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Styx River Conservation Reserve – Walnut Tree Lookout

Qualitative Engineering Evaluation

Functional Location ID: PRK 2625 BLDG 001

Address: 53 Willowview Drive, Redwood

Reference: 231556

Prepared for:

Christchurch City Council

Revision: 2

Date: 14 October 2013

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Current Revision		**2**				

Approval			
Author Signature		Approver Signature	
Name	Thomas Bolton	Name	Luis Castillo
Title	Structural Engineer	Title	Senior Structural Engineer

Contents

Appendices

Executive Summary

This is a summary of the Qualitative Engineering Evaluation for the Styx River Conservation Reserve – Walnut Tree Lookout and is based on the Detailed Engineering Evaluation Procedure document issued by the Engineering Advisory Group on 19 July 2011, visual inspections, available structural documentation and summary calculations as appropriate.

Building Details	**Name**	Styx River Conservation Reserve – Walnut Tree Lookout			
Building Address	53 Willowview Drive, Redwood			**No. of residential units**	1
Soil Technical Category	N/A	**Importance Level**	1	**Approximate Year Built**	2009
Foot Print (m^2)	30	**Stories above ground**	1	**Stories below ground**	0
Type of Construction	No roof, reinforced blockwork retaining walls with concrete barriers and it is assumed to be founded on concrete strip footings.				
Qualitative Results Summary					
Building Occupied	Y	The Styx River Conservation Reserve – Walnut Tree Lookout is currently in use.			
Suitable for Continued Occupancy	Y	The Styx River Conservation Reserve – Walnut Tree Lookout is suitable for continued occupation.			
Key Damage Summary	Y	Refer to summary of building damage Section 3.1 report body.			
Critical Structural Weaknesses (CSW)	N	No critical structural weaknesses were identified.			
Levels Survey Results	Y	Variations in floor levels were within the MBIE Guidelines, with falls of less than 1:200 or 0.5%			
Building %NBS From Analysis	73%	Based on direct comparison of codes.			
Qualitative Report Recommendations					
Geotechnical Survey Required	N	Geotechnical survey not required due to lack of observed ground damage on site.			
Proceed to L5 Quantitative DEE	N	A quantitative DEE is not required for this structure.			
Approval					
Author Signature			**Approver Signature**		
Name	Thomas Bolton		**Name**	Luis Castillo	
Title	Structural Engineer		**Title**	Senior Structural Engineer	

1 Introduction

1.1 General

On 10 September 2012 an Aurecon engineer visited the Styx River Conservation Reserve – Walnut Tree Lookout to carry out a qualitative building damage assessment on behalf of Christchurch City Council. Detailed visual inspections were carried out to assess the damage caused by the earthquakes on 4 September 2010, 22 February 2011, 13 June 2011, 23 December 2011 and related aftershocks.

The scope of work included:

- Assessment of the nature and extent of the building damage.
- Visual assessment of the building strength particularly with respect to safety of occupants if the building is currently occupied.
- Assessment of requirements for detailed engineering evaluation including geotechnical investigation, level survey and any areas where linings and floor coverings need removal to expose structural damage.

This report outlines the results of our Qualitative Assessment of damage to the Styx River Conservation Reserve – Walnut Tree Lookout and is based on the Detailed Engineering Evaluation Procedure document issued by the Structural Advisory Group on 19 July 2011, visual inspections, available structural documentation and summary calculations as appropriate.

2 Description of the Building

2.1 Building Age and Configuration

Built in/around 2009 the Styx River Conservation Reserve – Walnut Tree Lookout is a timber deck with a stack bond retaining wall on three sides. The retaining wall supports heavy precast panels which form a barrier for the viewing platform. The lower 2.6 metres of the retaining wall is blockwork with reinforcing every 400mm vertically and 600mm horizontally. The concrete panels are reinforced 150mm in both directions, on both faces. The 2.6 metre retaining wall is retaining up to 1.9 metres of soil. In the northwest corner of the structure there is a steel frame cantilevering 3.2 metres from the cantilever wall and the steel frame is supporting a timber deck. Behind the cantilever walls there is a timber deck supported on timber piles on the retained fill. The approximate floor area of the deck within the retaining walls is 30 square metres. It is an importance level 1 structure in accordance with NZS 1170 Part 0:2002.

2.2 Building Structural Systems Vertical and Horizontal

The Styx River Conservation Reserve – Walnut Tree Lookout is a simple structure, though of unusual design. The timber deck is supported by timber piles on the retained fill. There is a gap between the deck and the retaining wall preventing transfer of loads from the deck directly into the retaining wall. The retaining wall is expected to resist lateral loads from its self-weight, the inertial load from the precast panels supported on top and the retained soil as a cantilever out of plane and a shear wall in plane.

2.3 Reference Building Type

The Styx River Conservation Reserve – Walnut Tree Lookout is a bespoke lookout structure. We assume it was has been subject to specific design based on its unique design, wide range of building materials and height of retaining walls.

