrounded.		19					107	Sonic					
	Fine to medium SAND, greenish brown. Very dense, poorly graded.			69		21/21// 20/16/16/17		SC	SPT				0.6m heave	

NOTES Refer to Site Plans for Location. Safety auto trip hammer #397 used (energy ratio 102%). LOGGED IN ACCORDANCE WITH NZ GEOTECHNICAL SOCIETY GUIDELINES (2005) SEE ATTACHED KEY SHEET FOR EXPLANATION OF SYMBOLS	STARTED	14/06/2013	FINISHED	18/06/2013
	INCLINATION/ AZIMUTH	Vertical; n/a	DRILLING Co.	McMillan Drilling
	LOGGED	F Neeson / S Cooke	DRILLING RIG	Geoprobe 8140LC
	CHECKED	S Cooke	DRILLER	D Berger
	CLIENT	NZ Transport Agency	PROJECT No.	6-DC716.52

A3 BOREHOLE SOIL NART_SD_GINT_2013_MASTER_FILE_GPJ_COMBO_TEM_MAR13.GDT 13/9/13



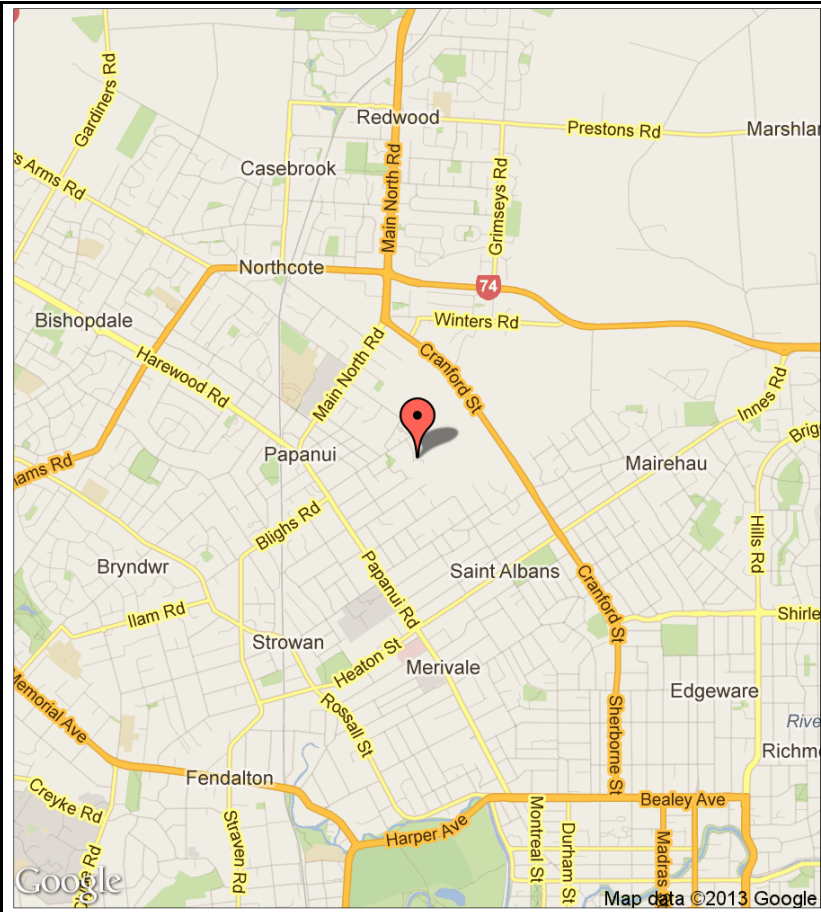
Borehole No: BH315

PROJECT	Northern Arterial Specimen Design	CO-ORD.	E392125 N811604	R.L.	14.63 m	SHEET	3 of 3
LOCATION	Queen Elizabeth II Drive, South Abutment	REF. GRID	Mount Pleasant 2000	DATUM	SCIRT_CCC	DEPTH	21.61 m

GEOLOGY/UNIT	MAIN DESCRIPTION	R.L. (m) DEPTH (m)	GRAPHIC LOG	TESTS		CORE		DRILLING			ADDITIONAL NOTES	PIEZOMETER DETAILS	OTHER INSTRUMENTATION
				SPT N' VALUE	SPT BLOW COUNTS OR SHEAR VALUE	TOTAL CORE RECOVERY (%)	SAMPLE TYPE	DRILLING METHOD	CASING	BASE OF HOLE & WATER LEVEL			
Riccarton Gravel	Gravelly fine to coarse SAND with minor silt; brown. 'Dense', saturated, well graded. Gravel, fine to medium, subangular to subrounded.	20		50	7/10// 12/12/12/14	97	Sonic	Rotary Sonic Drilling with SPTs			SWL +4.23m, casing depth 21.16m 21.35m fast artesian ground water encountered. 4.23m head.	Bentonite	
	Sandy fine to coarse GRAVEL with minor silt, greenish brown. Very dense, saturated, well graded. Gravel, fine to coarse, subrounded to rounded.	-6 21											
	Target depth not reached - borehole terminated at 21.61m. Artesian ground water prevents further progress: 4.23m head. Sealed and backfilled with bentonite. END OF BOREHOLE	22 -8 23 24 -10 25 26 -12 27 28 -14 29											

NOTES Refer to Site Plans for Location. Safety auto trip hammer #397 used (energy ratio 102%). LOGGED IN ACCORDANCE WITH NZ GEOTECHNICAL SOCIETY GUIDELINES (2005)	STARTED	14/06/2013	FINISHED	18/06/2013
	INCLINATION/ AZIMUTH	Vertical; n/a	DRILLING Co.	McMillan Drilling
	LOGGED	F Neeson / S Cooke	DRILLING RIG	Geoprobe 8140LC
	CHECKED	S Cooke	DRILLER	D Berger
	CLIENT	NZ Transport Agency	PROJECT No.	6-DC716.52

A3 BOREHOLE SOIL NART_SD_GINT_2013_MASTER_FILE_GPJ_COMBO_TEM_MAR13.GDT 13/9/13



⊕ = Test Location

Note: All images sourced from Google Maps



Date	Apr-13	Client	Medical Assurance Society		
Drawn by	DR	Project	EQ Claims		
Approved by	LF	Description	Site Location Plan		
Scale	NTS	Geoscience Ref.	9560	Client Ref.	Phase 730



TONKIN & TAYLOR LTD

BOREHOLE LOG

BH No: PAP-POD07-BHCPT017
 Hole Location: 218 Rutland Street
 SHEET 1 OF 2

PROJECT: CHCH TC3 GEOTECHNICAL INVESTIGATIONS	LOCATION: PAPANUI	JOB No: 52003.000
CO-ORDINATES: 5745236.84 mN 2479479.12 mE	DRILL TYPE: Roto-Sonic Mud	HOLE STARTED: 28/5/13
R.L.: 8.39 m	DRILL METHOD: PQDT/RM/Auto SPT	HOLE FINISHED: 28/5/13
DATUM: NZMG, MSL (CCC 20/01/12 Datum -9.043m)	DRILL FLUID: LP2000	DRILLED BY: Pro-Drill
		LOGGED BY: T&T-DG CHECKED: DAA

GEOLOGICAL										ENGINEERING DESCRIPTION									
GEOLOGICAL UNIT, GENERIC NAME, ORIGIN, MINERAL COMPOSITION.										SOIL DESCRIPTION									
TESTS										ROCK DESCRIPTION									
FLUID LOSS										DEFECTS									
WATER										TYPE, INCLINATION, THICKNESS, ROUGHNESS, FILLING.									
CORE RECOVERY (%)																			
METHOD																			
CASING																			
SAMPLES																			
R.L. (m)																			
DEPTH (m)																			
GRAPHIC LOG																			
CLASSIFICATION SYMBOL																			
MOISTURE / WEATHERING CONDITION																			
STRENGTH/DENSITY CLASSIFICATION																			
SHEAR STRENGTH (kPa)																			
COMPRESSIVE STRENGTH (MPa)																			
DEFECT SPACING (mm)																			
TOPSOIL										Organic SILT with trace rootlets and trace sand, dark brown, soft, moist, low plasticity. Organics are amorphous. Sand is fine to medium.									
YALDHURST MEMBER OF THE SPRINGSTON FORMATION (ALLUVIAL)										Sandy SILT, brownish grey, moist, low plasticity. Sand is fine to medium.									
Hand Auger										1.1m- wet, quick dilatancy.									
90										1.35 to 1.5m- no recovery.									
67 SPT										Sandy SILT, grey, very stiff, wet, low plasticity. Sand is fine to medium.									
0 SPT										1.5 to 1.8m- sample not retained.									
0 SPT										1.8 to 1.95m- no recovery.									
0 RM										1.95 to 2.0m- RM drill method.									
*ATP@3.0m										2.0 to 2.45m- no recovery.									
FC@3.0m										2.0m- very soft.									
0 SPT										[Obstruction at 1.65m, hole redrilled 2.0m away]									
100 SPT										SILT with some organics and trace sand, brownish grey, very soft, wet, high plasticity. Organics are fibrous. Sand is fine to Medium.									
0 RM																			
100 SPT																			
0 RM																			
0 SPT																			
67 SPT										5.0m- trace rootlets, grey, firm.									
0 RM										5.3 to 5.45m- no recovery.									
*FC@6.0m																			
1/2//4/3/3/4										Silty fine to medium SAND, grey, medium dense, wet, poorly graded.									
N=14										Sandy SILT, grey, stiff, wet, low plasticity. Sand is fine to medium.									
0 RM										6.3 to 6.45m- no recovery.									
0 SPT																			
78 SPT										Sandy fine to coarse GRAVEL with trace silt, grey, subangular to subrounded, dense, wet, well graded. Sand is fine to coarse.									
0 RM										7.35 to 7.45m- no recovery.									
100 SPT										Fine to medium SAND with minor silt, grey, medium dense, wet, poorly graded.									
2/1/2/3/2/2//										Fine to coarse GRAVEL with trace sand and trace silt, grey, subangular to subrounded, medium dense, wet, well graded. Sand is fine to coarse.									
2/2/2/2/2/1/										Fine to coarse SAND with minor silt, grey, medium dense, wet, well graded.									
2/1/2/1/2/2										8.4 to 9.1m- no recovery.									
N=21																			
33 PQDT																			
67 SPT										Sandy fine to coarse GRAVEL with trace silt, grey, subangular to subrounded, dense, wet, well graded. Sand is fine to coarse.									
4/5/3/4/3/3//										9.4 to 9.55m- no recovery.									
4/4/3/4/3/3/																			
3/2/3/3/2/2																			
N=36																			

T-T DATATEMPLATE-SPT.GDT reb



TONKIN & TAYLOR LTD

BOREHOLE LOG

BH No: PAP-POD07-BHCPT017 SHEET 2 OF 2
 Hole Location: 218 Rutland Street

PROJECT: CHCH TC3 GEOTECHNICAL INVESTIGATIONS LOCATION: PAPANUI JOB No: 52003.000
 CO-ORDINATES: 5745236.84 mN DRILL TYPE: Roto-Sonic Mud HOLE STARTED: 28/5/13
 2479479.12 mE DRILL METHOD: PQDT/RM/Auto SPT HOLE FINISHED: 28/5/13
 R.L.: 8.39 m DRILLED BY: Pro-Drill
 DATUM: NZMG, MSL (CCC 20/01/12 Datum -9.043m) DRILL FLUID: LP2000 LOGGED BY: T&T-DG CHECKED: DAA

GEOLOGICAL						ENGINEERING DESCRIPTION												
GEOLOGICAL UNIT, GENERIC NAME, ORIGIN, MINERAL COMPOSITION.	FLUID LOSS	WATER	CORE RECOVERY (%)	METHOD	CASING	TESTS	SAMPLES	R.L. (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MOISTURE CONDITION	WEATHERING	STRENGTH/DENSITY CLASSIFICATION	SHEAR STRENGTH (kPa)	COMPRESSIVE STRENGTH (MPa)	DEFECT SPACING (mm)	SOIL DESCRIPTION Soil type, minor components, plasticity or particle size, colour. ROCK DESCRIPTION Substance: Rock type, particle size, colour, minor components. Defects: Type, inclination, thickness, roughness, filling.
YALDHURST MEMBER OF THE SPRINGSTON FORMATION (ALLUVIAL)			71	PQDT		1/1/2/2/2/2// 3/2/2/2/2/1/ 2/2/2/2/2/2	█	-2			GW	W	D					Sandy fine to coarse GRAVEL with trace silt, grey, subangular to subrounded, dense, wet, well graded. Sand is fine to coarse. 10.4 to 10.7m- no recovery.
			56	SPT		N=24	█	11					MD					10.7m- medium dense. 10.95 to 11.15m- no recovery. 11
								-3										End of borehole at 11.15mbgl (target depth)
								12										12
								-4										13
								13										14
								-5										15
								14										16
								-6										17
								15										18
								-7										19
								16										20
								-8										
								17										
								-9										
								18										
								-10										
								19										
								-11										
								20										

T-T DATATEMPLATE-SPT.GDT reb



TONKIN & TAYLOR LTD

BOREHOLE LOG

BH No: STA-TC201-BH001
Hole Location: 332 Cranford Street

SHEET 1 OF 2

PROJECT: CHCH GEOTECHNICAL INVESTIGATIONS	LOCATION: ST ALBANS	JOB No: 52003.000
CO-ORDINATES: 5745485.06 mN 2479949.49 mE	DRILL TYPE: Roto-Sonic	HOLE STARTED: 9/4/13
R.L.: 6.43 m	DRILL METHOD: PQDT/Auto SPT	HOLE FINISHED: 9/4/13
DATUM: NZMG, MSL (CCC 20/01/12 Datum -9.043m)	DRILL FLUID: LP2000	DRILLED BY: Pro-Drill
		LOGGED BY: MWH-RM CHECKED: DAA

GEOLOGICAL						ENGINEERING DESCRIPTION												
GEOLOGICAL UNIT, GENERIC NAME, ORIGIN, MINERAL COMPOSITION.	FLUID LOSS	WATER	CORE RECOVERY (%)	METHOD	CASING	TESTS	SAMPLES	R.L. (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MOISTURE CONDITION	WEATHERING	STRENGTH/DENSITY CLASSIFICATION	SHEAR STRENGTH (kPa)	COMPRESSIVE STRENGTH (MPa)	DEFECT SPACING (mm)	SOIL DESCRIPTION
																		Soil type, minor components, plasticity or particle size, colour.
ROCK DESCRIPTION																		
Substance: Rock type, particle size, colour, minor components.																		
Defects: Type, inclination, thickness, roughness, filling.																		
FILL																		
YALDHURST MEMBER OF THE SPRINGSTON FORMATION (ALLUVIAL)			33	Hand Auger					6		SM	M						Silty fine to coarse SAND with minor gravel and trace rootlets, dark brown, moist, well graded. Gravel is fine to coarse, angular to subangular.
									1		SP							Fine to medium SAND with minor rootlets and minor silt, light brown, moist, poorly graded. 0.5 to 1.5m- no recovery.
									5			W						1.2m- wet.
			44	SPT		3/2//1/1/0/1 N=3			2		Pt		S					PEAT with trace silt and trace gravel, dark brown, fibrous to amorphous, soft, wet, high plasticity. Gravel is fine to medium, subangular to subrounded.
									4									1.7 to 1.95m- no recovery. 1.95m- trace fine to medium sand. 2.1m- some silt. 2.4 to 3.0m- no recovery.
			43	PQDT					3				VS					3.0m- very soft. 3.15 to 3.45m- no recovery.
			33	SPT		0/0//0/0/0/0 N=0 *ATP@3.5m *FC@3.5m	B	3			OH							Organic SILT with some sand, brownish grey, very soft, wet, high plasticity. Organics are fibrous and amorphous. Sand is fine to medium.
			100	PQDT					4									
									2				F					4.5m- firm. 4.6 to 4.95m- no recovery.
			22	SPT		2/2//1/2/1/3 N=7			5									SILT with minor organics and minor sand, grey, firm, wet, low plasticity. Organics are fibrous (wood) and amorphous. Sand is fine to medium.
									1									5.15m- trace amorphous and fibrous organics. 5.5 to 5.7m- some fibrous organics (wood).
			100	PQDT		*FC@5.4m	B	1			ML							Fine to medium SAND with trace gravel, trace organics, and trace silt, light grey, loose, wet, poorly graded. Gravel is medium to coarse, subrounded. Organics are fibrous.
									6				L					6.0m- medium dense.
			67	SPT		5/5//5/5/6/6 N=22			0		SP		MD					Sandy fine to coarse GRAVEL with trace silt, grey, subangular to subrounded, medium dense, saturated, well graded. Sand is fine to coarse.
									7									6.3 to 6.45m- no recovery.
			100	PQDT					8									
									1									7.7 to 7.95m- no recovery.
			44	SPT		1/1//1/1/2// 2/2/2//1/1/2/ 2/2/2//1/2/2 N=21			9									
									2									
			100	PQDT					3									
									9									9.4 to 9.45m- no recovery.
			89	SPT		1/1//2/2/2// 3/2/2//2/2/2/ 2/2/2//1/2/2 N=24			10									
			100	PQDT														

T-T-DATATEMPLATE-SPT.GDT reb

Log Scale 1:50

BORELOG-TC3 720016 STA-TC201.GPJ 30-Jul-2013



TONKIN & TAYLOR LTD

BOREHOLE LOG

BH No: STA-TC201-BH001
Hole Location: 332 Cranford Street

SHEET 2 OF 2

PROJECT: CHCH GEOTECHNICAL INVESTIGATIONS	LOCATION: ST ALBANS	JOB No: 52003.000
CO-ORDINATES: 5745485.06 mN 2479949.49 mE	DRILL TYPE: Roto-Sonic	HOLE STARTED: 9/4/13
R.L.: 6.43 m	DRILL METHOD: PQDT/Auto SPT	HOLE FINISHED: 9/4/13
DATUM: NZMG, MSL (CCC 20/01/12 Datum -9.043m)	DRILL FLUID: LP2000	DRILLED BY: Pro-Drill
		LOGGED BY: MWH-RM CHECKED: DAA

GEOLOGICAL						ENGINEERING DESCRIPTION												
GEOLOGICAL UNIT, GENERIC NAME, ORIGIN, MINERAL COMPOSITION.	FLUID LOSS	WATER	CORE RECOVERY (%)	METHOD	CASING	TESTS	SAMPLES	R.L. (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MOISTURE CONDITION	WEATHERING	STRENGTH/DENSITY CLASSIFICATION	SHEAR STRENGTH (kPa)	COMPRESSIVE STRENGTH (MPa)	DEFECT SPACING (mm)	SOIL DESCRIPTION Soil type, minor components, plasticity or particle size, colour. ROCK DESCRIPTION Substance: Rock type, particle size, colour, minor components. Defects: Type, inclination, thickness, roughness, filling.
YALDHURST MEMBER OF THE SPRINGSTON FORMATION (ALLUVIAL)			100	PQDT		3/3/3/3/2/2// 2/1/2/1/0/1/ 1/2/1/2/2/3	█	4			GW	S	MD					Sandy fine to coarse GRAVEL with trace silt, grey, subangular to subrounded, medium dense, saturated, well graded. Sand is fine to coarse.
			44	SPT		N=18	█	11										10.7 to 10.95m- no recovery.
								11										End of borehole at 10.95mbgl (target depth)
								-5										
								12										
								-6										
								13										
								-7										
								14										
								-8										
								15										
								-9										
								16										
								-10										
								17										
								-11										
								18										
								-12										
								19										
								-13										
								20										

T-T DATATEMPLATE-SPT.GDT reb

BOREHOLE INFORMATION	CO-ORDINATES N/A	Date Started: 5/05/2012	Logged by: TJP
Drilling Method: Sonic Drilling	Easting: N/A	Date Completed: 5/05/2012	Input by: TJP
Diameter Core: 100mm	Northing: N/A	Inclination:	Checked by: RS
Contractor: DCN Drilling Ltd	Ground Level: N/A	Orientation:	Verified by: RS

Method/Casing	Core Recovery (%)	Water Loss (%)	Groundwater Level (m)	R.L. (m)	Depth (m)	Graphic Log	Material Description	USC Description	Consistency/Density	Moisture	Sample	In-Situ Testing	Laboratory Testing	Notes	Backfill	Geological Unit				
Roto Sonic VB	NOT RECORDED				0.10		SILT with trace rootlets; brown. Stiff to very stiff; dry; low plasticity; friable (TOPSOIL).													
					0.50		SILT with some gravel and minor sand; brown. Stiff; moist; low plasticity. Gravel is medium to coarse grained and rounded to subrounded. Sand is fine to medium grained.													
					1.00		0.4m Becomes with no gravel; greyish brown with orange brown and dark brown mottling. Dry.													
					1.10		0.5m Becomes with trace of gravel. Gravel is medium to coarse grained and rounded to subrounded.													
					1.30		0.7 Becomes greyish brown with reddish brown mottling.													
					1.95		0.9 Becomes with no gravel; grey. Soft.													
					2.10		SAND with some silt and minor gravel; grey. Loosely packed; moist. Sand is fine to coarse grained and well graded. Gravel is fine to medium grained and rounded to subrounded.										SPT at 1.5m N = 1 1/0, 1 450mm (SS)			
					2.30		PEAT with some silt and minor sand; dark brown. Soft; moist. Peat is fibrous.													
					2.40		SILT; grey. Firm; moist; moderate plasticity.													
					2.50		PEAT; dark brown. Soft; moist. Peat is fibrous.													
					2.60		SILT with some peat; grey. Very soft; wet; moderate plasticity. Peat is fibrous.													
					2.85		2.0m Becomes greyish brown.													
					4.95		PEAT; dark brown. Soft; wet. Peat is fibrous.													
					5.20		SILT with some peat; brownish grey. Soft; wet; moderate plasticity.													
					5.30		PEAT; dark brown. Soft; wet. Peat is fibrous.													
					5.40		SILT with some peat; brownish grey. Soft; wet; moderate plasticity.													
7.00		3.45m Becomes very soft.																		
7.20		3.9m Becomes soft.																		
7.20		SAND some silt; grey. Moderately packed; wet. Sand is fine to medium grained.																		
7.20		Sandy SILT; grey. Firm; wet; low plasticity. Sand is fine to medium grained.																		
7.20		SILT with some sand; grey. Firm; saturated; low plasticity.																		
7.20		SAND with some silt; light brown. Loosely packed; saturated. Sand is fine to coarse grained and well graded.																		
7.20		5.6m Becomes with minor silt.																		
7.20		6.0m Becomes with no silt.																		
7.20		Sandy GRAVEL; greyish brown. Loosely packed; saturated. Gravel is fine to medium grained, well graded and rounded to subrounded.																		
7.20		GRAVEL with some sand and cobble inclusions; brownish grey. Loosely packed; saturated. Gravel is fine to coarse grained, well graded and rounded to subrounded. Sand is fine to coarse grained and well graded.																		
7.20		8.0m Becomes with no sand. Grey.																		
9.00																				
9.65																				

Method	USC Classification	Consistency	Soil Samples	In Situ Testing	Graphic Log
CC concrete core OB open barrel OSA solid stem auger HSA hollow stem auger WASH wash drill PQ3 PQ Triple Tube HQ3 HQ Triple Tube NQ3 NQ Triple Tube NMILC NMILC Triple Tube DP Direct Push DT Dual Tube (70mm) Casing	CH Inorganic CLAYS high plasticity CI Inorganic CLAYS medium plasticity CL Inorganic CLAYS low plasticity GC Clayey GRAVEL GM Silty GRAVEL GP Poorly Graded GRAVEL GW Well Graded GRAVEL MH Inorganic SILT high plasticity ML Inorganic SILT low plasticity OL ORGANIC CLAY medium to high plasticity OT ORGANIC SILT low plasticity PL PEAT and highly organic soils SC Clayey SAND SM Silty SAND SP Poorly graded SAND SW Well graded SAND	VS very soft S soft F firm S stiff VS very stiff H hard Density VL very loose L loose MD medium dense D dense VD very dense	B bulk U undisturbed D disturbed Water ▽ at end of excavation ▽ at time of excavation ▽ at time of closure	PP pen penetrometer VS vane shear SPT std. pen. test SS split spoon SC solid cone HB hammer bouncing SH sinks under own weight Moisture D dry M moist W wet S saturated	

BOREHOLE INFORMATION Drilling Method: Sonic Drilling Diameter Core: 100mm Contractor: DCN Drilling Ltd	CO-ORDINATES N/A Easting: N/A Northing: N/A Ground Level: N/A	Date Started: 5/05/2012 Date Completed: 5/05/2012 Inclination: Orientation:	Logged by: TJP Input by: TJP Checked by: RS Verified by: RS
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Method/Casing	Core Recovery (%)	Water Loss (%)	Groundwater Level (m)	R.L. (m)	Depth (m)	Graphic Log	Material Description	USC Description	Consistency/Density	Moisture	Sample	In-Situ Testing	Laboratory Testing	Notes	Backfill	Geological Unit	
Roto Sonic VB	95				10.50		SAND with minor; brown. Loosely packed; saturated. Sand is fine to medium grained.					SPT at 10.5m N = 50+ 15/27, 23 440mm (SS)					
	35				11		GRAVEL with some sand; greyish brown. Loosely packed; saturated. Gravel is fine to coarse grained, well graded and rounded to subangular. Sand is fine to coarse grained and well graded. (Layer Continued from previous page)										
	100				11.70		10.25m Becomes with minor sand. Gravel is medium to coarse grained, poorly graded and rounded to subrounded.										
	20				12		10.35m Becomes with some sand. Gravel is fine to coarse grained, well graded and rounded to subangular.						SPT at 12m N = 29 12/14, 15 450mm (SS)				
	100				13		SAND; greyish brown. Loosely packed; saturated. Sand is medium to coarse grained and poorly graded.										
	35				13.95		10.95m Becomes with some silt; orangish brown. Sand is fine to coarse grained.										
	100				14		11.1m Becomes no silt; greyish brown. Sand is medium to coarse grained.										
					14.20	14.35		11.3m Becomes with some gravel. Gravel is fine to medium grained, poorly graded and rounded to subangular.									
					14.20	14.35		Sandy GRAVEL; brownish grey. Loosely packed; saturated; gravel is fine to coarse, well graded and rounded to subrounded. Sand is fine to coarse grained and poorly graded.									
					15	15.00		SAND with minor gravel; greyish brown. Loosely packed; saturated. Sand is medium to coarse grained and poorly graded. Gravel is fine to medium grained, rounded to subangular.									
					16		12.7m Becomes with no gravel; brown. Sand is fine to coarse grained and well graded.										
					17		13.1m Becomes minor silt.										
					18		13.3m Becomes some silt; greyish brown.										
					19		13.95m Becomes with no silt; grey. Sand is medium to coarse grained and poorly graded.										
							SILT with some sand; grey. Stiff; saturated; low plasticity.										
							SAND with some silt; grey. Loosely packed; saturated. Sand is fine to coarse grained and well graded.										
							14.6m Becomes with no silt. Sand is medium to coarse grained.										
							Borehole Terminated at 15m (Required Depth)										