2.4 Building Foundation System and Soil Conditions

The Styx River Conservation Reserve – Walnut Tree Lookout, as discussed above, is assumed to have concrete strip foundations below the retaining wall. The timber deck is supported on timber piles. The land and surrounds of Styx River Conservation Reserve – Walnut Tree Lookout are zoned N/A which means that no mapping of the land with respect to technical categories has been done. However, there are no signs in the vicinity of Styx River Conservation Reserve – Walnut Tree Lookout of liquefaction bulges or boils and subsidence.

2.5 Available Structural Documentation and Inspection Priorities

No drawings were available for the Styx River Conservation Reserve – Walnut Tree Lookout. Inspection priorities related to a review of potential damage. The Styx River Conservation Reserve – Walnut Tree Lookout does not have a specific building type, its main structural element is a modern reinforced blockwork retaining wall which has performed well during the Canterbury Earthquakes.

2.6 Available Survey Information

A floor level survey was undertaken to establish the level of unevenness across the floors. The results of the survey are presented on the attached sketch in Appendix A. All of the levels were taken on top of the existing floor coverings which may have introduced some margin of error.

The Ministry of Business, Innovation and Employment (MBIE) published the guideline "Repairing and rebuilding houses affected by the Canterbury earthquakes" in 2012, which recommends some form of re-levelling or rebuilding of the floor

1. If the slope is greater than 0.5% for any two points more than 2m apart, or
2. If the variation in level over the floor plan is greater than 50mm, or
3. If there is significant cracking of the floor.

It is important to note that these figures are recommendations and are only intended to be applied to residential buildings. However, they provide useful guidance in determining acceptable floor level variations.

The floor levels for the Styx River Conservation Reserve – Walnut Tree Lookout were found to be within the recommended tolerances with slopes less than 0.5%.

3 Structural Investigation

3.1 Summary of Building Damage

The Styx River Conservation Reserve – Walnut Tree Lookout is currently in use and was occupied at the time the damage assessment was carried out.

The Styx River Conservation Reserve – Walnut Tree Lookout has performed well and has suffered no damage, the retaining walls are within 0.3 degrees of perfectly vertical.

3.2 Record of Intrusive Investigation

No damage was observed therefore, an intrusive investigation was neither warranted nor undertaken for the Styx River Conservation Reserve – Walnut Tree Lookout. A lot of the structure could be seen by visual inspection, and scanning of the concrete and masonry structure confirmed that they were reinforced.

3.3 Damage Discussion

There was no observed damage to the Styx River Conservation Reserve – Walnut Tree Lookout as a result of seismic actions.

4 Building Review Summary

4.1 Building Review Statement

As noted above no intrusive investigations were carried out for the Styx River Conservation Reserve – Walnut Tree Lookout. Because of the generic nature of the building a significant amount of information can be inferred from an external and internal inspection.

4.2 Critical Structural Weaknesses

No specific critical structural weaknesses were identified as part of the building qualitative assessment.

5 Building Strength (Refer to Appendix C for background information)

5.1 General

The Styx River Conservation Reserve – Walnut Tree Lookout is, as discussed above, a bespoke structure. The Styx River Conservation Reserve – Walnut Tree Lookout has performed well and there is no damage to the structure related to the recent earthquakes.

5.2 Initial %NBS Assessment

It is assumed the Styx River Conservation Reserve – Walnut Tree Lookout has been subject to specific engineering design and is also it is a relatively new structure, therefore we can assess the capacity using a direct code comparison. The seismic hazard factor for Canterbury increased from

0.22 given in NZS1170.5:2004 to 0.30 given as an amendment to the building code B1: Structure (in force from 19 May 2011 onwards).

Using a direct code comparison we can find that the building strength is approximately 0.22/0.3 = 73% of the new building standard. This assumes that the building was constructed exactly to code, it is likely that it was designed to be slightly above this.

5.3 Results Discussion

A direct code comparison shows that the Styx River Conservation Reserve – Walnut Tree Lookout is capable of achieving seismic performance in line with 73% of the current code requirements. The lack of damage or rotation of retaining walls suggests that this is an accurate result.

6 Conclusions and Recommendations

As there is no clear evidence of any liquefaction or ground movement in the vicinity of the Styx River Conservation Reserve – Walnut Tree Lookout **a geotechnical investigation is currently not considered necessary**.

The building is currently occupied and in use and in our opinion the Styx River Conservation Reserve – Walnut Tree Lookout **is considered suitable for continued occupation**.

7 Explanatory Statement

The inspections of the building discussed in this report have been undertaken to assess structural earthquake damage. No analysis has been undertaken to assess the strength of the building or to determine whether or not it complies with the relevant building codes, except to the extent that Aurecon expressly indicates otherwise in the report. Aurecon has not made any assessment of structural stability or building safety in connection with future aftershocks or earthquakes – which have the potential to damage the building and to jeopardise the safety of those either inside or adjacent to the building, except to the extent that Aurecon expressly indicates otherwise in the report.