Method CC concrete core OB open barrel SBA solid stem auger HSA hollow stem auger WASH wash drill PQ3 PQ Triple Tube HQ3 HQ Triple Tube NQ3 NQ Triple Tube NMILC NMILC Triple Tube DP Direct Push DT Dual Tube (70mm) Casing	USC Classification CH Inorganic CLAYS high plasticity CI Inorganic CLAYS medium plasticity CL Inorganic CLAYS low plasticity GC Clayey GRAVEL GM Silty GRAVEL GP Poorly Graded GRAVEL GW Well Graded GRAVEL MH Inorganic SILT high plasticity ML Inorganic SILT low plasticity OH ORGANIC CLAY medium to high plasticity OL ORGANIC SILT low plasticity PT PEAT and highly organic soils SC Clayey SAND SM Silty SAND SP Poorly graded SAND SW Well graded SAND	Consistency VS very soft S soft F firm S stiff VS very stiff H hard Density VL very loose L loose MD medium dense D dense VD very dense	Soil Samples B bulk U undisturbed D disturbed Water ▽ at end of excavation ▽ at time of excavation ▽ at time of closure	In Situ Testing PP pen penetrometer VS vane shear SPT std. pen. test SS split spoon SC solid cone HB hammer bouncing SH sinks under own weight Moisture D dry M moist W wet S saturated	Graphic Log Topsoil SILT SAND Peat Sandy SILT Sandy GRAVEL GRAVEL	Backfill
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Borelog for well M35/14022

Gridref: M35:78906-46103 Accuracy : 3 (1=high, 5=low)

Ground Level Altitude : 11.59 +MSD

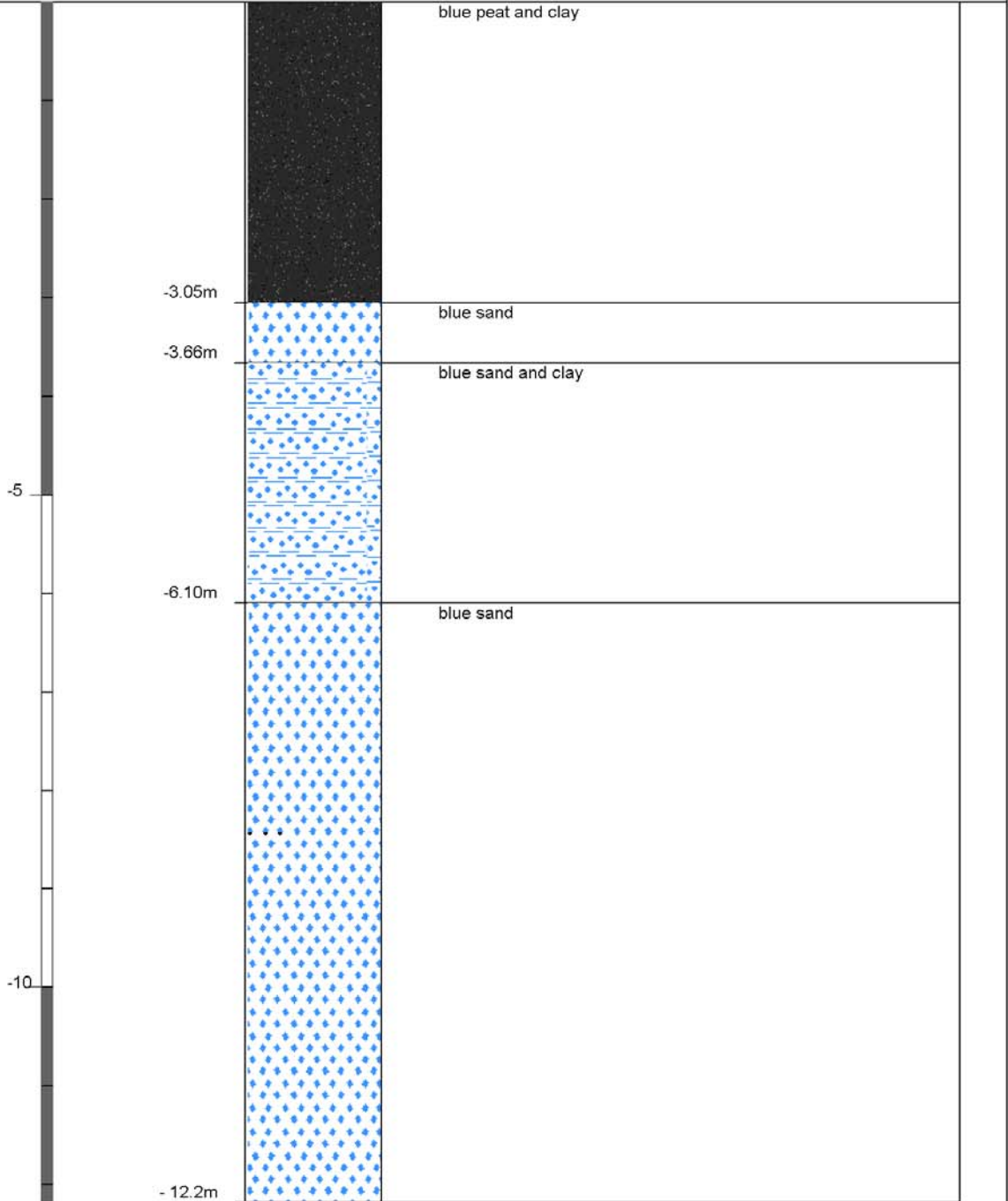
Well name : CCC BorelogID 2526

Drill Method : Not Recorded

Drill Depth : -12.19m Drill Date : 1/01/1959



Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
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Borelog for well M35/10866

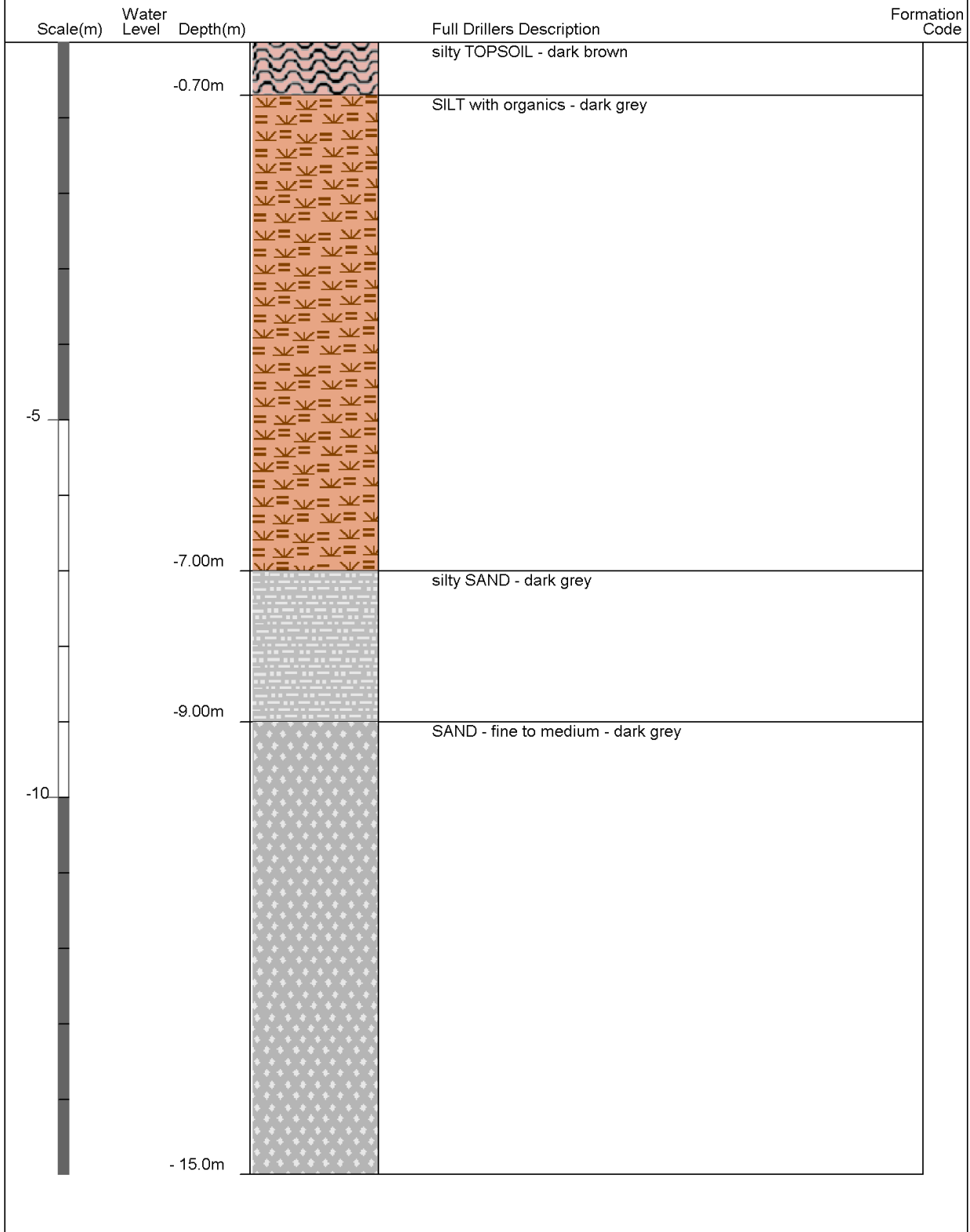
Gridref: M35:7951-4632 Accuracy : 4 (1=high, 5=low)

Ground Level Altitude : 10.86 +MSD

Driller : C W Drilling and Investigations Ltd

Drill Method : Concentrics

Drill Depth : -15m Drill Date : 2/08/2005



Appendix C – (Further Investigation Results)

Geotechnical Logs

CPT Plots

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569019.807, N 5184497.777 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 15.5m
Site: Grassmere Street **Commenced:** 26-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 29-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES				
																EW	VW	W	MS
0.3	HQ Coring	109	None			OL		TOPSOIL trace rootlets; dark brown. Moist; low plasticity.	M										
0.6						ML		SILT; grey. Soft to firm; moist; low plasticity.	M	S									
0.9						SP		Fine SAND trace silt; grey. Loose; wet; poorly graded.	M	L									
1.1						ML		SILT some sand; grey. Soft to firm; moist; low plasticity; sand, fine.	M	S									
1.3						OL		Organic SILT; dark brown. Soft; moist; low plasticity.	M	S									
1.5						ML		SILT some sand; grey. Very soft; moist; low plasticity; sand, fine.	M	VS									
1.8	SPT	11	None					Coreloss								SPT			
2.0						Pt		PEAT; amorphous; dark brown; soft; moist; H1.	M	S								0.0, 0.0, 0.0, [0]	
2.2						Pt		Inferred PEAT; amorphous; dark brown; soft; moist; H1.	M	S									
2.5	Push tube	100	None			ML		Inferred SILT; grey. Soft; moist; low plasticity.	M	S									
2.8						SM		Inferred Silty fine to medium SAND; grey. Wet; poorly graded.	W										
3.1	SPT	100	None			SM		Silty fine to medium SAND; grey. Medium dense; wet; poorly graded.	W	MD						SPT			
3.4																			3.3, 4.2, 3.3, [12]
3.8	HQ Coring	100	None			ML		SILT trace sand; grey. Very soft; wet; low plasticity; quick and dilatant behaviour; sand, fine.	W	VS									
4.2																			
4.6	SPT	100	None													SPT			
4.9																			

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT. 21/9/15

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569019.807, N 5184497.777 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 15.5m
Site: Grassmere Street **Commenced:** 26-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 29-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) / [Elev.]
Drilling Method
Core Run / Recovery (%)
Support / Casing (m)
Water
Geological Fm
Classification
Graphic Log
SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure.
(Geological Formation)
ROCK DESCRIPTION: Weathering, colour, fabric, **ROCK NAME** (Formation Name)
Moisture Condition
Consistency/Relative Density
Weathering
Estimated Rock Strength
RQD (%)
Defect Spacing (mm)
TESTS & SAMPLES
ROCK MASS DEFECTS: Depth, Type, Inclinations, Roughness, Texture, Aperture, Coating

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation)	ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
10.00	HQ Coring		None			SP		Fine to medium SAND; grey. Loose; wet; poorly graded. 10.14 to 10.19m wood fragment	W	L							
11.00	SPT		None													SPT 3.3, 1.1, 1.0, [3]	
12.00	HQ Coring		None						@12.04m becomes dense		D					SPT 7.7, 7.7, 7.9, [30]	
13.00	SPT		None						@13.56m becomes very dense		VD					SPT 7.5, 6.6, 15.30, [57]	
14.00	HQ Coring		None					14.4 to 14.55m wood fragment									
15.00																	

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT. 21/9/15

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569019.807, N 5184497.777 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 15.5m
Site: Grassmere Street **Commenced:** 26-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 29-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) [Elev.]
Drilling Method
Core Run / Recovery (%)
Support / Casing (m)
Water
Geological Fm
Classification
Graphic Log
SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure.
ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)
Moisture Condition
Consistency/Relative Density
Weathering
Estimated Rock Strength
RQD (%)
Defect Spacing (mm)
TESTS & SAMPLES

SPT	None	SP		W	L MD													SPT 6.7, 6.5, 5.5, [21]
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Termination Depth = 15.5m, Target Depth

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569278.232, N 5184443.543 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 12.5m
Site: Cranford Street **Commenced:** 24-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 24-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
																FW
0.0	HQ Coring	68	None		Christchurch Formation	OL		TOPSOIL trace rootlets; dark brown. Moist; low plasticity.	M							ROCK MASS DEFECTS: Depth, Type, Inclinations, Roughness, Texture, Aperture, Coating
0.6								Coreloss inferred TOPSOIL								
0.8	SPT	100	None		Christchurch Formation	SP		Fine SAND trace silt; grey. 'Loose'; wet; poorly graded; quick and dilatant behaviour.	W	'L'					SPT	
1.0																
1.2	HQ Coring	112	None		Christchurch Formation	ML		SILT; grey. Very soft; moist; low plasticity.	M	VS					SPT	
1.8																
2.0	Push tube	54	None		Christchurch Formation	ML		SILT with organics; brown. Very soft; moderately plastic.	M	VS					SPT	
2.5																
3.0	HQ Coring	211	None		Christchurch Formation	SP		Fine to medium SAND trace silt; grey. Loose; wet; poorly graded.	W	L					SPT	
3.5																
4.0	SPT	78	None		Christchurch Formation									SPT		
4.5																
5.0		142			Christchurch Formation									SPT		
5.5																
6.0																

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT 21/9/15

1,0,
0,0,
0,0,
[0]

0,0,
0,0,
2,2,
[4]

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569278.232, N 5184443.543 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 12.5m
Site: Cranford Street **Commenced:** 24-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 24-Jun-15


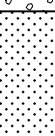

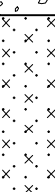
Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
																FW
6.5	HQ Coring	142			Christchurch Formation	SP		Gravelly fine to coarse SAND; grey. Wet; well graded; gravel, fine to medium, subangular to subrounded, greywacke.	W							
6.5 - 6.7	SPT	100	None			SP		Fine to medium SAND; grey. Wet; poorly graded.	W							SPT 1,3, 3,4, 3,3, [13]
6.7 - 7.0	HQ Coring	100	None			GW		Sandy fine to coarse GRAVEL; grey. Medium dense; well graded; subangular to subrounded; greywacke; sand, fine to coarse.	W	MD						
7.0 - 7.3	SPT	100	None			SP		Fine to medium SAND; grey. Loose; wet; poorly graded.	W	L						SPT 1,1, 1,1, 2,5, [9]
7.3 - 7.7	HQ Coring	100	None		GW		Sandy fine to coarse GRAVEL; grey. Dense; well graded; subangular to subrounded; greywacke; sand, fine to coarse.	W	D							
7.7 - 8.0	SPT	100	None												SPT 8,10, 13,12, 12,10, [47]	

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT. 21/9/15

Project:	Cranford Basin Geotechnical Investigations	Coordinates: E 1569278.232, N 5184443.543	Datum: NZTM
Client:	Christchurch City Council	Total Depth: 12.5m	
Site:	Cranford Street	Commenced: 24-Jun-15	Contractor: McMillan Drilling
Job No.:	5133038	Completed: 24-Jun-15	

Equipment: Track 8140 LS	Inclination: -90	Logged:	DW
Shear Vane:	Comments:	Processed:	DW
Bore Diameter (mm): 96		Checked:	JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
																EW
10.5	HQ Coring	100	None		Christchurch Formation	GW		Sandy fine to coarse GRAVEL; grey. Dense; well graded; subangular to subrounded; greywacke; sand, fine to coarse.	W	D						
11.0	SPT	110	None			SP		Fine to medium SAND; grey. Very dense; wet; poorly graded.	W	VD						SPT 10,13, 16,16, 20,8, [60+]
11.5	HQ Coring	96	None			GW		Sandy fine to coarse GRAVEL; grey. 'Dense'; well graded; subangular to subrounded; greywacke; sand, fine to coarse.	W	'D'						
12.0	SPT	100				SM		Silty fine SAND; grey. Dense; wet; poorly graded.	W	D						SPT 8,8, 12,13, 12,12, [49]
12.5	Termination Depth = 12.49m, Target Depth															

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT 21/9/15

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569379.036, N 5184555.284 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 17.1m
Site: Cranford Street **Commenced:** 23-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 24-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES
0.0	HQ Coring	100	None		Christchurch Formation	OL		TOPSOIL trace rootlets; dark brown. Moist; low plasticity.	M						
0.5	HQ Coring	109	None			ML		SILT; grey. Firm; moist; low plasticity.	M	F					
1.0	HQ Coring	213	None			SP		Fine to medium SAND trace silt; grey. Very loose; moist; poorly graded.	M	VL					
1.5	SPT	100	None												SPT 2,1, 1,0, 1,1, [3]
2.0	HQ Coring	100	None			ML		SILT; grey. Firm; moist; low plasticity.	M	F					
2.5	Push Tube	71	None					Push Tube, no sample to log							
3.0															
3.5															
3.7	HQ Coring	100	None			OL		SILT with organics; grey mottled dark brown. Very soft; slightly plastic; organics, wood and rootlets.	M	VS					
4.0						ML		SILT; grey. Firm; moist; low plasticity.	M	F					
4.5					ML		SILT trace organics; brown. Soft; moist; moderately plastic.	M	F						
5.0	SPT	100	None		ML		SILT; grey. Firm; wet; low plasticity; quick and dilatant behaviour.	W	F					SPT 0,0, 0,0, 2,1, [3]	

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT. 21/9/15

Project:	Cranford Basin Geotechnical Investigations	Coordinates: E 1569379.036, N 5184555.284	Datum: NZTM
Client:	Christchurch City Council		Total Depth: 17.1m
Site:	Cranford Street	Commenced: 23-Jun-15	Contractor: McMillan Drilling
Job No.:	5133038	Completed: 24-Jun-15	

Equipment: Track 8140 LS	Inclination: -90	Logged:	DW
Shear Vane:	Comments:	Processed:	DW
Bore Diameter (mm): 96		Checked:	JR

Depth (m) [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES
5.5	HQ Coring	100	None		Christchurch Formation	ML	x x x x x	SILT; grey. Firm; wet; low plasticity; quick and dilatant behaviour.	W	F					
5.5	HQ Coring	100	None			SM	x x x x x	Silty fine SAND; grey. Wet; poorly graded.	W						
6.6	HQ Coring	122	None			ML	x x x x x	SILT; grey. Soft; wet; low plasticity; quick and dilatant behaviour.	W						
6.6	HQ Coring	122	None			SM	x x x x x	Silty fine SAND; grey. Wet; poorly graded; quick and dilatant behaviour.	W						
7.0	HQ Coring	100	None			ML	x x x x x	SILT; grey. Soft; wet; low plasticity; quick and dilatant behaviour.	W						
7.0	HQ Coring	100	None			SM	x x x x x	Silty fine SAND; grey. Wet; poorly graded; quick and dilatant behaviour.	W						
7.5	SPT	100	None			SP	Fine to medium SAND trace silt; grey. Loose; wet; poorly graded.	W	L					SPT 0.0, 0.0, 1.3, [4]
8.0	HQ Coring	100	None												
9.0	SPT	100	None												SPT 1.0, 1.0, 3.4, [8]
10.0	HQ Coring	100	None												

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569379.036, N 5184555.284 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 17.1m
Site: Cranford Street **Commenced:** 23-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 24-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/ Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
																EW
15.1	SPT	100	None		Christchurch Formation	SP		Organic fine SAND trace wood fragments; dark brown. Medium dense; moist; poorly graded.	M	MD					SPT 2,1, 3,2, 3,4, [12]	
15.8	HQ Coring	100	None			SP		Fine to medium SAND; grey. Medium dense; wet; poorly graded.	W	MD						
16	SPT	100	None													SPT 4,3, 4,4, 4,9, [21]
17								Termination Depth = 17.05m, Target Depth								
17.1																
18																
19																
20																

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569475.26, N 5184305.058 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 11.0m
Site: Cranford Street **Commenced:** 25-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 25-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES
0.00	HQ Coring	100	None		Christchurch Formation	OL		TOPSOIL trace rootlets; dark brown. Moist; low plasticity.	M						
0.50	HQ Coring	100	None			ML		SILT; grey. Soft to firm; moist; low plasticity.	M	S					
1.00	SPT	100	None			OL		Organic SILT with wood fragments; dark brown. Very soft; moist; low plasticity.	M	VS					SPT 0.0, 0.0, 0.0, [0]
1.50	Push Tube	100	None			SM		Silty fine SAND; grey. Wet; poorly graded; quick and dilatant behaviour.	W						
2.00	HQ Coring	100	None			SP		Fine to medium SAND trace silt; grey. Medium dense; wet; poorly graded.	W	MD					SPT 1.0, 2.3, 4.6, [15]
2.50	HQ Coring	100	None												
3.00	HQ Coring	100	None												
3.50	HQ Coring	100	None												
4.00	HQ Coring	100	None												
4.50	HQ Coring	100	None												
5.00	HQ Coring	100	None												

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT 21/9/15

Project: Cranford Basin Geotechnical Investigations **Coordinates:** E 1569475.26, N 5184305.058 **Datum:** NZTM
Client: Christchurch City Council **Total Depth:** 11.0m
Site: Cranford Street **Commenced:** 25-Jun-15 **Contractor:** McMillan Drilling
Job No.: 5133038 **Completed:** 25-Jun-15

Equipment: Track 8140 LS **Inclination:** -90 **Logged:** DW
Shear Vane: **Comments:** **Processed:** DW
Bore Diameter (mm): 96 **Checked:** JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES	
																EW
5.1	HQ Coring	100	None		Christchurch Formation	SP		Sandy fine to coarse GRAVEL; grey. Medium dense; wet; subangular to subrounded, greywacke; well graded; sand, fine to coarse.	W	MD						
6.5	SPT	100	None			GW		Fine to medium SAND; grey. Medium dense; wet; poorly graded.	W	MD						SPT 4.5, 4.6, 5.5, [20]
6.8	HQ Coring	100	None			SP		Fine to medium SAND; grey. Dense; wet; poorly graded.	W	D						
8.0	SPT	100	None			GW		Fine to medium SAND; grey. Dense; wet; poorly graded.	W	D						SPT 4.7, 8.7, 9.8, [32]
8.5	HQ Coring	100	None			SP		Fine to medium SAND; grey. Dense; wet; poorly graded.	W	D						
9.0	SPT	100	None												SPT 8.8, 8.10, 10.12, [40]	

BOREHOLE LOG NZ ALT CRANFORD BASIN.GPJ NZ GINT DATA TEMPLATE VER 1.5.GDT. 21/9/15

Project:	Cranford Basin Geotechnical Investigations	Coordinates: E 1569475.26, N 5184305.058	Datum: NZTM
Client:	Christchurch City Council		Total Depth: 11.0m
Site:	Cranford Street	Commenced: 25-Jun-15	Contractor: McMillan Drilling
Job No.:	5133038	Completed: 25-Jun-15	

Equipment: Track 8140 LS	Inclination: -90	Logged:	DW
Shear Vane:	Comments:	Processed:	DW
Bore Diameter (mm): 96		Checked:	JR