This report is necessarily limited by the restricted ability to carry out inspections due to potential structural instabilities/safety considerations, and the time available to carry out such inspections. The report does not address defects that are not reasonably discoverable on visual inspection, including defects in inaccessible places and latent defects. Where site inspections were made, they were restricted to external inspections and, where practicable, limited internal visual inspections.

To carry out the structural review, existing building drawings were obtained from the Christchurch City Council records. We have assumed that the building has been constructed in accordance with the drawings.

While this report may assist the client in assessing whether the building should be repaired, strengthened, or replaced that decision is the sole responsibility of the client.

This review has been prepared by Aurecon at the request of its client and is exclusively for the client's use. It is not possible to make a proper assessment of this review without a clear understanding of the terms of engagement under which it has been prepared, including the scope of the instructions and directions given to and the assumptions made by Aurecon. The report will not address issues which would need to be considered for another party if that party's particular circumstances, requirements and experience were known and, further, may make assumptions about matters of which a third party is not aware. No responsibility or liability to any third party is accepted for any loss or damage whatsoever arising out of the use of or reliance on this report by any third party.

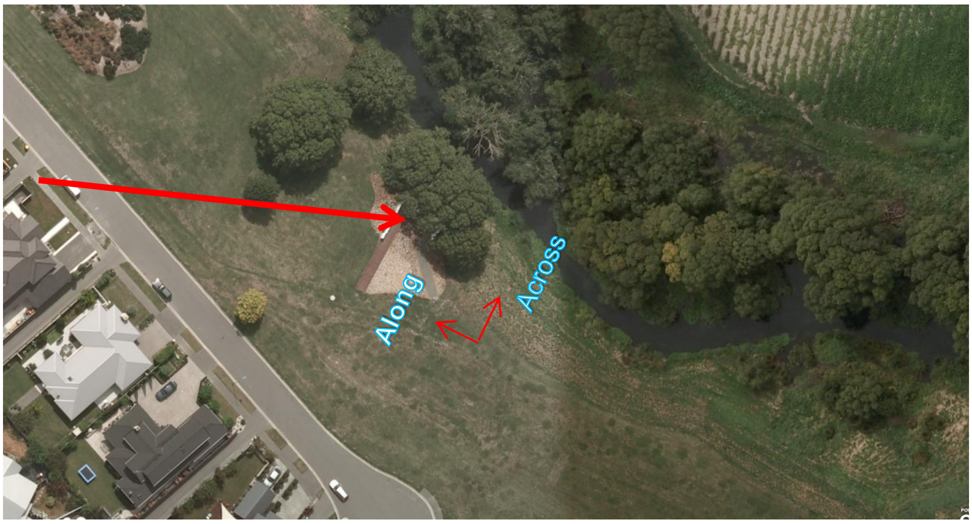
Without limiting any of the above, Aurecon's liability, whether under the law of contract, tort, statute, equity or otherwise, is limited as set out in the terms of the engagement with the client.