Depth (m) / [Elev.]	Drilling Method	Core Run / Recovery (%)	Support / Casing (m)	Water	Geological Fm	Classification	Graphic Log	SOIL DESCRIPTION: (Soil Code), Soil Name [minor MAJOR], colour, structure [zoning, defects, cementing], plasticity or grain size, secondary components, structure. (Geological Formation) / ROCK DESCRIPTION: Weathering, colour, fabric, ROCK NAME (Formation Name)	Moisture Condition	Consistency/Relative Density	Weathering	Estimated Rock Strength	RQD (%)	Defect Spacing (mm)	TESTS & SAMPLES
11.110	SPT	100	None		Christchurch Formation	SP		Fine to medium SAND; grey. Dense; wet; poorly graded.	W	D					<div style="border: 1px solid black; width: 100%; height: 100%; position: relative;"> <div style="position: absolute; top: 0; right: 0; bottom: 0; left: 0; background-color: black; width: 100%; height: 100%;"></div> <div style="position: absolute; top: 50%; left: 50%; transform: translate(-50%, -50%);"> <p>SPT</p> <p>1,0, 3,4, 5,8, [20]</p> </div> </div>
11.000	HQ Coring	100	None		Christchurch Formation			Termination Depth = 10.97m, Target Depth							

CONE PENETRATION TEST (CPT) REPORT



Client: GHD NZ Ltd
Location: Grassmere Street, Cranford Street
Christchurch

Printed: 26/06/2015

CONE PENETRATION TEST

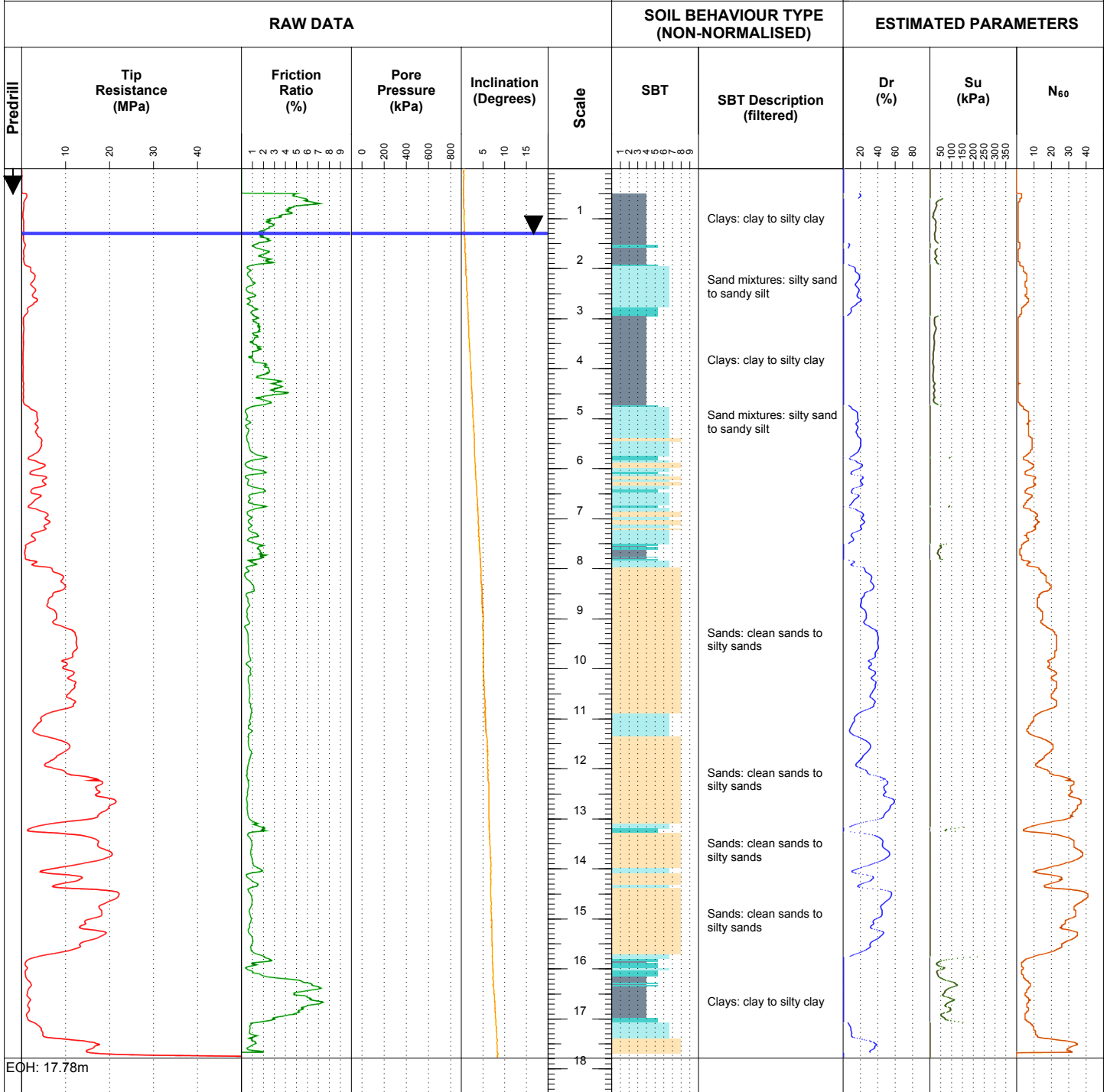
Job: 14784

CPT No.: CPT101

Name: Cranford Basin
 Client: GHD NZ Ltd
 Location: 37 Grassmere Street, Christchurch

Grid: NZTM
 Datum: Ground
 Termination: -

North (m): 5184441.09
 East (m): 1569102.68
 Elevation (m): -
 Hole Depth (m): 17.78



Operator: P. Buunk

Rig: 14t truck mounted rig

Cone Reference: 080238T

Cone Area Ratio: 0.75

Cone Type: I-CFXY-10

Tip Resistance (MPa) Initial: -4.1778

Local Friction (MPa) Initial: -0.0362

Pore Pressure (KPa) Initial: -

Date: 16/06/2015

Predrill: 0.50

Water Level: 1.30

Collapse: -

Final: -4.1051

Final: -0.0364

Final: -

Effective Refusal

Tip: ✓

Gauge:

Inclinometer:

Other:

Target Depth:

Soil Behaviour Type (SBT) - Robertson et al. 1986

0 Undefined

1 Sensitive fine-grained

2 Clay - organic soil

3 Clays: clay to silty clay

4 Silt mixtures: clayey silt & silty clay

5 Sand mixtures: silty sand to sandy silt

6 Sands: clean sands to silty sands

7 Dense sand to gravelly sand

8 Stiff sand to clayey sand

9 Stiff fine-grained

Notes & Limitations

Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. Both McMillan Drilling Ltd & GeroC Solutions Ltd do not warrant the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

Remarks

Effective Refusal

Hole Depth (m): 17.78

CONE PENETRATION TEST

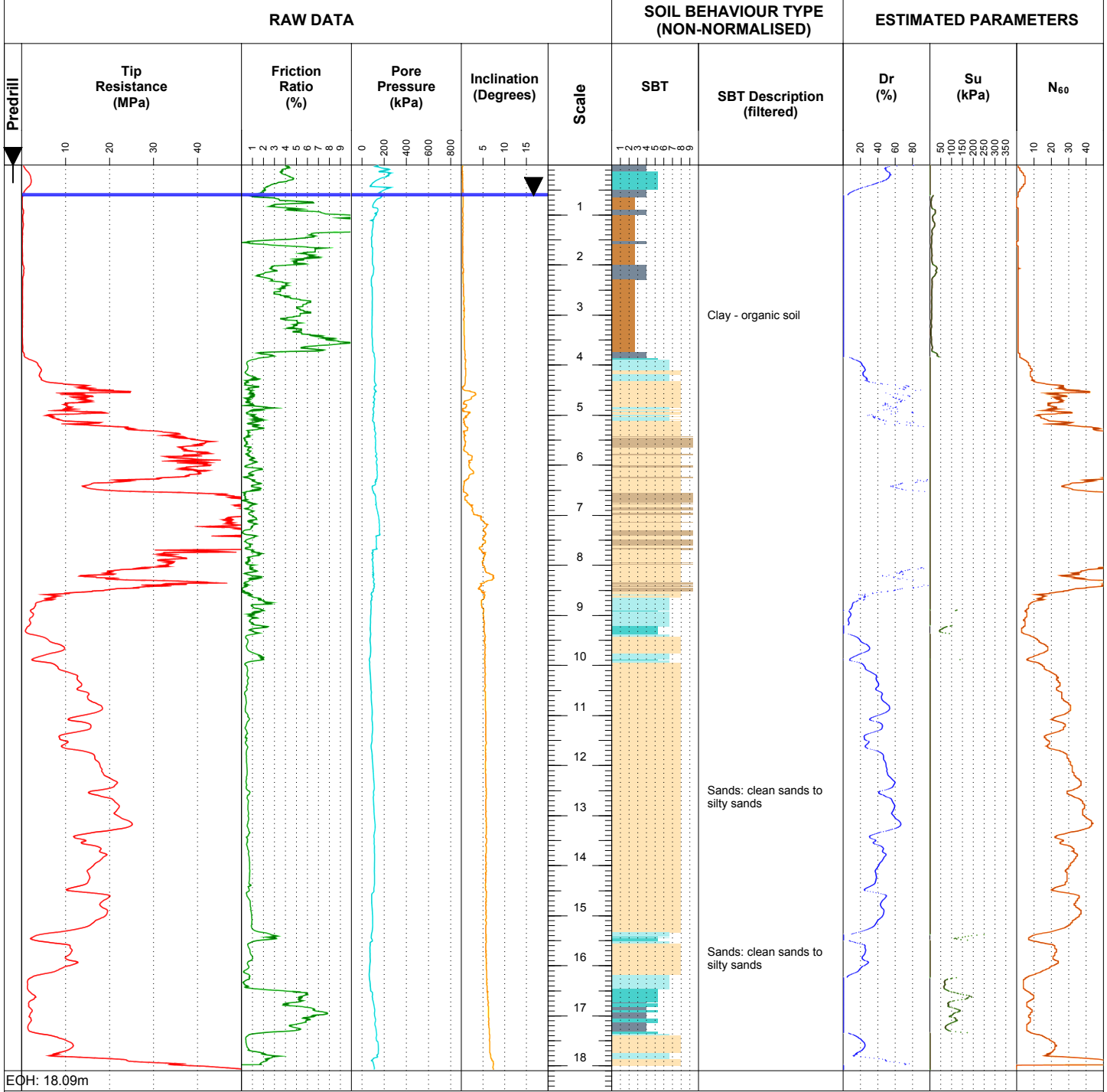
Job: 14784

CPT No.: CPTu102

Name: Cranford Basin
 Client: GHD NZ Ltd
 Location: 45 Grassmere Street, Christchurch

Grid: NZTM
 Datum: Ground
 Termination: -

North (m): 5184275.13
 East (m): 1569205.79
 Elevation (m): -
 Hole Depth (m): 18.09



EQH: 18.09m

Operator: S. Cardona

Date: 26/06/2015

Effective Refusal

Soil Behaviour Type (SBT) - Robertson et al. 1986

Rig: 14t truck mounted rig

Predrill: 0.00

Tip: ✓

Cone Reference: 100992T

Water Level: 0.60

Gauge:

Cone Area Ratio: 0.75

Collapse: 4.50

Inclinometer:

Cone Type: I-CFYXP20-10

Tip Resistance (MPa) Initial: -4.6763

Final: -4.4542

Local Friction (MPa) Initial: -0.0604

Final: -0.0627

Pore Pressure (KPa) Initial: -269.189

Final: -230.069

Other:

Target Depth:

0 Undefined

1 Sensitive fine-grained

2 Clay - organic soil

3 Clays: clay to silty clay

4 Silt mixtures: clayey silt & silty clay

5 Sand mixtures: silty sand to sandy silt

6 Sands: clean sands to silty sands

7 Dense sand to gravelly sand

8 Stiff sand to clayey sand

9 Stiff fine-grained

Notes & Limitations

Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. Both McMillan Drilling Ltd & Geroc Solutions Ltd do not warrant the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

Remarks

Effective Refusal

Hole Depth (m): 18.09

CONE PENETRATION TEST

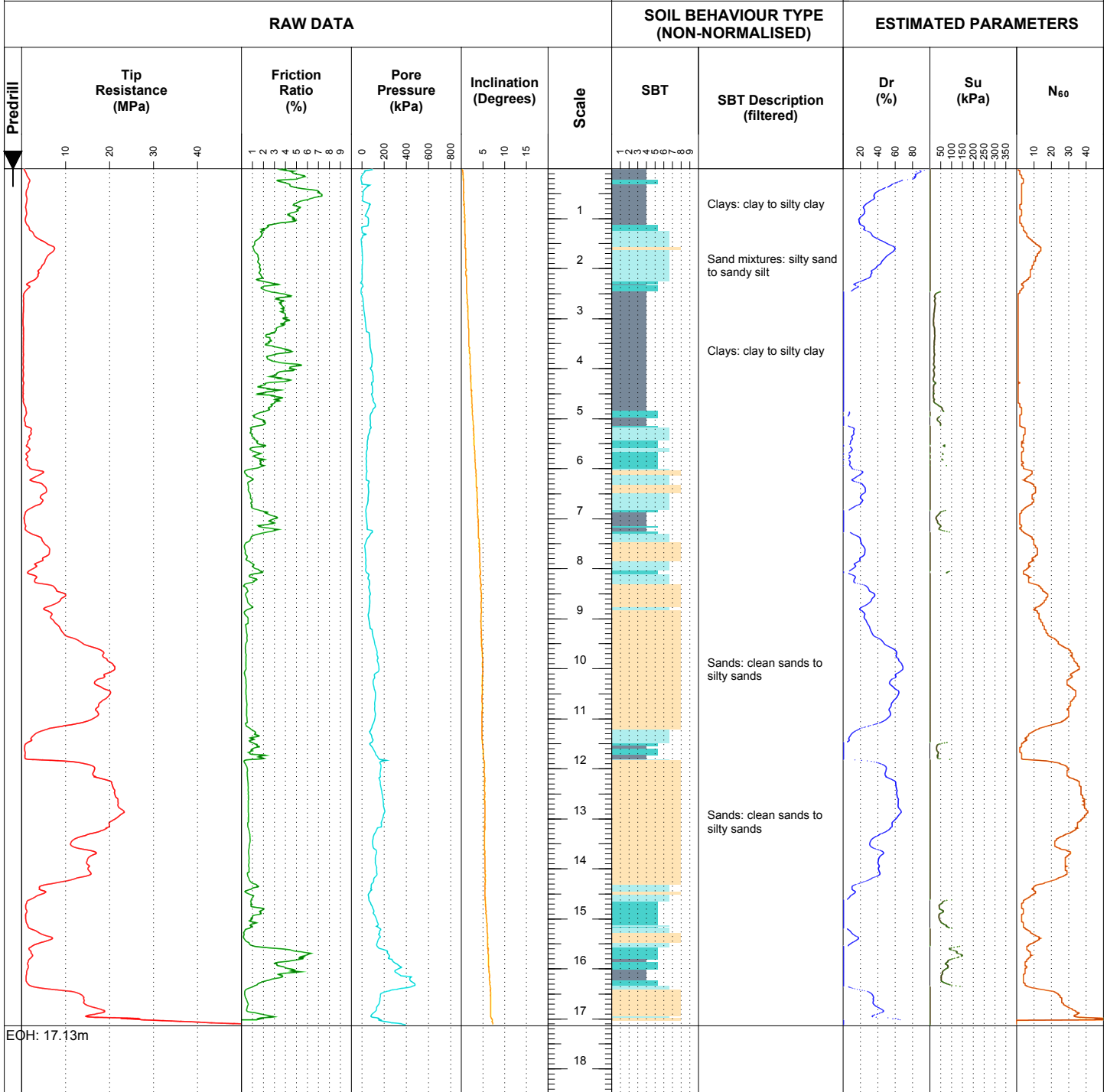
Job: 14784

CPT No.: CPTu103

Name: Cranford Basin
 Client: GHD NZ Ltd
 Location: 503 Cranford Street, Christchurch

Grid: NZTM
 Datum: Ground
 Termination: -

North (m): 5184523.00
 East (m): 1569299.52
 Elevation (m): -
 Hole Depth (m): 17.13



Operator: S. Cardona

Date: 25/06/2015

Effective Refusal

Soil Behaviour Type (SBT) - Robertson et al. 1986

Rig: 14t truck mounted rig

Predrill: 0.00

Tip: ✓

Cone Reference: 100992T

Water Level: -

Gauge:

Cone Area Ratio: 0.75

Collapse: 3.60

Inclinometer:

Cone Type: I-CFYXP20-10

Final: -4.7023

Other:

Tip Resistance (MPa) Initial: -4.9018

Final: -0.0624

Local Friction (MPa) Initial: -0.0565

Pore Pressure (KPa) Initial: -251.949

Final: -232.375

Target Depth:

0 Undefined

5 Sand mixtures: silty sand to sandy silt

1 Sensitive fine-grained

6 Sands: clean sands to silty sands

2 Clay - organic soil

7 Dense sand to gravelly sand

3 Clays: clay to silty clay

8 Stiff sand to clayey sand

4 Silt mixtures: clayey silt & silty clay

9 Stiff fine-grained

Notes & Limitations

Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. Both McMillan Drilling Ltd & GeroC Solutions Ltd do not warrant the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

Remarks

Effective Refusal

Hole Depth (m): 17.13

CONE PENETRATION TEST

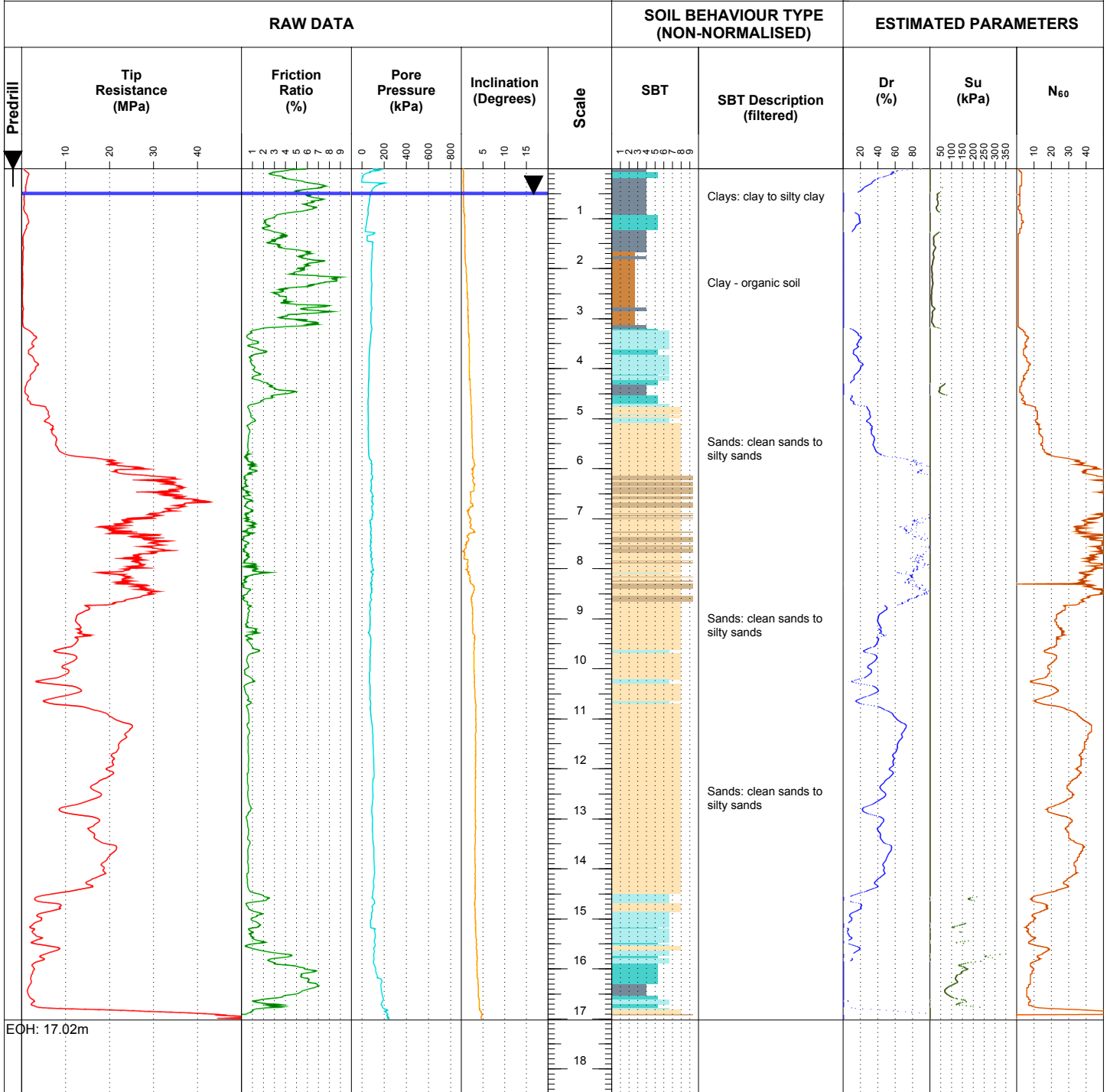
Job: 14784

CPT No.: CPTu104

Name: Cranford Basin
 Client: GHD NZ Ltd
 Location: 471 Cranford Street, Christchurch

Grid: NZTM
 Datum: Ground
 Termination: -

North (m): 5184434.20
 East (m): 1569474.94
 Elevation (m): -
 Hole Depth (m): 17.02



EOH: 17.02m

Operator: S. Cardona

Date: 25/06/2015

Effective Refusal

Soil Behaviour Type (SBT) - Robertson et al. 1986

Rig: 14t truck mounted rig

Predrill: 0.00

Tip: ✓

Cone Reference: 100992T

Water Level: 0.50

Gauge:

Cone Area Ratio: 0.75

Collapse: 2.40

Inclinometer:

Cone Type: I-CFYXP20-10

Tip Resistance (MPa) Initial: -4.8535

Final: -4.7471

Local Friction (MPa) Initial: -0.0542

Final: -0.0628

Pore Pressure (KPa) Initial: -253.544

Final: -219.617

Other:

Target Depth:

0 Undefined

1 Sensitive fine-grained

2 Clay - organic soil

3 Clays: clay to silty clay

4 Silt mixtures: clayey silt & silty clay

5 Sand mixtures: silty sand to sandy silt

6 Sands: clean sands to silty sands

7 Dense sand to gravelly sand

8 Stiff sand to clayey sand

9 Stiff fine-grained

Notes & Limitations

Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. Both McMillan Drilling Ltd & Geroc Solutions Ltd do not warrant the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

Remarks

Effective Refusal

Hole Depth (m): 17.02

TEST DETAIL

PointID: CPT101

Sounding: 101

Operator: P. Buunk
Cone Reference: 080238T
Cone Area Ratio: 0.75
Cone Type: I-CFXY-10

Date: 16/06/2015
Predrill: 0.50
Water Level: 1.30
Collapse:

Effective Refusal
Tip: ✓
Gauge:
Inclinometer:
Other:

Tip Resistance (MPa) Initial: -4.1778
Local Friction (MPa) Initial: -0.0362
Pore Pressure (kPa) Initial: -

Final: -4.1051
Final: -0.0364
Final: -

Target Depth:

PointID: CPTu102

Sounding: 102

Operator: S. Cardona
Cone Reference: 100992T
Cone Area Ratio: 0.75
Cone Type: I-CFXYP20-10

Date: 26/06/2015
Predrill: 0.00
Water Level: 0.60
Collapse: 4.50

Effective Refusal
Tip: ✓
Gauge:
Inclinometer:
Other:

Tip Resistance (MPa) Initial: -4.6763
Local Friction (MPa) Initial: -0.0604
Pore Pressure (kPa) Initial: -269.189

Final: -4.4542
Final: -0.0627
Final: -230.069

Target Depth:

PointID: CPTu103

Sounding: 103

Operator: S. Cardona
Cone Reference: 100992T
Cone Area Ratio: 0.75
Cone Type: I-CFXYP20-10

Date: 25/06/2015
Predrill: 0.00
Water Level: -
Collapse: 3.60

Effective Refusal
Tip: ✓
Gauge:
Inclinometer:
Other:

Tip Resistance (MPa) Initial: -4.9018
Local Friction (MPa) Initial: -0.0565
Pore Pressure (kPa) Initial: -251.949

Final: -4.7023
Final: -0.0624
Final: -232.375

Target Depth:

PointID: CPTu104

Sounding: 104

Operator: S. Cardona
Cone Reference: 100992T
Cone Area Ratio: 0.75
Cone Type: I-CFXYP20-10

Date: 25/06/2015
Predrill: 0.00
Water Level: 0.50
Collapse: 2.40

Effective Refusal
Tip: ✓
Gauge:
Inclinometer:
Other:

Tip Resistance (MPa) Initial: -4.8535
Local Friction (MPa) Initial: -0.0542
Pore Pressure (kPa) Initial: -253.544

Final: -4.7471
Final: -0.0628
Final: -219.617

Target Depth:

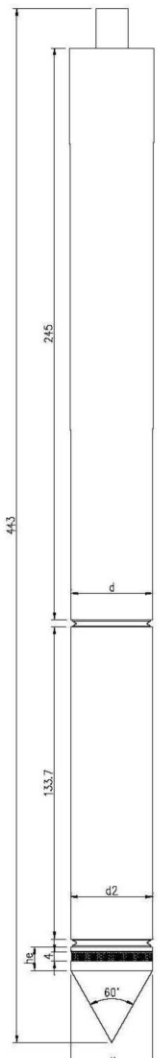
CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the following cone types:

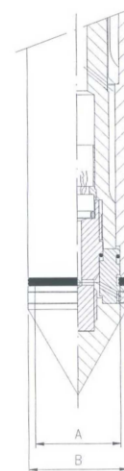
- ELCI-10CFXY measuring cone resistance, sleeve friction and inclination (standard cone);
- ELCI-CFXYP20-10 measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone).