Appendices

Appendix A

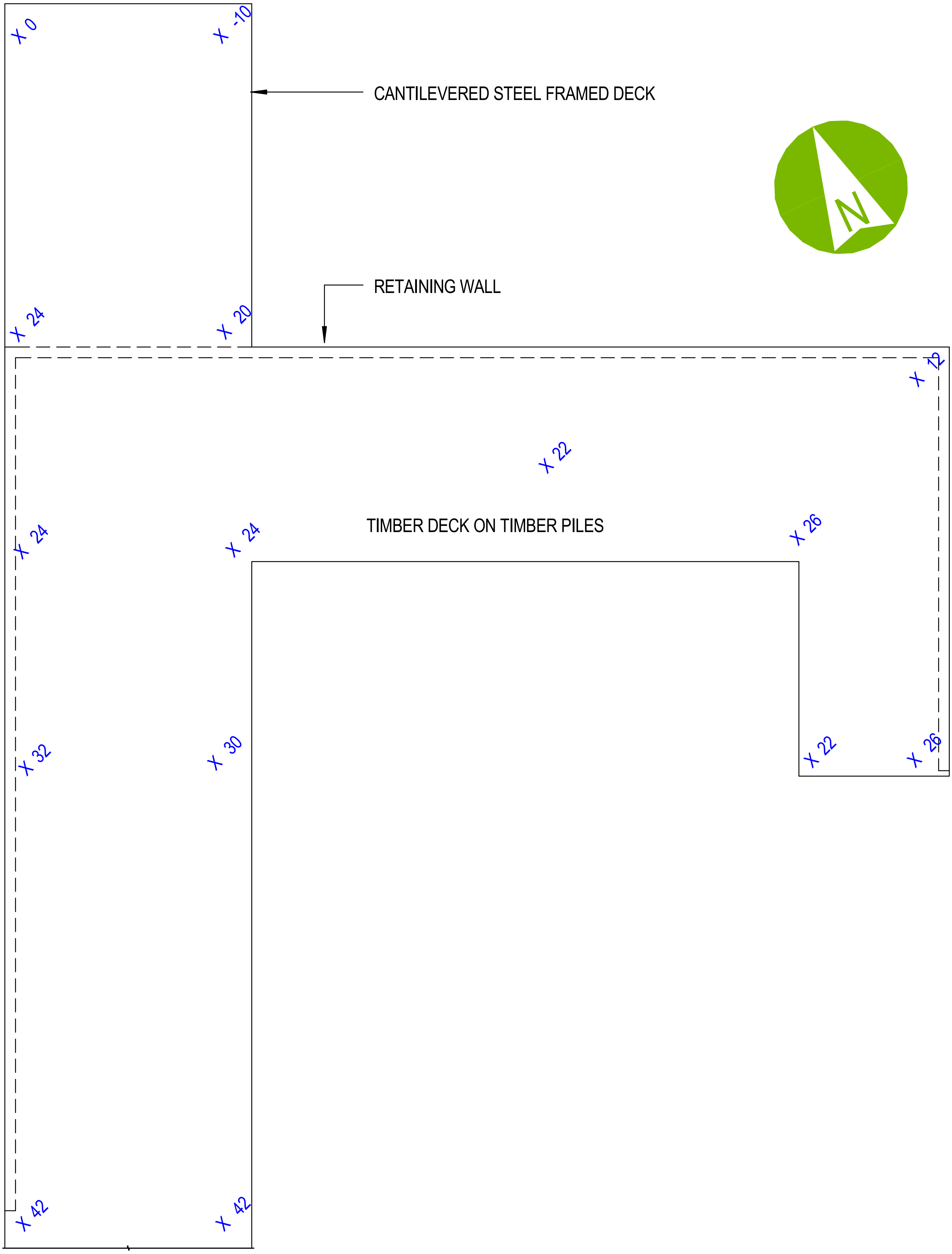
Site Map, Photos and Levels Survey Results

10 September 2012 – Styx River Conservation Reserve – Walnut Tree Lookout Site Photographs

Location of Styx River Conservation Reserve – Walnut Tree Lookout.	
Aerial photograph of Styx River Conservation Reserve – Walnut Tree Lookout.	

Structure northern elevation.	
Structure western elevation.	

Structure eastern elevation.	
Structure Southern elevation.	



PLAN - LEVELS

1 : 50

12/09/2012 1:20:32 p.m.

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CLIENT: Christchurch City Council

REV	DATE	REVISION DETAILS	APPROVAL
A	12.09.12	PRELIMINARY	APP

DRAWN	DESIGNED
N.Stanojevic	S.Waldrip

CHECKED: Checker

APPROVED: Approver DATE

PROJECT: STYX RIVER CONSERVATION LOOKOUT

TITLE: PLAN - LEVELS

PRELIMINARY
NOT FOR CONSTRUCTION

PROJECT No.	SCALE	SIZE	DRAWING No.	REV
231556	1 : 50	A4	S-01-00	A

Appendix B
References

1. The Ministry of Business, Innovation and Employment (MBIE) “Repairing and rebuilding houses affected by the Canterbury earthquakes”, 2012

2. New Zealand Society for Earthquake Engineering (NZSEE), “Assessment and Improvement of the Structural Performance of Buildings in Earthquakes”, April 2012

3. Standards New Zealand, “AS/NZS 1170 Part 0, Structural Design Actions: General Principles”, 2002

4. Standards New Zealand, “AS/NZS 1170 Part 1, Structural Design Actions: Permanent, imposed and other actions”, 2002

5. Standards New Zealand, “NZS 1170 Part 5, Structural Design Actions: Earthquake Actions – New Zealand”, 2004

6. Standards New Zealand, “NZS 3101 Part 1, The Design of Concrete Structures”, 2006

7. Standards New Zealand, “NZS 3404 Part 1, Steel Structures Standard”, 1997

8. Standards New Zealand, “NZS 3606, Timber Structures Standard”, 1993

9. Standards New Zealand, “NZS 3604, Timber Framed Structures”, 2011

10. Standards New Zealand, “NZS 4229, Concrete Masonry Buildings Not Requiring Specific Engineering Design”, 1999

11. Standards New Zealand, “NZS 4230, Design of Reinforced Concrete Masonry Structures”, 2004

Appendix C
Strength Assessment Explanation

New building standard (NBS)

New building standard (NBS) is the term used with reference to the earthquake standard that would apply to a new building of similar type and use if the building was designed to meet the latest design Codes of Practice. If the strength of a building is less than this level, then its strength is expressed as a percentage of NBS.

Earthquake Prone Buildings

A building can be considered to be earthquake prone if its strength is less than one third of the strength to which an equivalent new building would be designed, that is, less than 33%NBS (as defined by the New Zealand Building Act). If the building strength exceeds 33%NBS but is less than 67%NBS the building is considered at risk.

Christchurch City Council Earthquake Prone Building Policy 2010

The Christchurch City Council (CCC) already had in place an Earthquake Prone Building Policy (EPB Policy) requiring all earthquake-prone buildings to be strengthened within a timeframe varying from 15 to 30 years. The level to which the buildings were required to be strengthened was 33%NBS.

As a result of the 4 September 2010 Canterbury earthquake the CCC raised the level that a building was required to be strengthened to from 33% to 67% NBS but qualified this as a target level and noted that the actual strengthening level for each building will be determined in conjunction with the owners on a building-by-building basis. Factors that will be taken into account by the Council in determining the strengthening level include the cost of strengthening, the use to which the building is put, the level of danger posed by the building, and the extent of damage and repair involved.

Irrespective of strengthening level, the threshold level that triggers a requirement to strengthen is 33%NBS.

As part of any building consent application fire and disabled access provisions will need to be assessed.

Christchurch Seismicity

The level of seismicity within the current New Zealand loading code (AS/NZS 1170) is related to the seismic zone factor. The zone factor varies depending on the location of the building within NZ. Prior to the 22nd February 2011 earthquake the zone factor for Christchurch was 0.22. Following the earthquake the seismic zone factor (level of seismicity) in the Christchurch and surrounding areas has been increased to 0.3. This is a 36% increase.

For this assessment, the building's earthquake resistance is compared with the current New Zealand Building Code requirements for a new building constructed on the site. This is expressed as a percentage of new building standard (%NBS). The new building standard load requirements have been determined in accordance with the current earthquake loading standard (NZS 1170.5:2004 Structural design actions - Earthquake actions - New Zealand).

The likely capacity of this building has been derived in accordance with the New Zealand Society for Earthquake Engineering (NZSEE) guidelines 'Assessment and Improvement of the Structural Performance of Buildings in Earthquakes' (AISPBE), 2006. These guidelines provide an Initial Evaluation Procedure that assesses a buildings capacity based on a comparison of loading codes from when the building was designed and currently. It is a quick high-level procedure that can be used when undertaking a Qualitative analysis of a building. The guidelines also provide guidance on calculating a modified Ultimate Limit State capacity of the building which is much more accurate and can be used when undertaking a qualitative analysis.

The New Zealand Society for Earthquake Engineering has proposed a way for classifying earthquake risk for existing buildings in terms of %NBS and this is shown in Figure C1 below.

Description	Grade	Risk	%NBS	Existing Building Structural Performance	Improvement of Structural Performance: Legal Requirement	Improvement of Structural Performance: NZSEE Recommendation
Low Risk Building	A or B	Low	Above 67	Acceptable (improvement may be desirable)	The Building Act sets no required level of structural improvement (unless change in use) This is for each TA to decide. Improvement is not limited to 34%NBS.	100%NBS desirable. Improvement should achieve at least 67%NBS
Moderate Risk Building	B or C	Moderate	34 to 66	Acceptable legally. Improvement recommended		Not recommended. Acceptable only in exceptional circumstances
High Risk Building	D or E	High	33 or lower	Unacceptable (Improvement	Unacceptable	Unacceptable

Figure C1: NZSEE Risk Classifications Extracted from table 2.2 of the NZSEE 2006 AISPBE Guidelines

Table C1 below compares the percentage NBS to the relative risk of the building failing in a seismic event with a 10% probability of exceedance in 50 years (i.e. 0.2% in the next year). It is noted that the current seismic risk in Christchurch results in a 6% probability of exceedance in the next year.

Table C1: Relative Risk of Building Failure In A

Percentage of New Building Standard (%NBS)	Relative Risk (Approximate)
>100	<1 time
80-100	1-2 times
67-80	2-5 times
33-67	5-10 times
20-33	10-25 times
<20	>25 times

Appendix D
Background and Legal Framework

Background

This report is a Qualitative Assessment of the building structure, and is based on the Detailed Engineering Evaluation Procedure document (draft) issued by the Structural Advisory Group on 19 July 2011.

A qualitative assessment involves inspections of the building and a desktop review of existing structural and geotechnical information, including existing drawings and calculations, if available.

The purpose of the assessment is to determine the likely building performance and damage patterns, to identify any potential critical structural weaknesses or collapse hazards, and to make an initial assessment of the likely building strength in terms of percentage of new building standard (%NBS).

At the time of this report, no intrusive site investigation, detailed analysis, or modelling of the building structure had been carried out. Construction drawings were made available, and these have been considered in our evaluation of the building. The building description below is based on a review of the drawings and our visual inspections.

Compliance

This section contains a brief summary of the requirements of the various statutes and authorities that control activities in relation to buildings in Christchurch at present.