Dimensions

Dimensional specifications for both cone types are detailed below. All tolerances are routinely checked prior to testing and measurements taken are manually recorded on CPT field sheets. All field sheets are kept on file and available on request.

A.P. van den Berg Machinefabriek tel.: +31 (0)513-631355 info@apvandenbergh.com	DEVIATION of Straightness + MINIMUM Dimensions tip, friction jacket, cone adaptor	Standards: EN ISO 22476-1 APB-standard
Type of cone: <u>ALLOWABLE SIZE VARIATION</u> Diameter of tip: Diameter of centering ring CFP Diameter of friction jacket: Height dimension of tip edge: <u>PRODUCTION DIMENSIONS</u> Tip: Jacket (C-cone): Friction jacket (CF-cone): Tip for used cone: <u>MINIMUM DIMENSIONS</u> Minimum diameter jacket (C-cone): Minimum diameter friction jacket (CF-cone): Use "used cone"-tip when friction jacket diameter: Minimum diameter of cone adaptor: Maximum deviation of straightness:	Icone 10 cm ² $35,3 \leq d_1 \leq 36,0$ $35,3 \leq d_1 \leq 36,0$ $d_1 \leq d_2 < d_1 + 0,35$ $7 \leq h_e \leq 10$ $d_1 = 35,7^{+0,2}_0$ $d_2 = 35,7^{+0,2}_0$ $d_2 = 35,9^{+0,1}_0$ $d_1 = 35,5^{+0,1}_0$ $d_2 = 35,2$ (APB standard) $d_2 = 35,3$ $d_2 \leq 35,65$ $d = 35,3$ 1 mm on a length of 1000 mm (max. oscillation 1,0 mm.)	

Cone surface ratio



$$A = 0,25 \times 3,14 \times 30,9 \times 30,9 = 750 \text{ MM}^2$$

$$B = 0,25 \times 3,14 \times 35,7 \times 35,7 = 1000 \text{ MM}^2$$

$$\alpha = A/B \quad \beta = 1 - A/B$$

$$\alpha = 750/1000 = 0,75$$

$$\beta = 1 - 0,75 = 0,25$$

CPT CALIBRATION AND TECHNICAL NOTES (cont.)

Calibration

Each cone has a unique identification number that is electronically recorded and reported for each CPT test. The identification number enables the operator to compare 'zero-load offsets' to manufacturer calibrated zero-load offsets.

The recommended maximum zero-load offset for each sensor is determined as $\pm 5\%$ of the nominal measuring range.

In addition to maximum zero-load offsets, McMillan Drilling also limits the difference in zero load offset before and after the test as $\pm 2\%$ of the maximum measuring range. See table below:

	Tip (MPa)	Friction (MPa)	Pore Pressure (MPa)
Maximum Measuring Range:	150	1.50	3.00
Nominal Measuring Range:	75	1.00	2.00
Max. 'zero-load offset':	7.5	0.10	0.20
Max 'before and after test':	3	0.03	0.06

Note: The zero offsets are electronically recorded and reported for each test in the same units as that of each sensor.

TEST CERTIFICATE Icône (all versions)		
Supplier:	A.P. van den Berg Machinefabriek, Heerenveen The Netherlands	
Production-order:	65193	
Client:	MC Milan	
Cone-type:	I-CFx4-10	
Cone-number:	080238	
To test / To check item	Required value	Checked value
Check Quad-ring groove behind friction sleeve with check ring ; Place ring behind friction sleeve without O-rings and Q-rings mounted Place friction sleeve, prepressure ring, centering ring and tighten tip	Sleeve fixed	✓
Isolation-resistance	>0.5 GΩ	✓ GΩ
Straightness total Icône (10 cm ²). (Base part Icône: S ≤ 0,2 mm) For dimensions 15cm Icones: see standard/table.	S ≤ 2,2 mm	✓ mm
All Measurements: Test with both GOnsite! v2.xx and v3.12.		
Check alarm-settings Icône. Alarm values are set. (Kill Shutdown)	O.K.	✓
Software version? Check at opening screen. NOTE DOWN version nr.:	Version:	1.8
Calibration date of Icône; check cone data [F1]..[F1]	O.K.	✓
Zero-Value Tip	Good	-4,317 MPa
Zero-Value Local Friction	Good	-0,042 MPa
Zero-Value Pore Pressure	Good	— kPa
Zero-Value Inclination X	-2° < X < +2°	-1,4 °
Zero-Value Inclination Y	-2° < Y < +2°	0,5 °
Measurements Tip resistance OK?	Yes	✓
Influence of Tip on Local Friction? Tip: Max Load ; Mantle free? 10cm ² : 150 kN. // 15 cm ² : 150 kN.	150 MPa	✓
Measurements Local Friction OK?	Yes	✓
Local Friction: Max Load	O.K.	✓
Measurements Pore Pressure OK?	Yes	—
Measure Pore Pressure to 150%	O.K.	—
Measurements Inclination OK?	Yes	✓
Cone recognition on disconnecting and connecting Icône again?	Yes	✓
Remarks:		

Calibrated by: C.J. Ouwéjan	Date: 28.08.14	Sign.:
Final check: E.v.d. Pijl	Date: 29.08.14	Sign.:

Work instructions: H:\Electro\Productie\Icône\beschrijving beproeving Icones.doc.

R:\E&D\Beproevingprotocollen\Beproevingprotocol Icône English.doc

TEST CERTIFICATE Icône (all versions)		
Supplier:	A.P. van den Berg Machinefabriek, Heerenveen The Netherlands	
Production-order:	65193	
Client:	MC. Milan	
Cone-type:	I-CFxYP 20-10	
Cone-number:	100992	
To test / To check item	Required value	Checked value
Check Quad-ring groove behind friction sleeve with check ring ; Place ring behind friction sleeve without O-rings and Q-rings mounted Place friction sleeve, prepressure ring, centering ring and tighten tip	Sleeve fixed	<i>f</i>
Isolation-resistance	>0.5 GΩ	<i>f</i> GΩ
Straightness total Icône (10 cm ²). (Base part Icône: S ≤ 0,2 mm) For dimensions 15cm Icones: see standard/table.	S ≤ 2,2 mm	<i>f</i> mm
All Measurements: Test with both GOnsite! v2.xx and v3.12.		
Check alarm-settings Icône. Alarm values are set. (Kill Shutdown)	O.K.	<i>f</i>
Software version? Check at opening screen. NOTE DOWN version nr.:	Version:	1.08°
Calibration date of Icône; check cone data [F1]..[F1]	O.K.	<i>f</i>
Zero-Value Tip	Good	-5,266 MPa
Zero-Value Local Friction	Good	-0,1005 MPa
Zero-Value Pore Pressure	Good	-257 kPa
Zero-Value Inclination X Zero-Value Inclination Y	-2° < X < +2° -2° < Y < +2°	0,0 ° -6,1 °
Measurements Tip resistance OK?	Yes	<i>f</i>
Influence of Tip on Local Friction? Tip: Max Load ; Mantle free? 10cm ² : 150 kN. // 15 cm ² : 150 kN.	150 MPa	<i>f</i>
Measurements Local Friction OK?	Yes	<i>f</i>
Local Friction: Max Load	O.K.	<i>f</i>
Measurements Pore Pressure OK?	Yes	<i>f</i>
Measure Pore Pressure to 150%	O.K.	<i>f</i>
Measurements Inclination OK?	Yes	<i>f</i>
Cone recognition on disconnecting and connecting Icône again?	Yes	<i>f</i>
Remarks:		

Calibrated by: <i>C. J. Ouwéjan</i>	Date: <i>20.00.14</i>	Sign.: <i>[Signature]</i>
Final check: <i>Ewim vd Duijn</i>	Date: <i>29.00.14</i>	Sign.: <i>[Signature]</i>

Work instructions: H:\Electro\Productie\Icône\beschrijving beproeving Icones.doc.

R:\E&D\Beproeingsprotocollen\Beproeingsprotocol Icône English.doc

Appendix D – (Laboratory Results)



Our Ref: 616674.000/Rep1
Customer Ref: 5133038
27 July 2015
Page 1 of 6

GHD
PO Box 13 468
Christchurch
Auckland

Attention: Mr Darren Woods

Dear Darren

LABORATORY TEST REPORT
Cranford Street, Christchurch

Sampling Procedure

Samples have been tested as received from the customer.

Sample/Test Location Plan

None.

Samples

Four push tube samples were delivered to our laboratory.

Date of Sample Receipt

09 July 2015.

Customer's Instructions

Testing instructions provided by Darren Woods of GHD.

Test Method

NZS 4402:1986 Test 7.1 One-dimensional consolidation.

Test Results

See pages 3 to 6.

Test Remarks

See pages 3 to 6.

Sample Descriptions

See pages 3 to 6.

General Remarks

Samples were destroyed during testing.

Descriptions are enclosed for your information, but are not covered under our scope of IANZ accreditation.

Please reproduce the report in full when transmitting to others or including in internal reports.

If we can be of any further assistance, feel free to call us on phone.

GEOTECHNICS LTD

Report prepared by:

Authorised for Geotechnics by:

.....
Sim Tirunahari
Soils Laboratory Manager

.....
Steven Anderson
PROJECT DIRECTOR
Approved Signatory

Report checked by:

.....
Steven Anderson
Regional Manager
Approved Signatory

Site: **Cranford Street, Christchurch**

Our Job No.: 616674.000

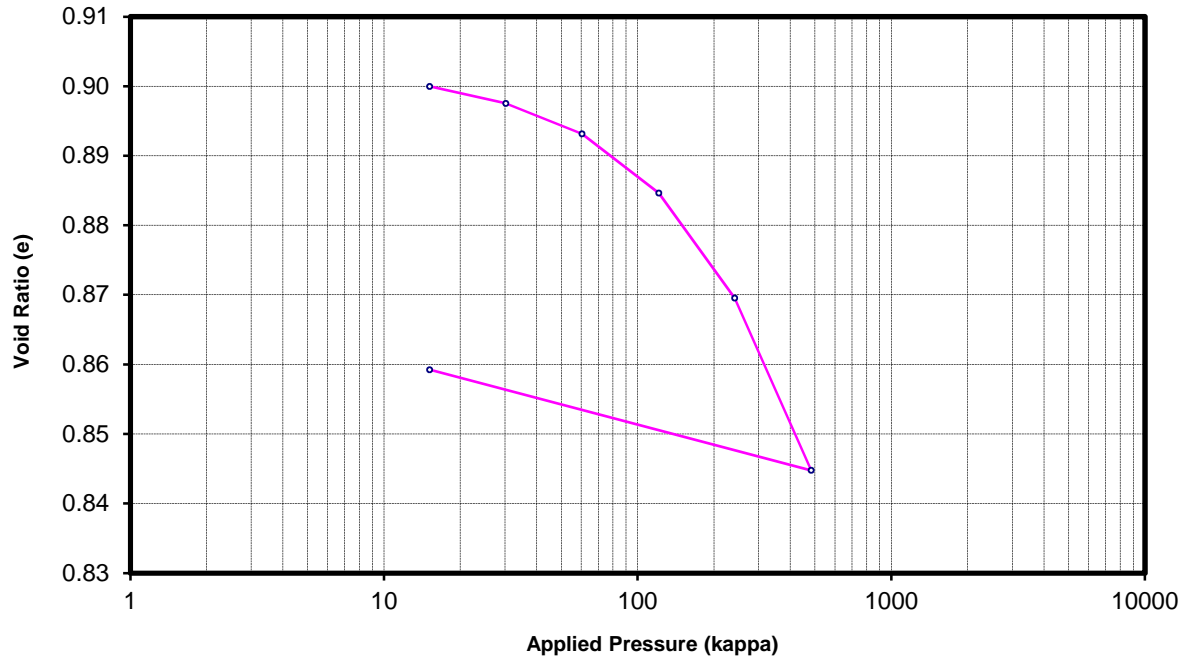
BH No.: 101

Sample No.: ---

Depth: 2.50-2.55 (m)

Test Method Used: NZS 4402:1986 Test 7.1 One-Dimensional Consolidation

ONE-DIMENSIONAL CONSOLIDATION TEST



Pressure (kPa)	Void Ratio (e)	Pressure Increment (kPa)	Coefficient of Consolidation C_v (m ² /yr)	Coefficient of Volume Compressibility M_v (m ² /MN)
As received	0			
Preload	15.1	0 to 15.1	NA	0.090
	30.2	15.1 to 30.2	38	0.085
	60.3	30.2 to 60.3	32	0.077
	121	60.3 to 121	16	0.074
	241	121 to 241	14	0.067
	483	241 to 483	12	0.055
Unload	15.1	483 to 15.1	NA	NA

Sample History: Undisturbed core trimmed at NWC. SQR of time fitting method used.