Canterbury Earthquake Recovery Authority (CERA)

CERA was established on 28 March 2011 to take control of the recovery of Christchurch using powers established by the Canterbury Earthquake Recovery Act enacted on 18 April 2011. This act gives the Chief Executive Officer of CERA wide powers in relation to building safety, demolition and repair. Two relevant sections are:

Section 38 – Works

This section outlines a process in which the chief executive can give notice that a building is to be demolished and if the owner does not carry out the demolition, the chief executive can commission the demolition and recover the costs from the owner or by placing a charge on the owners' land.

Section 51 – Requiring Structural Survey

This section enables the chief executive to require a building owner, insurer or mortgagee carry out a full structural survey before the building is re-occupied.

We understand that CERA will require a detailed engineering evaluation to be carried out for all buildings (other than those exempt from the Earthquake Prone Building definition in the Building Act). It is anticipated that CERA will adopt the Detailed Engineering Evaluation Procedure document (draft) issued by the Structural Advisory Group on 19 July 2011. This document sets out a methodology for both qualitative and quantitative assessments.

The qualitative assessment is a desk-top and site inspection assessment. It is based on a thorough visual inspection of the building coupled with a review of available documentation such as drawings and specifications. The qualitative assessment involves analytical calculation of the buildings strength and may require non-destructive or destructive material testing, geotechnical testing and intrusive investigation.

It is anticipated that factors determining the extent of evaluation and strengthening level required will include:

- The importance level and occupancy of the building
- The placard status and amount of damage
- The age and structural type of the building
- Consideration of any critical structural weaknesses
- The extent of any earthquake damage

Building Act

Several sections of the Building Act are relevant when considering structural requirements:

Section 112 – Alterations

This section requires that an existing building complies with the relevant sections of the Building Code to at least the extent that it did prior to any alteration. This effectively means that a building cannot be weakened as a result of an alteration (including partial demolition).

Section 115 – Change of Use

This section requires that the territorial authority (in this case Christchurch City Council (CCC)) be satisfied that the building with a new use complies with the relevant sections of the Building Code 'as near as is reasonably practicable'. Regarding seismic capacity 'as near as reasonably practicable' has previously been interpreted by CCC as achieving a minimum of 67%NBS however where practical achieving 100%NBS is desirable. The New Zealand Society for Earthquake Engineering (NZSEE) recommend a minimum of 67%NBS.

Section 121 – Dangerous Buildings

The definition of dangerous building in the Act was extended by the Canterbury Earthquake (Building Act) Order 2010, and it now defines a building as dangerous if:

- in the ordinary course of events (excluding the occurrence of an earthquake), the building is likely to cause injury or death or damage to other property; or
- in the event of fire, injury or death to any persons in the building or on other property is likely because of fire hazard or the occupancy of the building; or
- there is a risk that the building could collapse or otherwise cause injury or death as a result of earthquake shaking that is less than a 'moderate earthquake' (refer to Section 122 below); or
- there is a risk that that other property could collapse or otherwise cause injury or death; or
- a territorial authority has not been able to undertake an inspection to determine whether the building is dangerous.

Section 122 – Earthquake Prone Buildings

This section defines a building as earthquake prone if its ultimate capacity would be exceeded in a 'moderate earthquake' and it would be likely to collapse causing injury or death, or damage to other property. A moderate earthquake is defined by the building regulations as one that would generate ground shaking 33% of the shaking used to design an equivalent new building.

Section 124 – Powers of Territorial Authorities

This section gives the territorial authority the power to require strengthening work within specified timeframes or to close and prevent occupancy to any building defined as dangerous or earthquake prone.

Section 131 – Earthquake Prone Building Policy

This section requires the territorial authority to adopt a specific policy for earthquake prone, dangerous and insanitary buildings.

Christchurch City Council Policy

Christchurch City Council adopted their Earthquake Prone, Dangerous and Insanitary Building Policy in 2006. This policy was amended immediately following the Darfield Earthquake of the 4th September 2010.

The 2010 amendment includes the following:

- A process for identifying, categorising and prioritising Earthquake Prone Buildings, commencing on 1 July 2012;
- A strengthening target level of 67% of a new building for buildings that are Earthquake Prone;
- A timeframe of 15-30 years for Earthquake Prone Buildings to be strengthened; and,
- Repair works for buildings damaged by earthquakes will be required to comply with the above.

The council has stated their willingness to consider retrofit proposals on a case by case basis, considering the economic impact of such a retrofit.

We anticipate that any building with a capacity of less than 33%NBS (including consideration of critical structural weaknesses) will need to be strengthened to a target of 67%NBS of new building standard as recommended by the Policy.

If strengthening works are undertaken, a building consent will be required. A requirement of the consent will require upgrade of the building to comply 'as near as is reasonably practicable' with:

- The accessibility requirements of the Building Code.
- The fire requirements of the Building Code. This is likely to require a fire report to be submitted with the building consent application.