Description: sandy SILT with trace of clay, firm, light greenish grey.

Initial Dry Density (t/m³): 1.41 Initial Water Content: 32.6%

Solid Density (t/m³): 2.68 (Assumed) Initial Saturation: 97%

Temperature During Testing: Max = 16 °C Min = 15 °C

Remarks: The calculations of void ratio are affected by the solid density value. We have assumed a value of 2.68 t/m³.

Sample description is not IANZ accredited.

Entered by: ST

Date: 24.07.2015

Checked by: MP

Date: 24.07.2015

Site: **Cranford Street, Christchurch**

Our Job No.: 616674.000

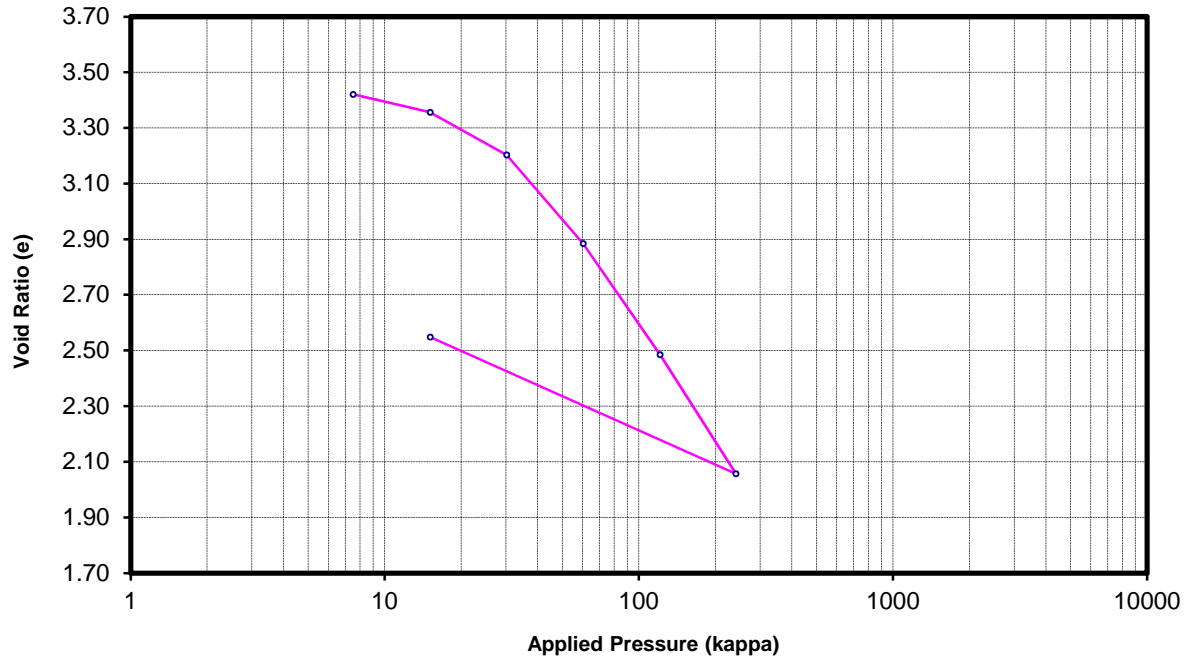
BH No.: 102

Sample No.: ---

Depth: 3.65-3.70 (m)

Test Method Used: NZS 4402:1986 Test 7.1 One-Dimensional Consolidation

ONE-DIMENSIONAL CONSOLIDATION TEST



Pressure (kPa)	Void Ratio (e)	Pressure Increment (kPa)	Coefficient of Consolidation C_v (m ² /yr)	Coefficient of Volume Compressibility M_v (m ² /MN)
As received	0	3.492		
Preload	7.5	3.421	0 to 7.5	NA
	15.1	3.356	7.5 to 15.1	2.6
	30.2	3.203	15.1 to 30.2	2.0
	60.3	2.884	30.2 to 60.3	1.3
	121	2.485	60.3 to 121	1.0
	241	2.057	121 to 241	0.74
Unload	15.1	2.549	241 to 15.1	NA

Sample History: Undisturbed core trimmed at NWC. SQR of time fitting method used.

Description: Organic SILT with trace to minor clay and trace of sand, few rootlets, soft, dark brown-black mixed with light greenish grey.

Initial Dry Density (t/m³): 0.53 Initial Water Content: 141%

Solid Density (t/m³): 2.40 (Assumed) Initial Saturation: 97%

Temperature During Testing: Max = 16 °C Min = 15 °C

Remarks: The calculations of void ratio are affected by the solid density value. We have assumed a value of 2.40 t/m³.

Sample description is not IANZ accredited.

Entered by: ST

Date: 24.07.2015

Checked by: MP

Date: 24.07.2015

Site: **Cranford Street, Christchurch**

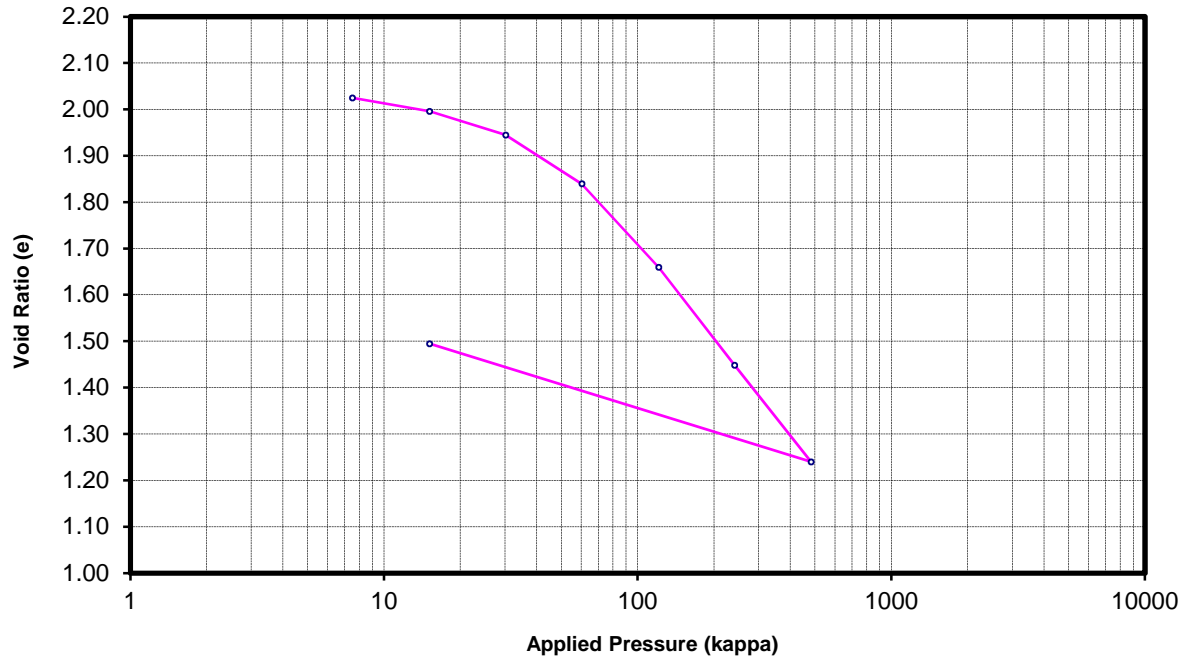
Our Job No.: 616674.000

BH No.: 103 Sample No.: ---

Depth: 3.05-3.10 (m)

Test Method Used: NZS 4402:1986 Test 7.1 One-Dimensional Consolidation

ONE-DIMENSIONAL CONSOLIDATION TEST



Pressure (kPa)	Void Ratio (e)	Pressure Increment (kPa)	Coefficient of Consolidation Cv (m ² /yr)	Coefficient of Volume Compressibility Mv (m ² /MN)
As received	0	2.057		
Preload	7.5	2.025	0 to 7.5	NA
	15.1	1.996	7.5 to 15.1	3.7
	30.2	1.945	15.1 to 30.2	3.2
	60.3	1.839	30.2 to 60.3	2.6
	121	1.660	60.3 to 121	2.2
	241	1.449	121 to 241	1.9
	483	1.240	241 to 483	1.8
Unload	15.1	1.495	483 to 15.1	NA

Sample History: Undisturbed core trimmed at NWC. SQR of time fitting method used.

Description: SILT with minor to some organics and trace to minor clay, trace of sand, few rootlets, soft, dark brown-black mixed with light greenish grey.

Initial Dry Density (t/m³): 0.82 Initial Water Content: 79.0%

Solid Density (t/m³): 2.50 (Assumed) Initial Saturation: 96%

Temperature During Testing: Max = 16 °C Min = 15 °C

Remarks: The calculations of void ratio are affected by the solid density value. We have assumed a value of 2.50 t/m³.

Sample description is not IANZ accredited.

Site: **Cranford Street, Christchurch**

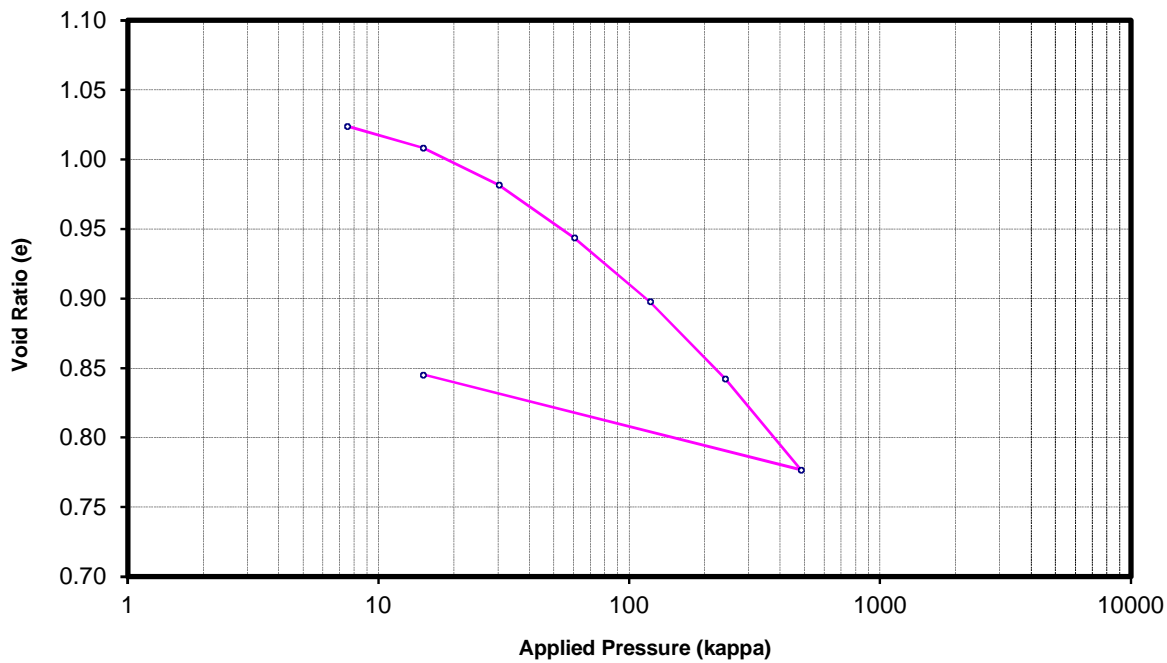
Our Job No.: 616674.000

BH No.: **104** Sample No.: ---

Depth: 3.10-3.15 (m)

Test Method Used: NZS 4402:1986 Test 7.1 One-Dimensional Consolidation

ONE-DIMENSIONAL CONSOLIDATION TEST



Pressure (kPa)	Void Ratio (e)	Pressure Increment (kPa)	Coefficient of Consolidation Cv (m ² /yr)	Coefficient of Volume Compressibility Mv (m ² /MN)
As received	0	1.042		
Preload	7.5	1.024	0 to 7.5	NA
	15.1	1.008	7.5 to 15.1	2.8
	30.2	0.982	15.1 to 30.2	4.1
	60.3	0.944	30.2 to 60.3	5.8
	121	0.898	60.3 to 121	7.9
	241	0.842	121 to 241	11
	483	0.777	241 to 483	14
Unload	15.1	0.845	483 to 15.1	NA

Sample History: Undisturbed core trimmed at NWC. SQR of time fitting method used.

Description: SILT with trace to minor clay and trace of sand, few rootlets, soft, light greenish grey, mottled dark brown.

Initial Dry Density (t/m³): 1.31 Initial Water Content: 37.8%

Solid Density (t/m³): 2.68 (Assumed) Initial Saturation: 97%

Temperature During Testing: Max = 16 °C Min = 15 °C

Remarks: The calculations of void ratio are affected by the solid density value. We have assumed a value of 2.68 t/m³.

Sample description is not IANZ accredited.

Appendix E - (Liquefaction Analysis)

Provided as separate appendix document

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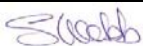

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Rev No.	Author	Reviewer		Approved for Issue		
		Name	Signature	Name	Signature	Date
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