Building Code

The building code outlines performance standards for buildings and the Building Act requires that all new buildings comply with this code. Compliance Documents published by The Department of Building and Housing can be used to demonstrate compliance with the Building Code.

After the February Earthquake, on 19 May 2011, Compliance Document B1: Structure was amended to include increased seismic design requirements for Canterbury as follows:

- Hazard Factor increased from 0.22 to 0.3 (36% increase in the basic seismic design load)
- Serviceability Return Period Factor increased from 0.25 to 0.33 (80% increase in the serviceability design loads when combined with the Hazard Factor increase)

The increase in the above factors has resulted in a reduction in the level of compliance of an existing building relative to a new building despite the capacity of the existing building not changing.

Appendix E
Standard Reporting Spread Sheet

Detailed Engineering Evaluation Summary Data V1.11

Location

Building Name:	Walnut Tree Lookout	Reviewer:	Lee Howard
	Unit / No: 53 / Street: Willowview Drive	CPEng No:	1008889
Building Address:	Styx River Conservation Reserve	Company:	Aurecon NZ Ltd
Legal Description:		Company project number:	231556
		Company phone number:	03 366 0821
	Degrees / Min / Sec		
GPS south:	43 / 33 / 38.67	Date of submission:	Oct-13
GPS east:	172 / 39 / 37.13	Inspection Date:	Oct-12
		Revision:	2
Building Unique Identifier (CCC):	PRK 2625 BLDG 001	Is there a full report with this summary?	yes

Site

Site slope:	slope >1 in 5	Max retaining height (m):	2
Soil type:	mixed	Soil Profile (if available):	
Site Class (to NZS1170.5):	D		
Proximity to waterway (m, if <100m):		If Ground improvement on site, describe:	
Proximity to clifftop (m, if < 100m):			
Proximity to cliff base (m,if <100m):		Approx site elevation (m):	8.00

Building

No. of storeys above ground:	1	single storey = 1	Ground floor elevation (Absolute) (m): 8.00
Ground floor split?	no		Ground floor elevation above ground (m): 0.10
Storeys below ground	0		
Foundation type:	other (describe)		if Foundation type is other, describe: floor surported on timber piles
Building height (m):	3.80		height from ground to level of uppermost seismic mass (for IEP only) (m):
Floor footprint area (approx):	30		
Age of Building (years):	3		Date of design: 2004-
Strengthening present?	no		If so, when (year)?
			And what load level (%g)?
Use (ground floor):	public		Brief strengthening description:
Use (upper floors):			
Use notes (if required):	viewing platform		
Importance level (to NZS1170.5):	IL1		

Gravity Structure

Gravity System:	load bearing walls		
Roof:	other (note)	describe system	none
Floors:	timber	joist depth and spacing (mm)	
Beams:	none	overall depth x width (mm x mm)	
Columns:	load bearing walls	typical dimensions (mm x mm)	
Walls:	fully filled concrete masonry	#N/A	

Lateral load resisting structure

Lateral system along:	fully filled CMU	**Note: Define along and across in detailed report!**		
Ductility assumed, μ:	1.25		note total length of wall at ground (m):	
Period along:	1.50	##### enter height above at H31	estimate or calculation?	calculated
Total deflection (ULS) (mm):	70		estimate or calculation?	estimated
maximum interstorey deflection (ULS) (mm):	70		estimate or calculation?	estimated
Lateral system across:	fully filled CMU			
Ductility assumed, μ:	1.25		note total length of wall at ground (m):	
Period across:	1.50	##### enter height above at H31	estimate or calculation?	calculated
Total deflection (ULS) (mm):	70		estimate or calculation?	estimated
maximum interstorey deflection (ULS) (mm):	70		estimate or calculation?	estimated

Separations:

north (mm):		leave blank if not relevant
east (mm):		
south (mm):		
west (mm):		

Non-structural elements

Stairs:		
Wall cladding:	exposed structure	describe
Roof Cladding:		
Glazing:		
Ceilings:	none	
Services(list):		

Available documentation

Architectural	none	original designer name/date	
Structural	none	original designer name/date	
Mechanical	none	original designer name/date	
Electrical	none	original designer name/date	
Geotech report	none	original designer name/date	

Damage

Site: (refer DEE Table 4-2)

Site performance:	good	Describe damage:	
Settlement:	none observed	notes (if applicable):	
Differential settlement:	none observed	notes (if applicable):	
Liquefaction:	none apparent	notes (if applicable):	
Lateral Spread:	none apparent	notes (if applicable):	
Differential lateral spread:	none apparent	notes (if applicable):	
Ground cracks:	none apparent	notes (if applicable):	
Damage to area:	none apparent	notes (if applicable):	

Building:

	Current Placard Status:	green	
Along	Damage ratio:	0%	Describe how damage ratio arrived at:
	Describe (summary):		
Across	Damage ratio:	0%	
	Describe (summary):		
Diaphragms	Damage?:	no	Describe:
CSWs:	Damage?:	no	Describe:
Pounding:	Damage?:	no	Describe:
Non-structural:	Damage?:	no	Describe:

$$Damage\_Ratio = \frac{(\%NBS(before) - \%NBS(after))}{\%NBS(before)}$$

Recommendations

	Level of repair/strengthening required:	none	Describe:
	Building Consent required:	no	Describe:
	Interim occupancy recommendations:	full occupancy	Describe:
Along	Assessed %NBS before e'quakes:	73%	0% %NBS from IEP below
	Assessed %NBS after e'quakes:	73%	If IEP not used, please detail assessment methodology: direct code comparison
Across	Assessed %NBS before e'quakes:	73%	0% %NBS from IEP below
	Assessed %NBS after e'quakes:	73%	

IEP

Use of this method is not mandatory - more detailed analysis may give a different answer, which would take precedence. Do not fill in fields if not using IEP.

Period of design of building (from above): 2004-

h_n from above: m

Seismic Zone, if designed between 1965 and 1992:

Design Soil type from NZS1170.5:2004, cl 3.1.3:
not required for this age of building

	along	across
Period (from above):	1.5	1.5
(%NBS)nom from Fig 3.3:	0.0%	0.0%

Note:1 for specifically design public buildings, to the code of the day: pre-1965 = 1.25; 1965-1976, Zone A =1.33; 1965-1976, Zone B = 1.2; all else 1.0	1.00
Note 2: for RC buildings designed between 1976-1984, use 1.2	1.0
Note 3: for buildngs designed prior to 1935 use 0.8, except in Wellington (1.0)	1.0

	along	across
Final $(\%NBS)_{nom}$:	**0%**	**0%**

2.2 Near Fault Scaling Factor

		along	across
Near Fault scaling factor, from NZS1170.5, cl 3.1.6:			1.00
Near Fault scaling factor (1/N(T,D), **Factor A**:		1	1

2.3 Hazard Scaling Factor

Hazard factor Z for site from AS1170.5, Table 3.3:	0.30
Z_{1992}, from NZS4203:1992	
Hazard scaling factor, **Factor B**:	0

2.4 Return Period Scaling Factor

Building Importance level (from above):	1
Return Period Scaling factor from Table 3.1, **Factor C**:	1.00

2.5 Ductility Scaling Factor

	along	across
Assessed ductility (less than max in Table 3.2)	1.25	1.25
Ductility scaling factor: =1 from 1976 onwards; or =kμ, if pre-1976, fromTable 3.3:	1.14	1.14
Ductiity Scaling Factor, **Factor D**:	1.00	1.00

2.6 Structural Performance Scaling Factor:

	along	across
Sp:	0.925	0.925
Structural Performance Scaling Factor **Factor E**:	1.081081081	1.081081081

2.7 Baseline %NBS, $(NBS\%)_b = (\%NBS)_{nom} \times A \times B \times C \times D \times E$

	along	across
$\%NBS_b$:	**0%**	**0%**

Global Critical Structural Weaknesses: (refer to NZSEE IEP Table 3.4)

3.1. Plan Irregularity, factor A:	insignificant	1
3.2. Vertical irregularity, Factor B:	insignificant	1
3.3. Short columns, Factor C:	insignificant	1

3.4. Pounding potential

Pounding effect D1, from Table to right	1.0
Height Difference effect D2, from Table to right	1.0
Therefore, Factor D:	1

Table for selection of D1	Severe	Significant	Insignificant/none
Separation	0<sep<.005H	.005<sep<.01H	Sep>.01H
Alignment of floors within 20% of H	**0.7**	**0.8**	**1**
Alignment of floors not within 20% of H	**0.4**	**0.7**	**0.8**

Table for Selection of D2	Severe	Significant	Insignificant/none
Separation	0<sep<.005H	.005<sep<.01H	Sep>.01H
Height difference > 4 storeys	0.4	0.7	1
Height difference 2 to 4 storeys	0.7	0.9	1
Height difference < 2 storeys	1	1	1

3.5. Site Characteristics	insignificant	1

3.6. Other factors, Factor F

	Along	Across
For ≤ 3 storeys, max value =2.5, otherwise max valule =1.5, no minimum	1.0	1.0
Rationale for choice of F factor, if not 1		

Detail Critical Structural Weaknesses: (refer to DEE Procedure section 6)
List any: Refer also section 6.3.1 of DEE for discussion of F factor modification for other critical structural weaknesses

	along	across
3.7. Overall Performance Achievement ratio (PAR)	**1.00**	**1.00**
4.3 PAR x (%NBS)b: PAR x Baselline %NBS:	**0%**	**0%**
4.4 Percentage New Building Standard (%NBS), (before)		**0%**

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